

# Thévenin & Norton Equivalent Circuits

## Lecture 4 review:

- Nodal analysis
- Loop analysis
- Series and parallel resistors

## Today:

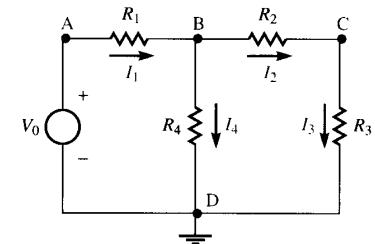
- Equivalent circuits (Thévenin & Norton equivalents)
- Series & parallel resistors (revisit & generalize)
- Voltage divider & current divider
- Real voltmeters & ammeters

# Node Analysis

**Goals:** Solve all unknown node voltages.

## How?

•By writing equations expressing Kirchhoff's current law (KCL) for each node where the voltage is unknown.



# Node Analysis (cont.)

5 circuit elements - 4 resistors, 1 voltage source.

4 nodes:

2 unknown voltages:  $v_B, v_C$

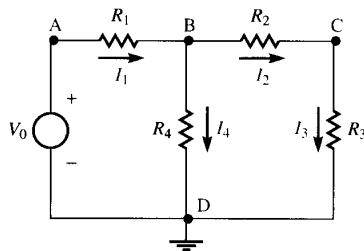
2 known voltages:

1 reference voltage:  $v_D$

1 voltage source:  $v_A = v_0$

4 branch currents:  $I_1, I_2, I_3, I_4$

(but  $I_2 = I_3$ ) => 3 unknown currents



Apply KCL at node B:

$$\frac{V_0 - V_B}{R_1} + \frac{V_C - V_B}{R_2} + \frac{V_D - V_B}{R_4} = 0$$

Apply KCL at node C:

$$\frac{V_B - V_C}{R_2} + \frac{V_D - V_C}{R_3} = 0$$

But  $V_D = 0$  in both cases.

# Node Analysis

$$\frac{V_0 - V_B}{R_1} + \frac{V_C - V_B}{R_2} + \frac{-V_B}{R_4} = 0$$

$$\frac{V_B - V_C}{R_1} + \frac{-V_C}{R_3} = 0$$

2 equations and 2 unknowns.

Can be solved simultaneously for  $V_B$  &  $V_C$

$$V_C = V_0 \cdot \frac{R_3 R_4}{R_1 R_2 + R_1 R_3 + R_1 R_4 + R_2 R_4 + R_3 R_4}$$

$$\left. \begin{aligned} V_B &= f(V_0) \\ V_C &= f(V_0) \end{aligned} \right\}$$

$$V_B = V_0 \cdot \frac{R_4 (R_2 + R_3)}{R_1 R_2 + R_1 R_3 + R_1 R_4 + R_2 R_4 + R_3 R_4}$$

$$\text{if } \begin{cases} V_0 = 0 \\ V_B = V_C = 0 \end{cases}$$

What about the 4 branch currents?

Apply Ohm's law

$$I_1 = \frac{V_A - V_B}{R_1} = \frac{V_0 - V_B}{R_1} \quad I_2 = \frac{V_B - V_C}{R_2} \quad I_3 = \frac{V_C - V_D}{R_3} = \frac{V_C}{R_3} \quad I_4 = \frac{V_B - V_D}{R_4} = \frac{V_B}{R_4}$$

## Node Analysis (nodal analysis)

- 1 Choose a Reference Node  $\equiv$
- 2 Define unknown node voltages (those not fixed by voltage sources)
- 3 Write KCL at each unknown node, expressing current in terms of the node voltages (using the constitutive relationships of branch elements: **for resistor element use Ohm's law**)
- 4 Solve the set of equations (N equations for N unknown node voltages)

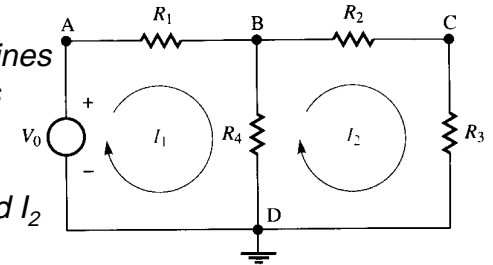
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## Loop Analysis

- In node analysis (or nodal analysis), voltage is obtained first by using KCL, then current is found by using the V-I characteristic of the circuit element (for resistor element: Ohm's law).
- In loop analysis, current is obtained first by KVL, then voltage is found by using the V-I characteristic (for resistor element: Ohm's law).

In loop analysis, one defines special current known as **mesh currents**.

In this example, 2 mesh currents is defined,  $I_1$  and  $I_2$

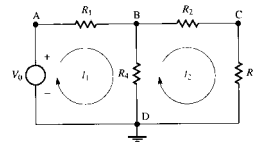


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## Loop Analysis (Mesh Analysis)

The number of mesh currents = (Number of branches) - (Number of nodes) + 1

In this case, there are 4 nodes, 5 branches.  
# of mesh = 5 - 4 + 1 = 2



### How to define mesh current?

A lot of freedom, except that every branch of the circuit have at least one mesh current flowing thru it.

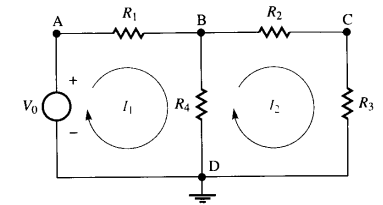
The value of the mesh currents are now the unknown to be solved for. The number of equations = The number of unknown mesh current

**The equations** are obtained by applying Kirchhoff Voltage law on the loops of the mesh currents.

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## Loop Analysis

Assume  $I_1$  and  $I_2$  are defined as the mesh current. Notice the mesh current go thru the whole loop.  $R_4$  has 2 mesh currents go thru it.



The voltage drop from A to B across  $R_1$ :  $I_1 R_1$

The voltage drop from B to D across  $R_4$ :  $(I_1 - I_2) R_4$

Apply KVL in the loop ABDA:

$$I_1 R_1 + (I_1 - I_2) R_4 - V_0 = 0$$

Apply KVL in the loop BCDB:

$$I_2 R_2 + I_2 R_3 + (I_2 - I_1) R_4 = 0$$

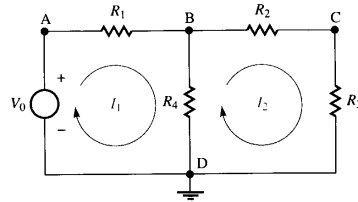
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## Loop Analysis

Solving these 2 equations simultaneously:

$$I_1 = V_0 \frac{R_2 + R_3 + R_4}{R_1 R_2 + R_1 R_3 + R_1 R_4 + R_2 R_4 + R_3 R_4}$$

$$I_2 = V_0 \frac{R_4}{R_1 R_2 + R_1 R_3 + R_1 R_4 + R_2 R_4 + R_3 R_4}$$



The individual branch current and voltage can be found from  $I_1$  and  $I_2$ .

$$V_{CD} = V_C = I_2 R_3 = V_0 \frac{R_4 R_3}{R_1 R_2 + R_1 R_3 + R_1 R_4 + R_2 R_4 + R_3 R_4}$$

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## Loop Analysis (mesh analysis)

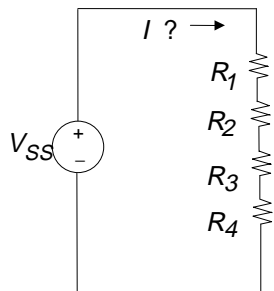
1. Select the **proper number of mesh current** such that at least one mesh current passes through each branch.
2. (a) **Express voltage drop across each element as functions of known and unknown mesh currents**,  
(b) write equations stating that the sum of the voltage drop around closed path are zero. (**KVL**)
3. **Solve equations** obtained in step 2 simultaneously for unknown mesh current.
4. Obtain branch currents from the mesh current found in in step 3 and obtain desired node voltages from branch currents and the  $I$ - $V$  relationship of the branches.

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## RESISTORS IN SERIES

(Here its more convenient to use KVL than node analysis)

Circuit with several resistors in series – Can we find an equivalent resistance?



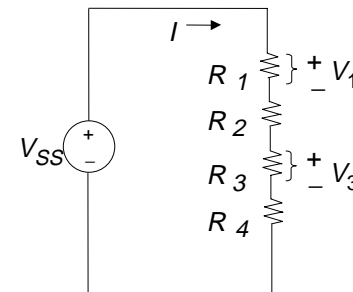
- KCL tells us same current flows through every resistor
- KVL tells us  $I \cdot R_1 + I \cdot R_2 + I \cdot R_3 + I \cdot R_4 = V_{SS}$
- Clearly,  $I = V_{SS} / (R_1 + R_2 + R_3 + R_4)$

☞ Thus, equivalent resistance of resistors in series is the simple sum

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## GENERALIZED VOLTAGE DIVIDER

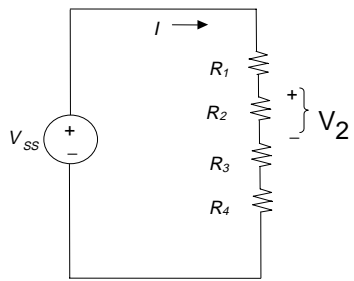
Circuit with several resistors *in series*



- We know  $I = V_{SS} / (R_1 + R_2 + R_3 + R_4)$
- Thus,  $V_1 = \frac{R_1}{R_1 + R_2 + R_3 + R_4} \cdot V_{SS}$   
and  $V_3 = \frac{R_3}{R_1 + R_2 + R_3 + R_4} \cdot V_{SS}$   
etc.. etc..

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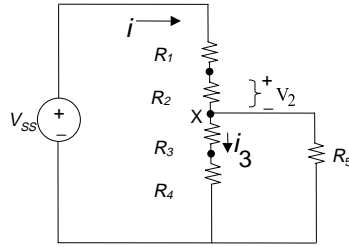
### WHEN IS VOLTAGE DIVIDER FORMULA CORRECT?



$$V_2 = \frac{R_2}{R_1 + R_2 + R_3 + R_4} \times V_{SS}$$

Correct if nothing else connected to nodes

What is  $V_2$ ?



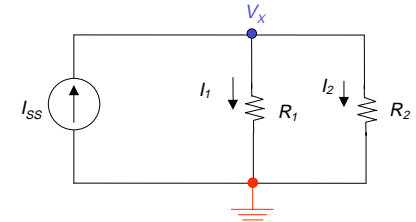
$$V_2 \neq \frac{R_2}{R_1 + R_2 + R_3 + R_4} \times V_{SS}$$

because  $R_5$  removes condition of resistors in series – i.e.  $i_3 \neq I$

Answer: 
$$\frac{R_2}{R_1 + R_2 + R_5 \parallel (R_3 + R_4)} \times V_{SS}$$

### RESISTORS IN PARALLEL

- 1 Select Reference Node
- 2 Define unknown node voltages



Note:  $I_{SS} = I_1 + I_2$ , i.e.,

$$I_{SS} = \frac{V_X}{R_1} + \frac{V_X}{R_2} \Rightarrow V_X = I_{SS} \cdot \frac{1}{\frac{1}{R_1} + \frac{1}{R_2}} = I_{SS} \cdot \frac{R_1 R_2}{R_1 + R_2}$$

RESULT 1 EQUIVALENT RESISTANCE:  $R_{\parallel} \equiv R_1 \parallel R_2 = \frac{R_1 R_2}{R_1 + R_2}$

RESULT 2 CURRENT DIVIDER:  $I_1 = \frac{V_X}{R_1} = I_{SS} \times \frac{R_2}{R_1 + R_2}$

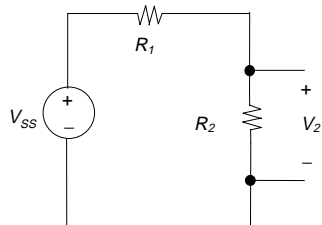
$$I_2 = \frac{V_X}{R_2} = I_{SS} \times \frac{R_1}{R_1 + R_2}$$

### REAL VOLTMETERS

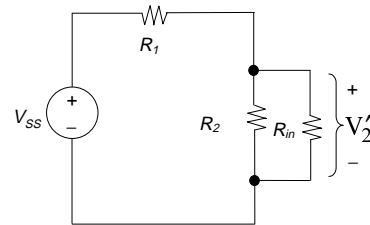
#### Concept of “Loading” as Application of Parallel Resistors

How is voltage measured? Modern answer: Digital multimeter (DMM)

Problem: Connecting leads from voltmeter across two nodes changes the circuit. The voltmeter is characterized by how much current it draws at a given voltage → “voltmeter input resistance,”  $R_{in}$ . Typical value: 10 M $\Omega$



$$V_2 = V_{SS} \left[ \frac{R_2}{R_1 + R_2} \right]$$



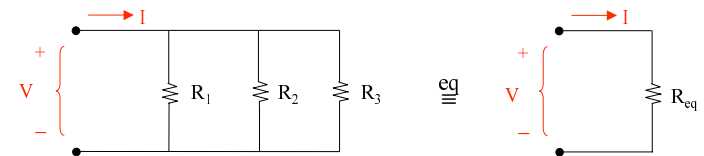
$$V'_2 = V_{SS} \left[ \frac{R_2 \parallel R_{in}}{R_2 \parallel R_{in} + R_1} \right]$$

Example:  $V_{SS} = 10V, R_2 = 100K, R_1 = 900K \Rightarrow V_2 = 1V$

But if  $R_{in} = 10M, V'_2 = 0.991V$ , a 1% error

### GENERALIZED PARALLEL RESISTORS

What single resistance  $R_{eq}$  is equivalent to three resistors in parallel?



$$I = \frac{V}{R_1} + \frac{V}{R_2} + \frac{V}{R_3} \equiv \frac{V}{R_{eq}} \Rightarrow R_{eq} \equiv R_1 \parallel R_2 \parallel R_3 = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}}$$

Note the simplicity if we use conductance instead of resistance

$$G_1 \equiv \frac{1}{R_1}, \text{ etc., } G_{eq} \equiv \frac{1}{R_{eq}}$$

Then,  $G_{eq} = G_1 + G_2 + G_3$

**ADD CONDUCTANCES IN PARALLEL**

### GENERALIZED CURRENT DIVIDER

Current splits among M resistors in parallel

Formal approach: 
$$V = \frac{I}{\left(\frac{1}{R_1}\right) + \left(\frac{1}{R_2}\right) + \left(\frac{1}{R_3}\right)}$$

$$I_3 = \frac{V}{R_3} = I \left[ \frac{1/R_3}{1/R_1 + 1/R_2 + 1/R_3} \right]$$

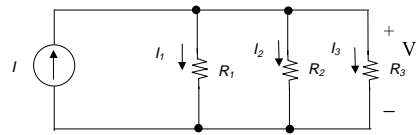
Note  $I_3 = I \left[ \frac{G_3}{G_1 + G_2 + G_3} \right]$

$$I_3 = I \left[ \frac{R_1 R_2}{R_2 R_3 + R_1 R_3 + R_1 R_2} \right] = I \left[ \frac{R_1 R_2 / (R_1 + R_2)}{R_1 R_2 / (R_1 + R_2) + R_3} \right]$$

Can we get this result by inspection?

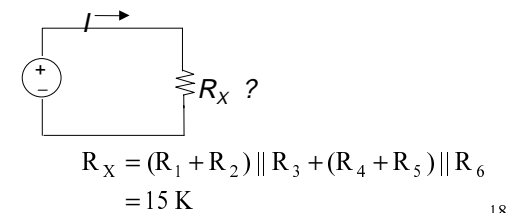
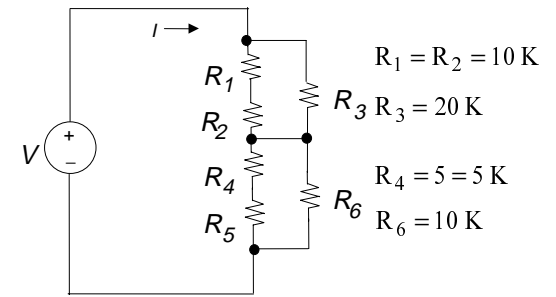
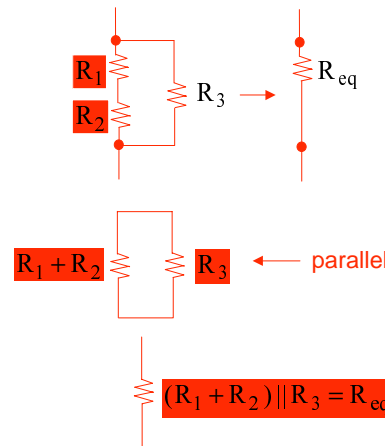
YES – Consider  $R_1 || R_2$  as “one equivalent resistor”

$$\text{Then } I_3 = \frac{R_1 || R_2}{R_1 || R_2 + R_3} \times I = \frac{R_1 R_2 / (R_1 + R_2)}{R_1 R_2 / (R_1 + R_2) + R_3} \times I$$



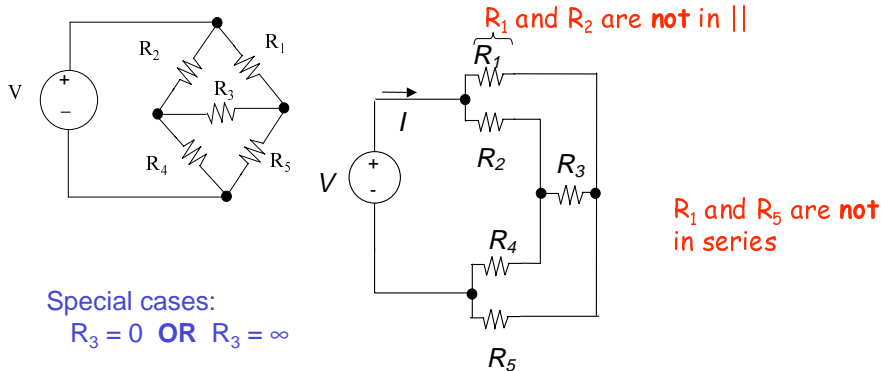
### IDENTIFYING SERIES AND PARALLEL COMBINATIONS

Use series/parallel equivalents to simplify a circuit before starting KVL/KCL



### IDENTIFYING SERIES AND PARALLEL COMBINATIONS (cont.)

Some circuits *must* be analyzed (not amenable to simple inspection)



Special cases:  
 $R_3 = 0$  OR  $R_3 = \infty$

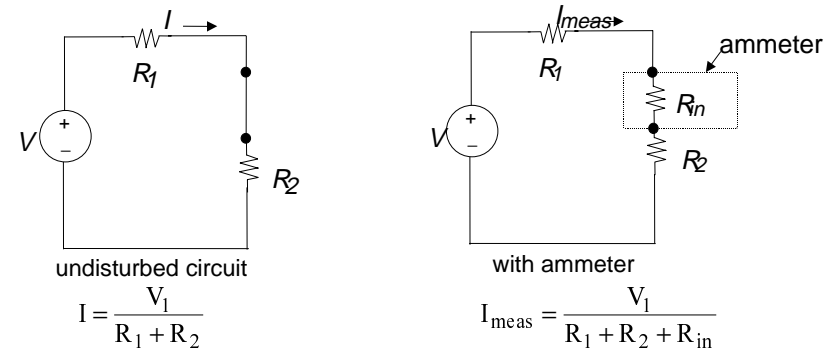
Example:  $R_3 = 0 \Rightarrow R_1 || R_2; R_4 || R_5$  in series;  $R_{eq} = R_1 || R_2 + R_4 || R_5$

OR IF  $R_3 = \infty \Rightarrow (R_1 + R_5) || (R_2 + R_4)$

### MEASURING CURRENT

Insert DMM (in current measurement mode) into circuit. But ammeters disturb the circuit. (Note: Ammeters are characterized by their “ammeter input resistance,”  $R_{in}$ . Ideally this should be very low. Typical value (in mA range)  $1\Omega$ .)

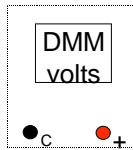
Potential measurement error due to non-zero input resistance:



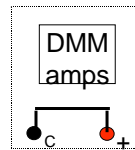
Example  $V = 1 \text{ V}; R_1 + R_2 = 1 \text{ K}\Omega$ ,  $R_{in} = 1\Omega$

$$I = 1 \text{ mA}, \quad I_{meas} = \frac{1}{1\text{K} + 1\Omega} \cong 0.999 \text{ mA} \quad (0.1\% \text{ error})$$

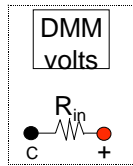
### IDEAL AND NON-IDEAL METERS



IDEAL



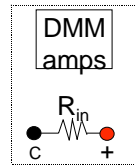
IDEAL



MODEL OF REAL DIGITAL VOLTMETER

Note:  $R_{in}$  may depend on range

$R_{in}$  typically  $\gtrsim 10\text{ M}\Omega$

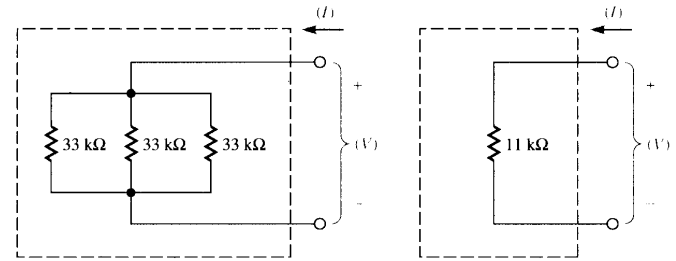


MODEL OF REAL DIGITAL AMMETER

Note:  $R_{in}$  usually depends on current range

$R_{in}$  typically  $\sim 1\ \Omega$

### Equivalent Circuits



Circuits on the left side is equivalent to the circuit on the right. Both circuits have a V-I curve equivalent to a  $11\text{ k}\Omega$  resistor.

### Composite Circuit Element

Find the I-V relationship of the circuit on the right.

KCL equation at node X:

$$10^{-2} + \frac{V_Y - V_X}{100} + I = 0$$

$$V_X = V_Y + 100I + 1$$

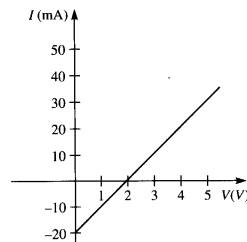
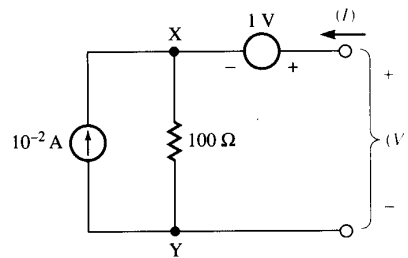
V is equal to:  $V = V_{XY} + 1 = V_X - V_Y + 1$

Substitute 2nd eq to 3rd eq:

$$V = (V_Y + 100I + 1 - V_Y) + 1 = 100I + 2$$

or

$$I = 10^{-2}V - 20 \times 10^{-3}$$



### Example

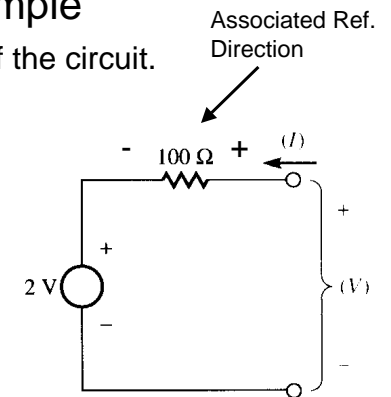
Calculate the I-V relationship of the circuit.

Write a KVL equation for this loop:

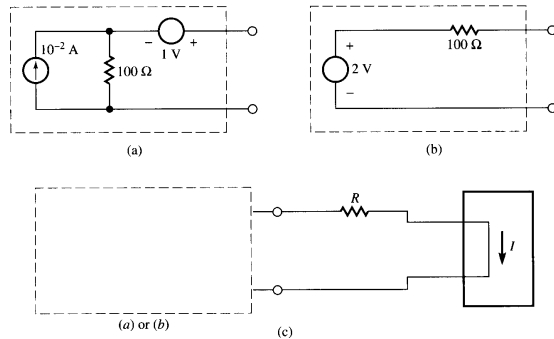
$$+V - 2 - 100I = 0$$

$$\Rightarrow I = 10^{-2}V - 20 \times 10^{-3}$$

$\therefore$  This circuit has an identical I-V relationship as the previous one  $\Rightarrow$  This circuit is equivalent to the previous circuit.

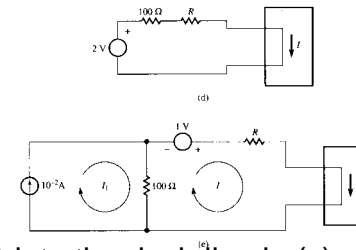


### Equivalent circuit



From the previous slide, ckt (a) and ckt (b) are equivalent. Let's check:  
 Substitute ckt (b) into the dash line in (c), we get ckt (d). We can solve this by Ohm's law:  
 $2 = I(100 + R) \Rightarrow I = \frac{2}{100 + R}$  (from subckt (b))

### Equivalent circuit example (cont.)



Substitute ckt (c) into the dash line in (c), we get ckt (e). Here we use loop analysis. 2 mesh current  $I_1$  and  $I$ . But  $I_1$  is already known. It is equal  $10^{-2}A$ .

The next loop equation is:  $100(I - I_1) - 1 + IR = 0$

Solve for I yields:  $I = \frac{2}{100 + R}$  (subckt (a)) (ckts (d) & (e) result in identical I)

∴ The operation of the remainder of a ckt is unaffected when a subcircuit is replaced by its equivalent.

### Equivalent circuits

- Two type of equivalent circuits
  - Thévenin equivalent circuits
  - Norton equivalent circuits

### Thévenin Equivalent Circuits

General form of Thévenin equivalent is shown in the ckt on right.

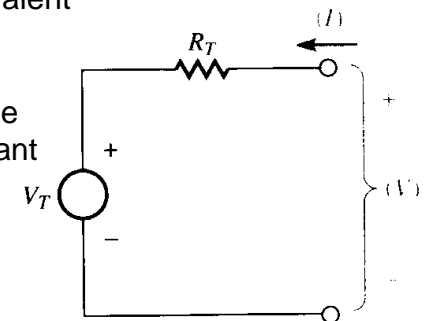
$V_T$  is called the Thévenin voltage  
 $R_T$  is called the Thévenin resistant  
 By KVL around the loop:

$$V - V_T - R_T I = 0$$

Simplifies into:

$$I = \frac{V}{R_T} - \frac{V_T}{R_T}$$

With  $1/R_T$  as the slope in the I-V graph and  $-V_T/R_T$  as the "y" intercept c. (Remember  $y=mx+c$ ?)



## Thévenin equivalent

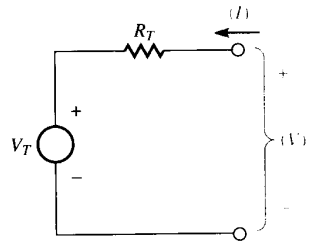
In order to find the Thévenin equivalent of a circuit, we need to find  $V_T$  and  $R_T$ . The next question is how to find  $V_T$  and  $R_T$ .

When this circuit is open circuit,  $I = 0$ .

$$I = \frac{V}{R_T} - \frac{V_T}{R_T} \quad (1)$$

becomes

$$0 = \frac{V_{OC}}{R_T} - \frac{V_T}{R_T} \Rightarrow \boxed{V_T = V_{OC}}$$



We can compute the  $R_T$  by using the  $I_{SC}$  (short circuit current):

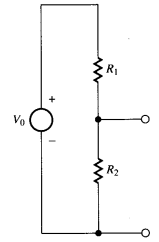
$$I_{SC} = \frac{0}{R_T} - \frac{V_T}{R_T} \Rightarrow \boxed{R_T = -\frac{V_T}{I_{SC}} = -\frac{V_{OC}}{I_{SC}}}$$

## Thévenin equivalent example

Find the Thévenin equivalent circuit.

We can solve this by 2 steps:

- (1) Find  $V_T$  by finding  $V_{OC}$
- (2) Find  $R_T$  by find  $I_{SC}$



$V_{OC}$  can be found by inspection (it is a voltage divider):

$$V_T = V_{OC} = V_0 \frac{R_2}{R_1 + R_2} \quad (a)$$

## Thévenin equivalent example cont.

Next we calculate  $I_{SC}$  as shown in circuit on the right.

Apply KCL at node A:

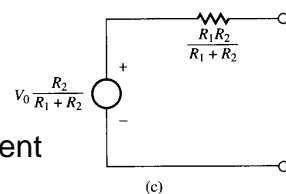
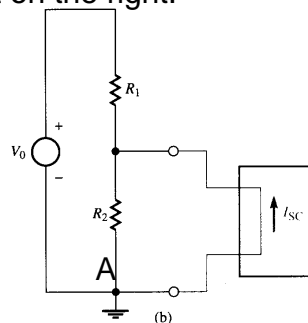
$$\frac{V_0 - 0}{R_1} + \frac{0 - 0}{R_2} + I_{SC} = 0 \Rightarrow I_{SC} = -\frac{V_0}{R_1} \quad (b)$$

From previous slide,  $R_T = -\frac{V_{OC}}{I_{SC}} \quad (c)$

Substitute (b) and (a) into (c)

$$R_T = V_{OC} \left( \frac{R_1}{V_0} \right) = V_0 \left( \frac{R_2}{R_1 + R_2} \right) \left( \frac{R_1}{V_0} \right) = \frac{R_1 R_2}{R_1 + R_2}$$

$\therefore$  Circuit © shows a Thévenin equivalent of the original circuit.



## Thévenin equivalent (alternative method)

There is an alternative method for finding  $R_T$ :

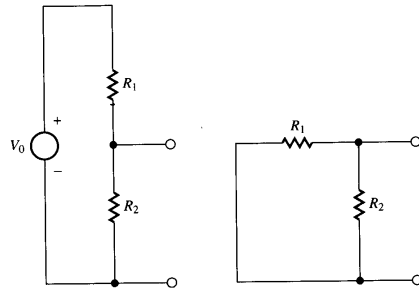
- Locate all independent voltage & current source inside the subcircuit whose equivalent is to be found.
- Replace all independent voltage sources by short circuits
- Replace all independent current sources by open circuits
- Compute the resistance between the 2 terminals



## Thévenin equivalent (alternative method) example

Find the  $R_T$  by the alternative method:

- Replace the voltage source by short circuit (current source by open circuit).
- Measure the resistance across the 2 terminals.
- The modified circuit becomes the circuit on the right.

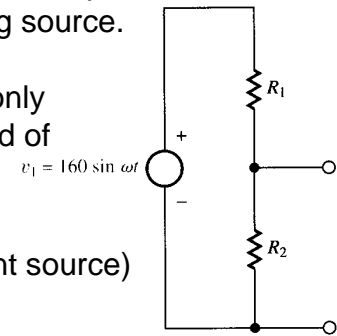


$$R_T = R_1 \parallel R_2$$

## Thévenin equivalent (time varying source)

This is identical to the previous example except that it has a time varying source.

The method is the same. The only difference is the source. Instead of  $V_0$ , we use  $V_1$  as source:



$$V_T = V_{OC} = V_0 \frac{R_2}{R_1 + R_2} \text{ (time invariant source)}$$

$$V_T = V_{OC} = V_1 \frac{R_2}{R_1 + R_2} = 160 \sin(\omega t) \frac{R_2}{R_1 + R_2} \text{ (time varying source)}$$

$$R_T = V_{OC} \left( \frac{R_1}{V_1} \right) = V_1 \left( \frac{R_2}{R_1 + R_2} \right) \left( \frac{R_1}{V_1} \right) = \frac{R_1 R_2}{R_1 + R_2}$$

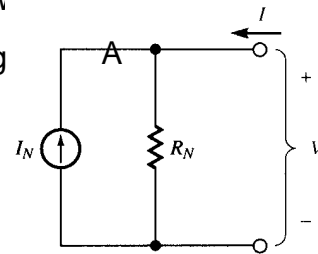
(time varying source)  
(time varying source)  
In this case,  $R_T$  does not depend time, thus, the same.

## Norton Equivalent Circuits

Principle of the Norton equivalent circuit is similar to that of the Thevenin equivalent circuit. Consider the general form of Norton equivalent circuit below:

We can find the I-V equation by applying KCL at node A:

$$I - \frac{V}{R_N} + I_N = 0 \Rightarrow I = \frac{V}{R_N} - I_N \quad (1)$$



Next we need to find  $I_N$  and  $R_N$ .

Use similar strategy as in Thevenin equivalent.

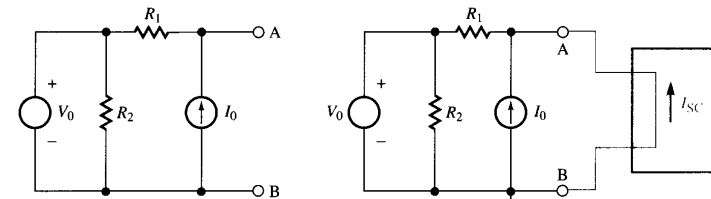
First short circuit the 2 terminals yields ( $I$  becomes  $I_{SC}$ ,  $V=0$  in eq. 1):

$$I_{SC} = \frac{0}{R_N} - I_N \Rightarrow I_N = -I_{SC}$$

Next we open circuit the terminals ( $I=0$ ,  $V=V_{OC}$  in eq. 1):

$$0 = \frac{V_{OC}}{R_N} - I_N \Rightarrow R_T = -\frac{V_{OC}}{I_{SC}}$$

## Norton equivalent circuits (example)



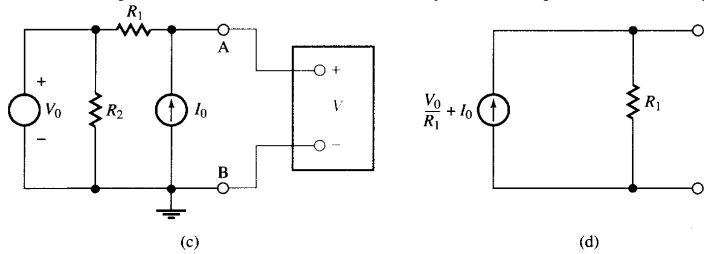
Find the Norton equivalent ckt of the ckt on the left.

First, find  $I_{SC}$  (the current indicated by an ideal ammeter connected to the terminals A and B.)

Apply KCL at node A in the right ckt :  $\frac{V_0 - 0}{R_1} + I_0 + I_{SC} = 0$

or  $I_{SC} = -\frac{V_0}{R_1} - I_0$

## Norton equivalent circuits (example cont.)



Next, find  $V_{OC}$  (from ideal voltmeter connected to terminals A&B)

Apply KCL at node A (assume open circuit,  $I=0$ ) (see circuit c):

$$\frac{V_0 - V_{OC}}{R_1} + I_0 = 0 \quad \text{or} \quad V_{OC} = I_0 R_1 + V_0$$

Use  $V_{OC}$  and  $I_{SC}$ , we can find  $I_N$  and  $R_N$  ( $I_N = -I_{SC}$ ,  $R_T = -\frac{V_{OC}}{I_{SC}}$ ):

$$I_N = \frac{V_0}{R_1} + I_0 \quad \text{and} \quad R_N = R_1$$