

$$R = 10 \text{ k}\Omega$$

$$V_1 = 15 \text{ V}$$

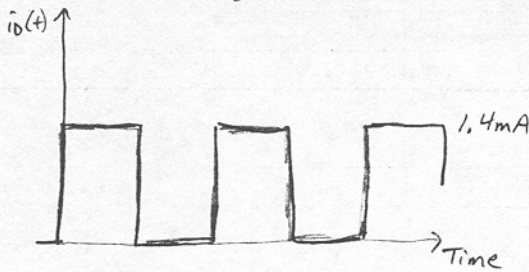
Current through resistor = Current through diode

$$\frac{v_D(t) - v_D(t)}{R} = I_S \left( e^{\frac{v_D(t)q}{kT}} - 1 \right) \quad I_S = 10^{-13} \text{ A}$$

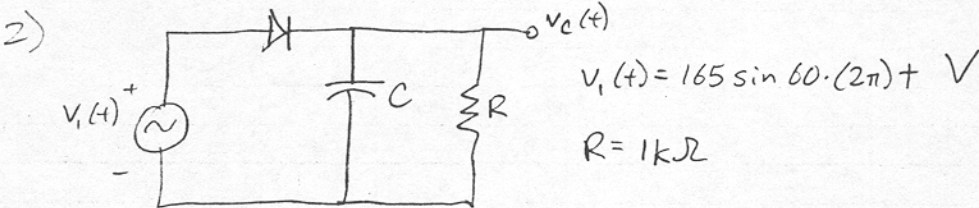
When  $v_D(t) = 0$ , current = 0

$$\text{When } v_D(t) = 15 \text{ V}, \quad \frac{15 - V_D}{10 \text{ k}\Omega} - 10^{-13} \left( e^{V_D/26 \text{ mV}} - 1 \right) = 0$$

$$\Rightarrow V_D = .608 \text{ V} \quad \text{current} = 1.4 \text{ mA}$$



Current graph has the same shape as the voltage graph

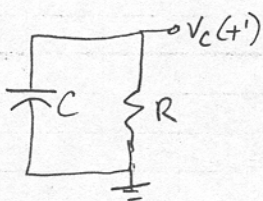


$$v_1(t) = 165 \sin 60 \cdot (2\pi) t \text{ V}$$

$$R = 1 \text{ k}\Omega$$

Remember that we assume the capacitor is fully charged when  $v_1(t) = 165 \text{ V}$  (time =  $t_1$ ). Current in the circuit may be very high, but finite.

During the discharge cycle (which starts at  $t' = 0$ ), the load behaves like:



$$v_C(t') = 165 e^{-\frac{t'}{RC}}$$

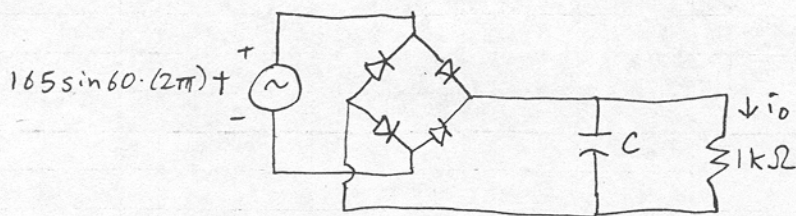
We want voltage to drop 0.5V in  $\frac{1}{60} \text{ s}$ :

$$164.5 = 165 e^{-\frac{1}{60RC}}$$

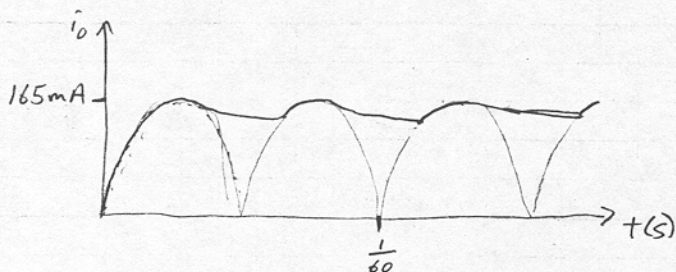
$$\ln\left(\frac{164.5}{165}\right) = -\frac{1}{60RC}$$

$$C = 5.5 \text{ mF} \quad \leftarrow \text{that's BIG!}$$

3)



Current through the resistor (with and without filter cap) looks like this:

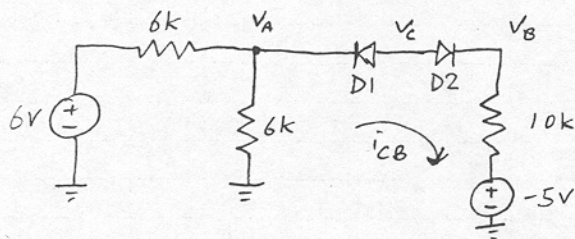


Compare this with Fig 13.15 in the book

This is really the same as the previous problem, except the discharge cycle last  $\approx \frac{1}{120}$  s.

$$\ln\left(\frac{164.5}{165}\right) = -\frac{1}{120RC} \Rightarrow C = 2.75 \text{ mF (half the previous answer)}$$

4)



a) if the diodes are perfect rectifiers, current can only flow in the direction of the diode arrow. By KCL, no current flows through either diode. Hence

$$V_A = 6V \frac{6k}{6k+6k} = 3V \quad V_B = -5V$$

$V_C$  is anywhere between  $-5V$  and  $3V$  (inclusive)

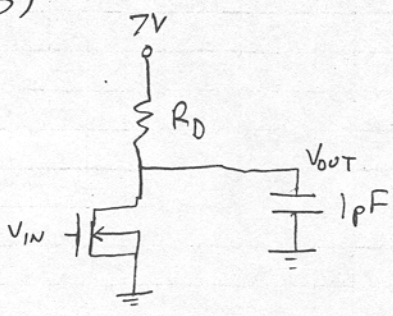
b) Again using KCL, the upper bound on  $|i_{CB}| = I_S = 10^{-16} \text{ A} \approx 0$  since current must flow against a diode arrow either way. ( $i_{CB} = +I_S$ , assuming  $V_A > V_B$ )

So again,  $V_A \approx 3V$  and  $V_B \approx -5V$  since the current through the diode is small.  $V_C$ , however, isn't arbitrary. We need:

$$I_S \left( e^{\frac{V_C - 3}{0.026}} - 1 \right) + I_S \left( e^{\frac{V_C - (-5)}{0.026}} - 1 \right) = 0$$

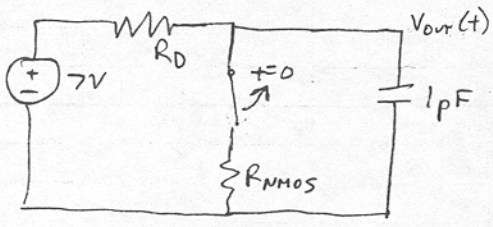
$$\Rightarrow V_C = -5 + 0.026 \ln 2 = -4.982$$

5)



(ignoring load capacitance)  
 When  $V_{IN} = 7V$ ,  $V_{OUT} = 0.6V$   
 $V_{IN} = 0V$ ,  $V_{OUT} = 7V$

We can draw an equivalent switch circuit, modelling the MOS as a switch plus resistor.

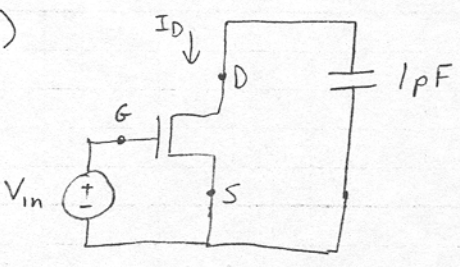


$V_{OUT}(0) = 0.6V$   
 $V_{OUT}(\infty) = 7V$

$V_{OUT}(t) = 7 - 6.4e^{-t/RC}$   
 $R_D = 23k\Omega$ ,  $C = 1pF$   
 $= 3.8V \Rightarrow t = 15.9ns$

When the input is 7V, there is 0.275mA flowing from VDD to ground (through the resistor and NMOS transistor), so power = 0.275mV \* 7V = 1.925mW

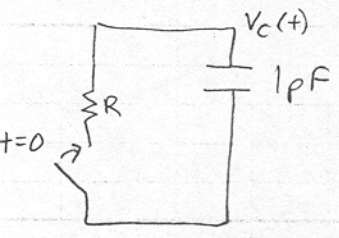
6)



- a)  $i_D = C \frac{\partial v_c}{\partial t}$   
 $v_c(t)$  is linear with a slope of  $\frac{dv}{dt} = 2E9 V/s$
- b)  $\Delta t = \frac{C}{i_D} \Delta V = \frac{1s}{2E9V} \cdot 1V = 500ps$

Using a switch model:

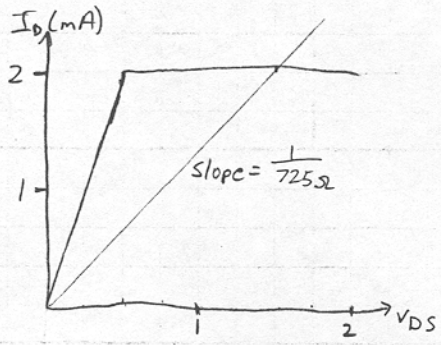
c) Here  $v_c(t)$  is a decaying exponential from 2V to 0V



$v_c(t) = 2e^{-t/RC}$   
 $= 1 \Rightarrow t = 0.69RC$

- d)  $500ps = 0.69 \cdot R \cdot 1pF \Rightarrow R = 725\Omega$   
 Remember that the  $v_c$  curves look different in parts (a) and (c), but coincide at  $t=0$  and  $t=500ps$ . That's all we want.

e)



The two plots cross at  $V = 1.45V$ , which is roughly the average of 1V and 2V.



## (Additional comments)

4b) This question could be solved using nodal analysis:

$$\frac{6 - V_A}{6k} + \frac{0 - V_A}{6k} + I_S \left( e^{\frac{V_C - V_A}{-0.026}} - 1 \right) = 0$$

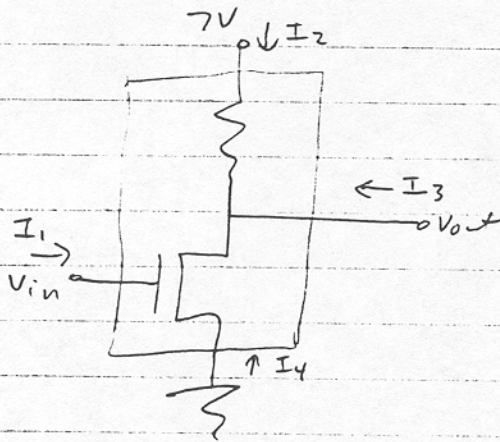
$$I_S \left( e^{\frac{V_C - V_B}{-0.026}} - 1 \right) + \frac{V_B + 5}{10k} = 0$$

$$I_S \left( e^{\frac{V_C - V_B}{-0.026}} - 1 \right) + I_S \left( e^{\frac{V_C - V_A}{-0.026}} - 1 \right) = 0$$

but involves solving a bunch of nonlinear equations (not fun).

Also,  $V_A$  is not exactly 3V and  $V_B$  is not exactly -5V, but very close (to the 12<sup>th</sup> decimal place).

5b) The inverter is just another "box" with ports:



$$\text{Power} = I_1 (V_{in} - 0) + I_2 (7V - 0) + I_3 (V_{out} - 0) + I_4 (0 - 0)$$

We know that  $I_1 = 0$ .  $I_3$  is also 0. (if we still have our load capacitor,  $I_3$  will also eventually be 0. In this case we are solving for "static" power dissipation)

$$\begin{aligned} \text{So Power} &= 0 \cdot (7 - 0) + I_2 (7V) + 0 (0.6 - 0) + I_4 (0) \\ &= I_2 \cdot 7V = .275 \text{mA} \cdot 7V = 1.925 \text{mW} \end{aligned}$$