

EE247

Lecture 22

ADC Converters

- Techniques to reduce flash ADC complexity (continued)

–Multi-Step ADCs

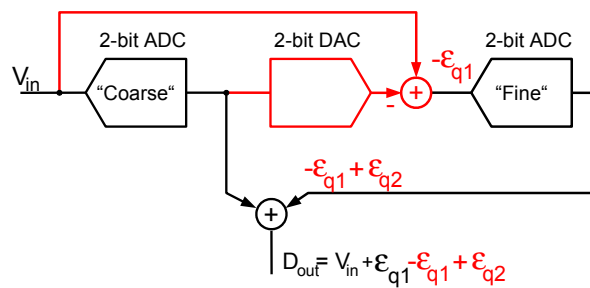
- Two-Step flash

- Pipelined ADCs

– Effect of sub-ADC, sub-DAC, gain stage non-idealities on overall ADC performance

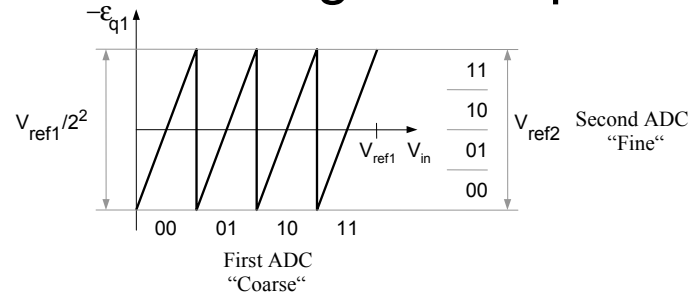
- Error correction by adding redundancy
- Digital calibration

Two Stage Example



- Use DAC to compute missing voltage
- Add quantized representation of missing voltage
- Why does this help? How about ϵ_{q2} ?

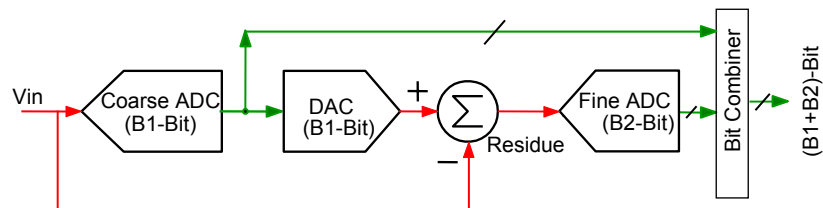
Two Stage Example



- Fine ADC is re-used 2^2 times
- Fine ADC's full scale range needs to span only 1 LSB of coarse quantizer

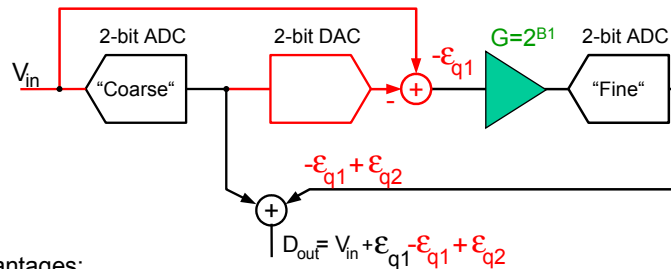
$$\epsilon_{q2} = \frac{V_{ref2}}{2^2} = \frac{V_{ref1}}{2^2 \cdot 2^2}$$

Residue or Multi-Step Type ADC Issues



- Operation:
 - Coarse ADC determines MSBs
 - DAC converts the coarse ADC output to analog- Residue is found by subtracting $(V_{in}-V_{DAC})$
 - Fine ADC converts the residue and determines the LSBs
 - Bits are combined in digital domain
- Issue:
 1. Fine ADC has to have precision in the order of overall ADC $1/2$ LSB
 2. Speed penalty \rightarrow Need at least 1 clock cycle per extra series stage to resolve one sample

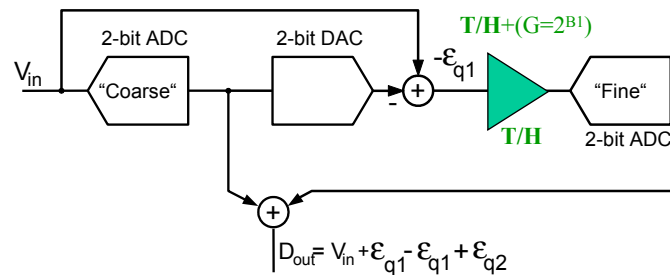
Solution to Issue (1) Reducing Precision Required for Fine ADC



Advantages:

- Accuracy needed for fine ADC relaxed by introducing inter-stage gain
 - Example: By adding gain of $x(G=2^{B1}=4)$ prior to fine ADC in (2+2)bit case, precision required for fine ADC is reduced from 4 to 2-bit only!
- Full-scale input same for both \rightarrow coarse and fine ADC can be identical stages
- Same reference voltage used for all stage w/o need for scaling down of V_{ref}

Solution to Issue (2) Increasing ADC Throughput

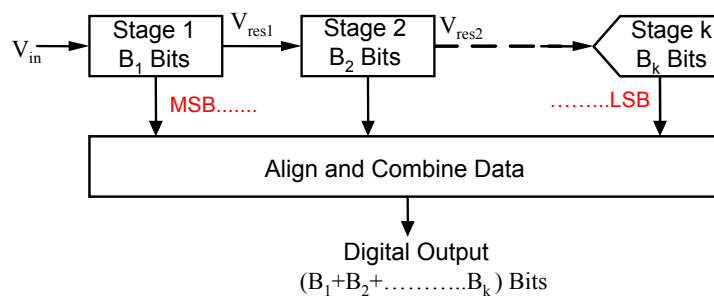


- Conversion time significantly decreased by employing T/H between stages
 - All stages busy at all times \rightarrow operation concurrent
 - During one clock cycle coarse & fine ADCs operate concurrently:
 - First stage samples/converts/generates residue of input signal sample # n
 - While 2nd stage samples/converts residue associated with sample # $n-1$

Pipelined A/D Converters

- Ideal operation
- Errors and correction
 - Redundancy
 - Digital calibration
- Implementation
 - Practical circuits
 - Stage scaling

Pipeline ADC Block Diagram

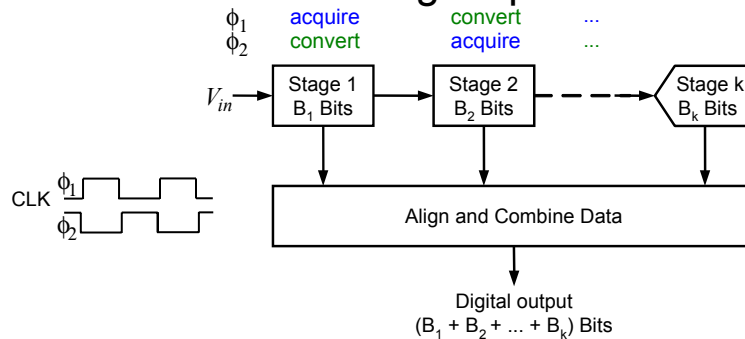


- Idea: Cascade several low resolution stages to obtain high overall resolution (e.g. 10bit ADC can be built with series of 10 ADCs each 1-bit only!)
- Each stage performs coarse A/D conversion and computes its quantization error, or "residue"
- All stages operate concurrently

Pipeline ADC Characteristics

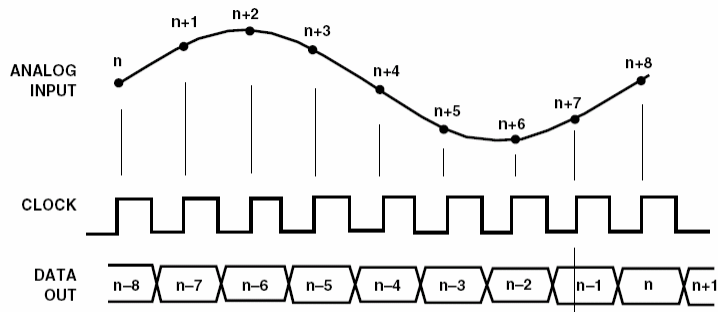
- Number of components (stages) grows linearly with resolution
- Pipelining
 - Trading latency for resolution
 - Latency may be an issue in e.g. control systems
 - Throughput limited by speed of one stage → Fast
- Versatile: 8...16bits, 1...200MS/s
- One important feature of pipeline ADC: many analog circuit non-idealities can be corrected digitally

Pipeline ADC Concurrent Stage Operation



- Stages operate on the input signal like a shift register
- New output data **every** clock cycle, but each stage introduces at least $\frac{1}{2}$ clock cycle latency

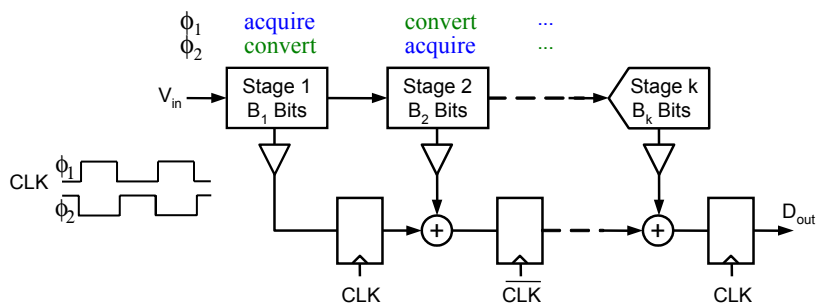
Pipeline ADC Latency



Note: One conversion per clock cycle & 8 clock cycle latency

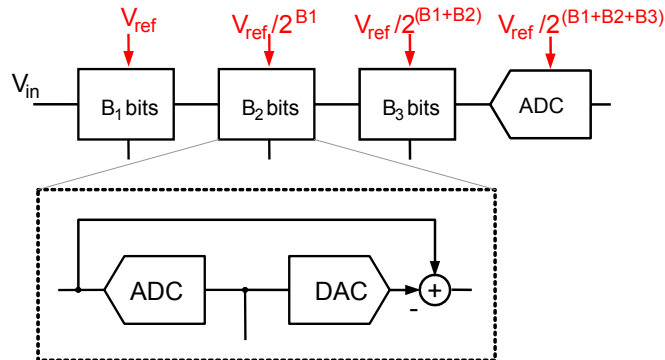
[Analog Devices, AD 9226 Data Sheet]

Pipeline ADC Digital Data Alignment



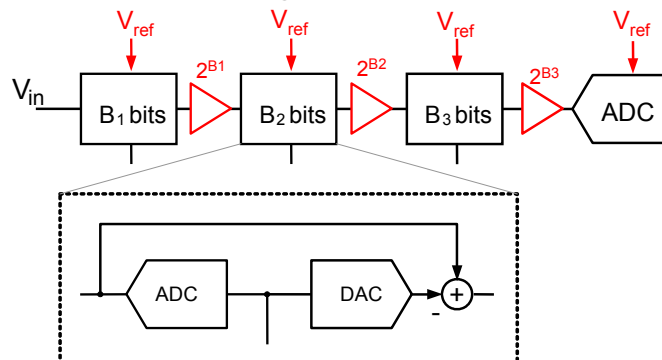
- Digital shift register aligns sub-conversion results in time

Cascading More Stages



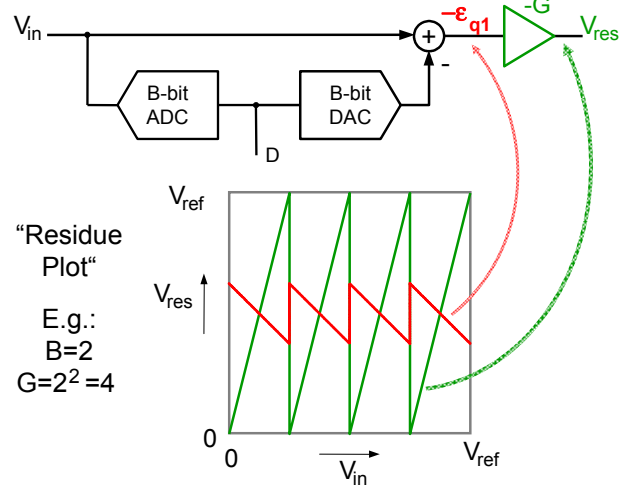
- LSB of last stage becomes very small
- Impractical to generate several V_{ref}
- All stages need to have full precision

Pipeline ADC Inter-Stage Gain Elements

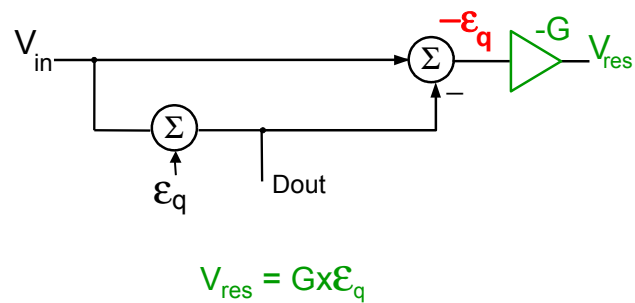


- Practical pipelines by adding inter-stage gain \rightarrow use single V_{ref}
- Precision requirements decrease down the pipe
 - Advantageous for noise, matching (later), power dissipation

Complete Pipeline Stage



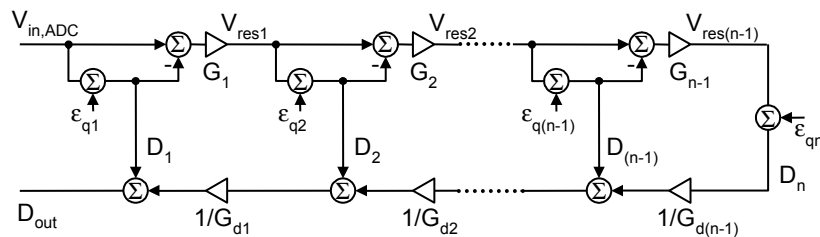
Pipeline ADC Single Stage Model



Pipeline ADC Errors

- Non-idealities associated with sub-ADCs, sub-DACs and gain stages → error in overall pipeline ADC performance
- Need to find means to tolerate/correct errors
- Important sources of error
 - Sub-ADC errors- comparator offset
 - Gain stage offset
 - Gain stage gain error
 - Sub-DAC error

Pipeline ADC Multi-Stage Model



$$D_{out} = V_{in,ADC} + \epsilon_{q1} \left(1 - \frac{G_1}{G_{d1}} \right) + \frac{\epsilon_{q2}}{G_{d1}} \left(1 - \frac{G_2}{G_{d2}} \right) + \dots + \frac{\epsilon_{q(n-1)}}{\prod_{j=1}^{n-2} G_{dj}} \left(1 - \frac{G_{(n-1)}}{G_{d(n-1)}} \right) + \frac{\epsilon_{qn}}{\prod_{j=1}^{n-1} G_{dj}}$$

Pipeline ADC Model

- If the "Analog" and "Digital" gain/loss is precisely matched:

$$D_{out} = V_{in,ADC} + \frac{\epsilon_{qn}}{\prod_{j=1}^{n-1} G_j}$$

$$D.R. = 20 \log \frac{\text{rms FS Signal}}{\text{rms Quant. Noise}} = 20 \log \frac{\frac{V_{ref}}{2\sqrt{2}}}{\frac{V_{ref}}{\sqrt{12} \times 2^{B_n} \prod_{j=1}^{n-1} G_j}} = 20 \log \left(\sqrt{\frac{3}{2}} \times 2^{B_n} \times \prod_{j=1}^{n-1} G_j \right)$$

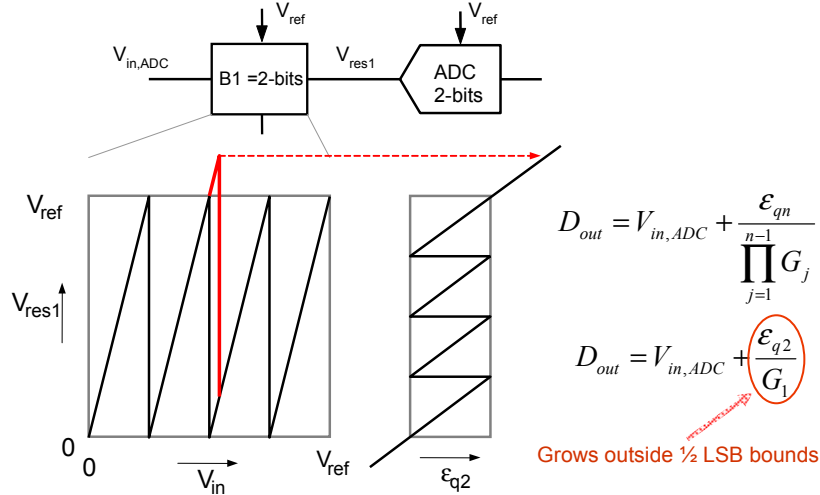
$$B_{ADC} \approx \log_2 \left(2^{B_n} \times \prod_{j=1}^{n-1} G_j \right)$$

$$B_{ADC} \approx B_n + \log_2 \prod_{j=1}^{n-1} G_j = B_n + \sum_{j=1}^{n-1} \log_2 G_j$$

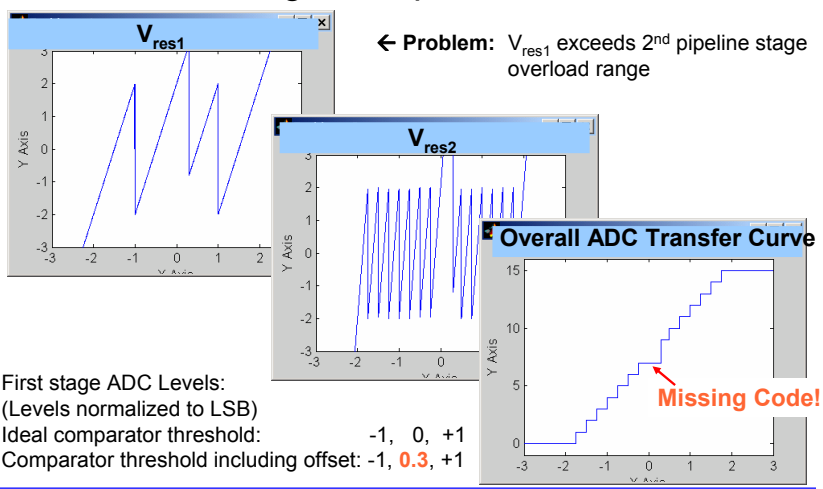
Pipeline ADC Observations

- The aggregate **ADC resolution is independent of sub-ADC resolution!**
- Effective* stage resolution $B_j = \log_2(G_j)$
- Overall conversion error does not (directly) depend on sub-ADC errors!**
- Only error term in D_{out} contains quantization error associated with the last stage
- So why do we care about sub-ADC errors?
 - Go back to two stage example

Pipeline ADC Sub-ADC Errors



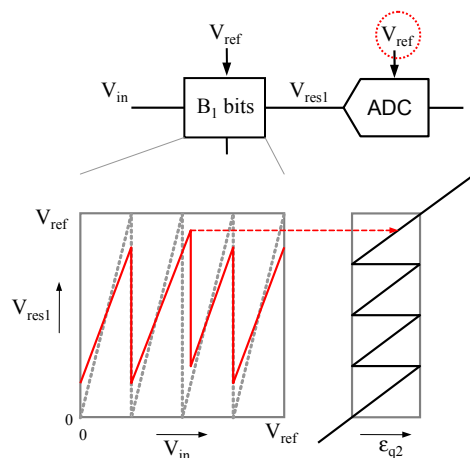
Pipeline ADC 1st-Stage Comparator Offset



Pipeline ADC Three Ways to Deal with Errors

- All involve "sub-ADC redundancy"
- Redundancy in stage that produces errors
 - Choose gain for residue to be processed by the 2nd stage $< 2^{B_1}$
 - Higher resolution sub-ADC & sub-DAC
- Redundancy in succeeding stage(s)

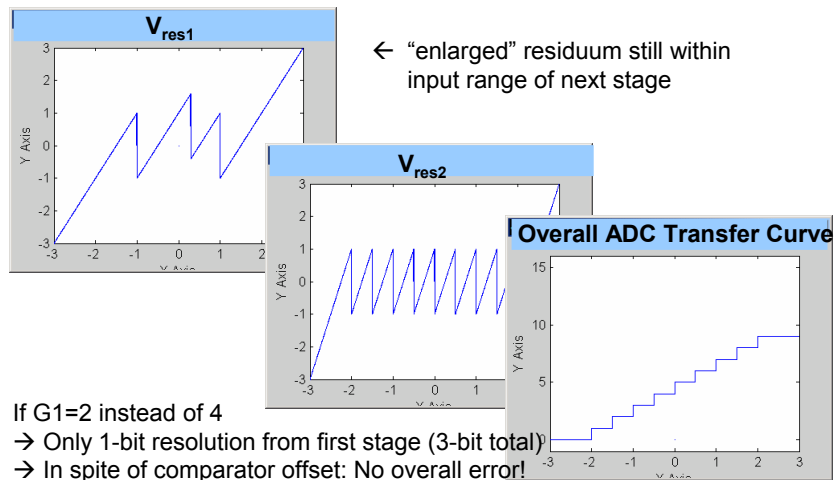
(1) Inter-Stage Gain Following 1st Stage $< 2^{B_1}$



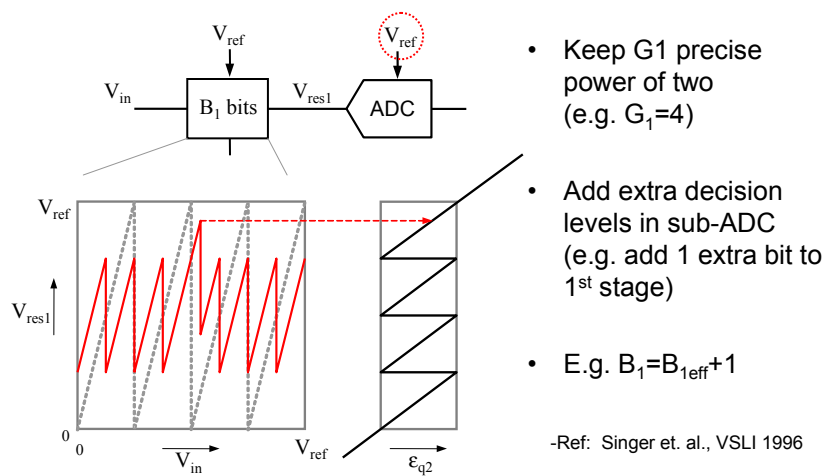
- Choose G_1 less than 2^{B_1}
- Effective stage resolution could become non-integer $B_{1eff} = \log_2 G_1$
- E.g. if $G_1 = 3.8 \rightarrow B_{1eff} = 1.8\text{bit}$

-Ref: A. Karanicolas et. al., JSSC 12/1993

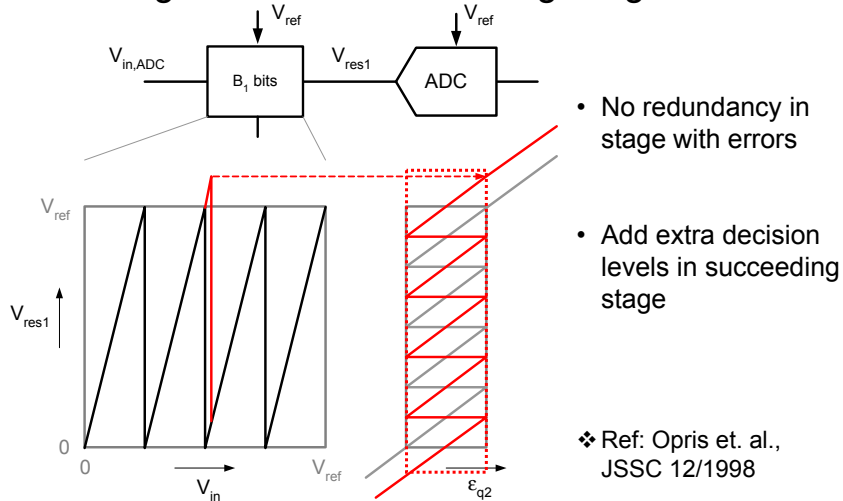
Correction Through Redundancy



(2) Higher Resolution Sub-ADC

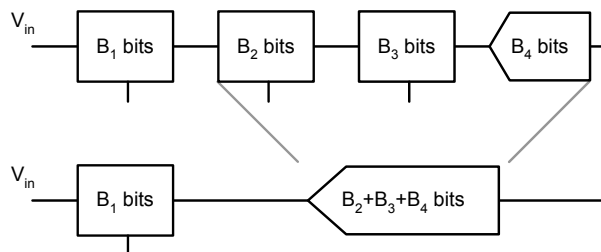


(3) Over-Range Accommodation Through Increase in Following Stage Resolution



Redundancy

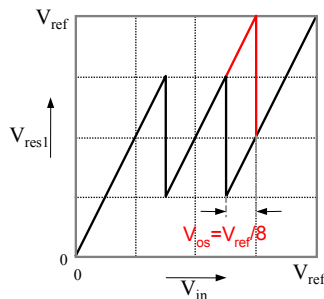
- The preceding analysis applies to any stage in an n-stage pipeline
- Can always perceive a multi-stage pipelined ADC as a single stage + backend ADC



Redundancy

- In literature, sub-ADC redundancy schemes are often called "digital correction" – a misnomer!
- No error correction takes place
- We can **tolerate** sub-ADC errors as long as:
 - The residues stay "within the box", or
 - Another stage downstream "returns the residue to "within the box" before it reaches last quantizer
- Let's calculate tolerable errors for popular "1.5 bits/stage" topology

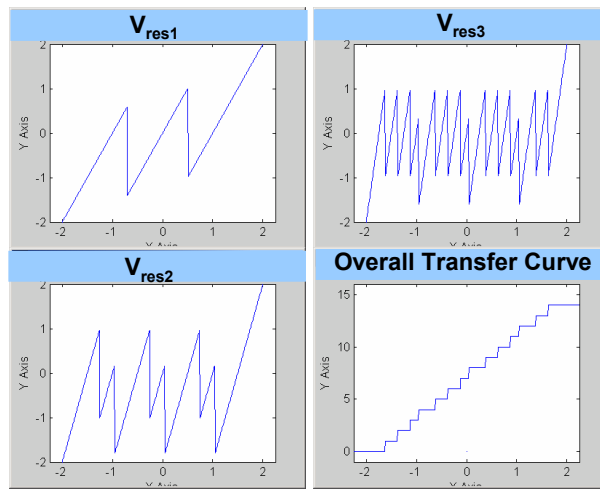
1.5 Bits/Stage Example



- Comparators placed strategically to minimize overhead
- $G=2$
- $B_{\text{eff}} = \log_2 G = \log_2 2 = 1$
- $B = \log_2(2+1) = 1.589\dots$
- 0.5bit \rightarrow redundancy

❖ Ref: Lewis et. al., JSSC 3/1992

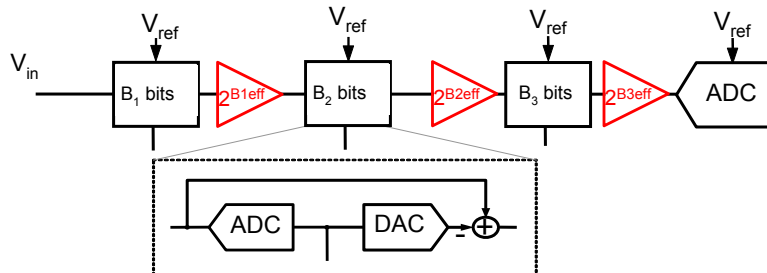
3-Stage 1.5-bit-per-Stage Pipelined ADC



- All three stages
→ Comparator with offset
- Overall transfer curve
 - No missing codes
 - Some DNL error

Ref: S. Lewis et al, "A 10-b 20-MS/s Analog-to-Digital Converter," J. Solid-State Circ., pp. 351-8, March 1992

Summary So Far Pipelined A/D Converters

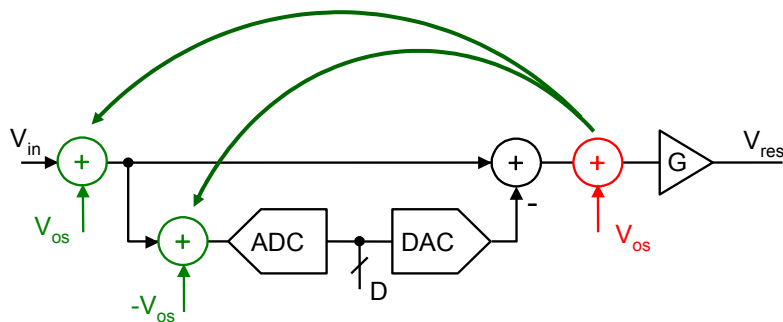


- Cascade of low resolution stages
 - Stages operate concurrently- trades latency for resolution
 - Throughput limited by speed of one stage → Fast
- Errors and correction
 - Built-in redundancy compensate for sub-ADC inaccuracies (interstage gain: $G=2^{B_{neff}}$, $B_{neff} < B_n$)

Pipeline ADC Errors

- Non-idealities associated with sub-ADCs, sub-DACs and gain stages → error in overall pipeline ADC performance
- Need to find means to tolerate/correct errors
- Important sources of error
 - Sub-ADC errors- comparator offset
 - Gain stage offset
 - Gain stage error
 - Sub-DAC error

Inter-Stage Amplifier Offset

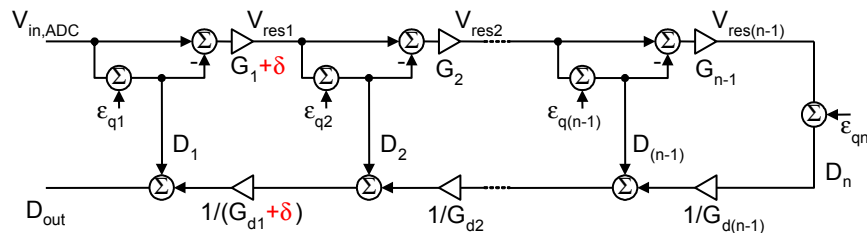


- Input referred converter offset – usually no problem
- Equivalent sub-ADC offset - accommodated through adequate redundancy

Pipeline ADC Errors

- Non-idealities associated with sub-ADCs, sub-DACs and gain stages → error in overall pipeline ADC performance
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 - Sub-DAC error

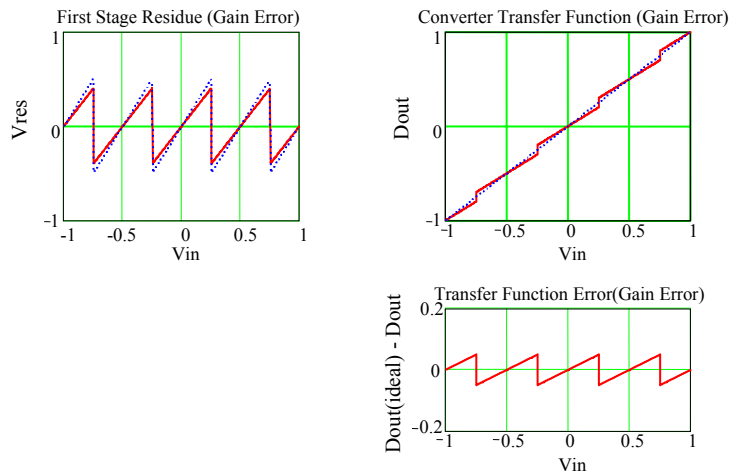
Gain Stage Gain Error



$$D_{out} = V_{in,ADC} + \epsilon_{q1} \left(1 - \frac{G_1 + \delta}{G_{d1} + \delta} \right) + \frac{\epsilon_{q2}}{G_{d1}} \left(1 - \frac{G_2}{G_{d2}} \right) + \dots + \frac{\epsilon_{q(n-1)}}{\prod_{j=1}^{n-2} G_{dj}} \left(1 - \frac{G_{(n-1)}}{G_{d(n-1)}} \right) + \frac{\epsilon_{qn}}{\prod_{j=1}^{n-1} G_{dj}}$$

→ Small amount of gain error can be tolerated

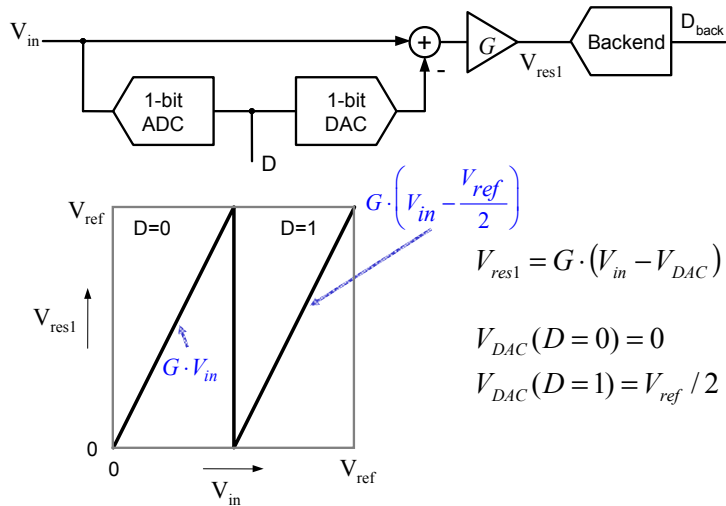
Interstage Gain Error



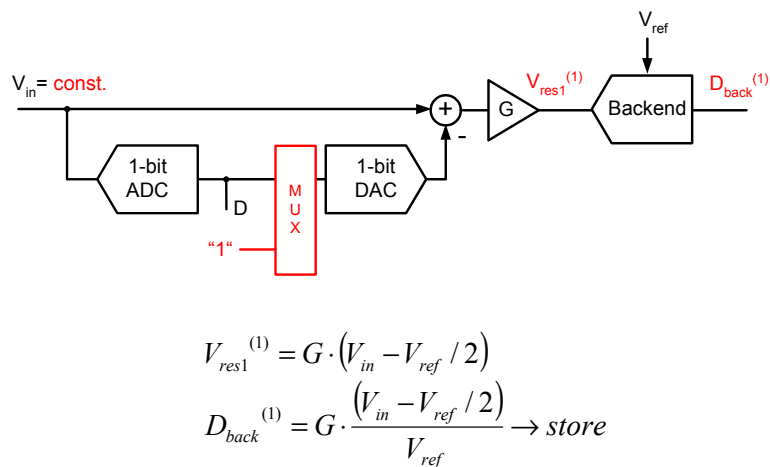
Gain Stage Gain Inaccuracy

- Gain error can be compensated in digital domain – "Digital Calibration"
- Problem: Need to measure/calibrate digital correction coefficient
- Example: Calibrate 1-bit first stage
- Objective: Measure G in digital domain

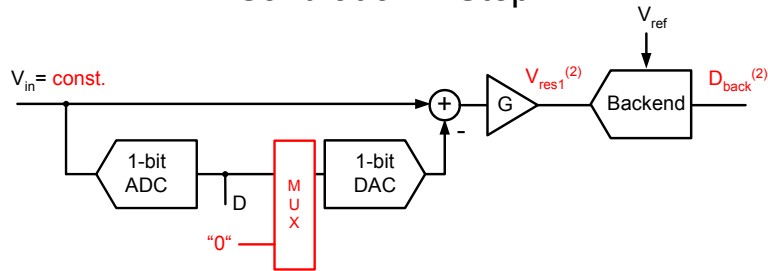
ADC Model



Gain Stage Inaccuracy Calibration – Step 1



Gain Stage Inaccuracy Calibration – Step 2



$$V_{res1}^{(2)} = G \cdot (V_{in} - 0)$$

$$D_{back}^{(2)} = G \cdot \frac{(V_{in} - 0)}{V_{ref}} \rightarrow \text{store}$$

Gain Stage Inaccuracy Calibration – Evaluate

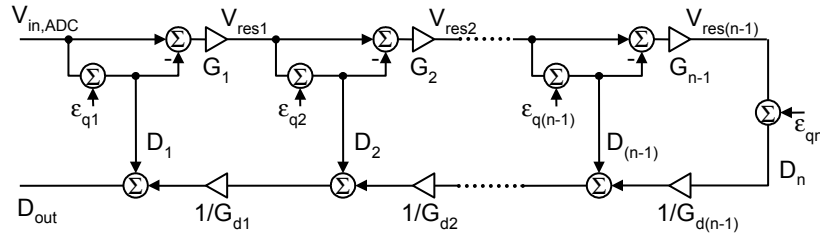
$$D_{back}^{(1)} = G \cdot \frac{(V_{in} - V_{ref} / 2)}{V_{ref}}$$

$$-D_{back}^{(2)} = G \cdot \frac{(V_{in} - 0)}{V_{ref}}$$

$$D_{back}^{(1)} - D_{back}^{(2)} = \frac{1}{2} \cdot G$$

- To minimize the effect of backend ADC noise → perform measurement several times and take the average

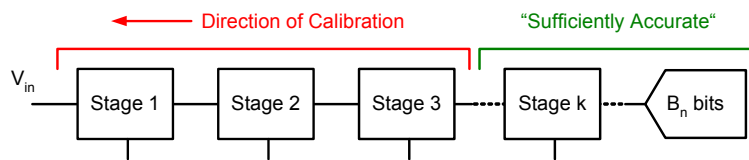
Accuracy Bootstrapping



$$D_{out} = V_{in,ADC} + \epsilon_{q1} \left(1 - \frac{G_1}{G_{d1}} \right) + \frac{\epsilon_{q2}}{G_{d1}} \left(1 - \frac{G_2}{G_{d2}} \right) + \dots + \frac{\epsilon_{q(n-1)}}{\prod_{j=1}^{n-2} G_{dj}} \left(1 - \frac{G_{(n-1)}}{G_{d(n-1)}} \right) + \frac{\epsilon_{qn}}{\prod_{j=1}^{n-1} G_{dj}}$$

- Highest sensitivity to gain errors in front-end stages

"Accuracy Bootstrapping"




Ref:

A. N. Karanicolas et al., "A 15-b 1-Msample/s digitally self-calibrated pipeline ADC," *IEEE J. Of Solid-State Circuits*, pp. 1207-15, Dec. 1993

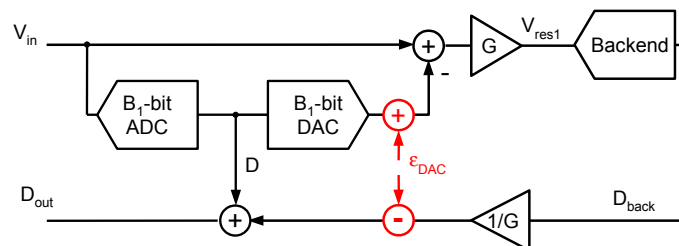
E. G. Soenen et al., "An architecture and an algorithm for fully digital correction of monolithic pipelined ADCs," *TCAS II*, pp. 143-153, March 1995

L. Singer et al., "A 12 b 65 MSample/s CMOS ADC with 82 dB SFDR at 120 MHz," *ISSCC 2000, Digest of Tech. Papers.*, pp. 38-9 (calibration in opposite direction!)

Pipeline ADC Errors

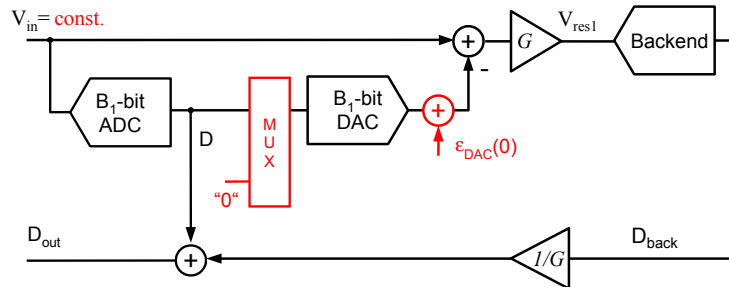
- Non-idealities associated with sub-ADCs, sub-DACs and gain stages \rightarrow error in overall pipeline ADC performance
- Need to find means to tolerate/correct errors
- Important sources of error
 - Sub-ADC errors- comparator offset
 - Gain stage offset
 - Gain stage error
 -  – Sub-DAC error

DAC Errors



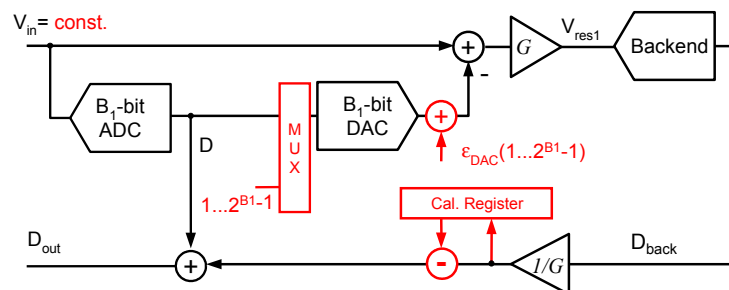
- Can be corrected digitally as well
- Same calibration concept as gain errors
 - \rightarrow Vary DAC codes & measure errors via backend ADC

DAC Calibration – Step 1



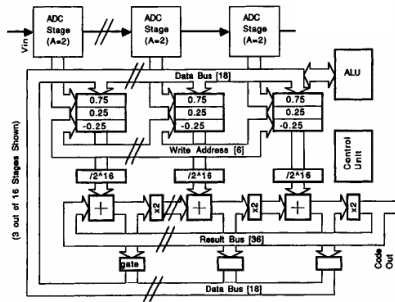
- $\epsilon_{DAC}(0)$ equivalent to amp. offset \rightarrow ignore

DAC Calibration – Step 2...2^{B1}



- Stepping through DAC codes $1 \dots 2^{(B_1-1)}$ yields all incremental correction values
- Measurements repeated and averages to account for variance associated with noise

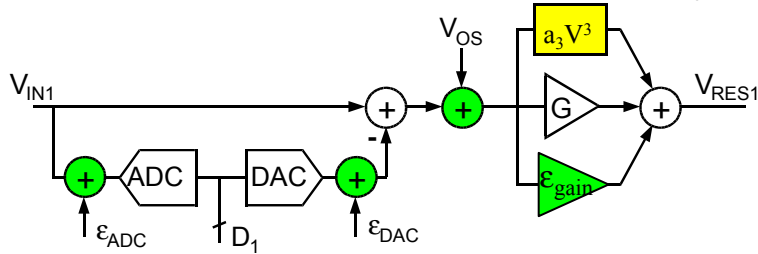
Pipeline ADC Example: Calibration Hardware



- Above block diagram may seem extensive however, in current fine-line CMOS technologies digital portion of a pipeline ADCs consume insignificant power and area compared to the analog sections

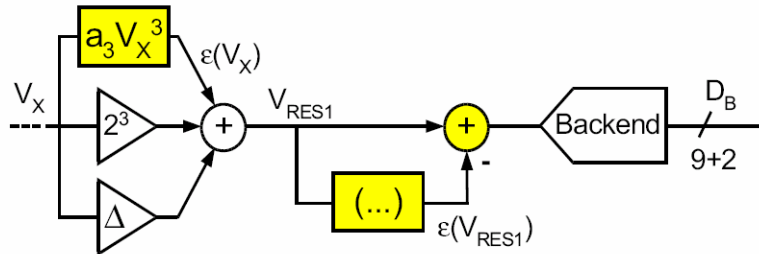
Ref: E. G. Soenen et al., "An architecture and an algorithm for fully digital correction of monolithic pipelined ADCs," TCAS II, pp. 143-153, March 1995

Pipelined ADC Error Correction/Calibration Summary



Error	Correction/Calibration
ϵ_{ADC}, V_{OS}	Redundancy either same stage or next stage
ϵ_{gain}	Digital adjustment
ϵ_{DAC}	Either sufficient component matching or digital calibration
Inter-stage amplifier non-linearity	?

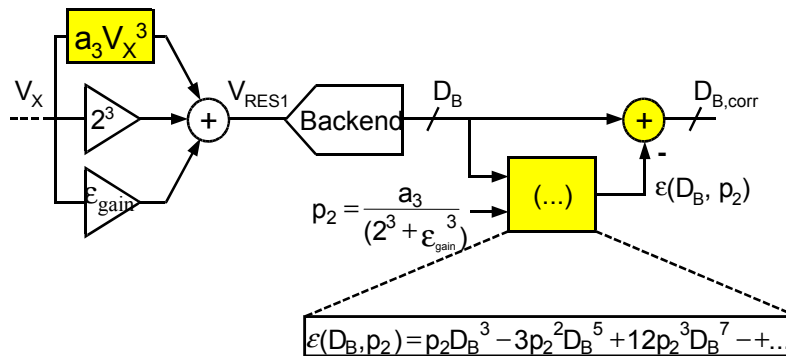
Inter-stage Gain Nonlinearity



- Invert gain stage non-linear polynomial
- Express error as function of V_{RES1}
- Push error into digital domain through backend

Ref: B. Murmann and B. E. Boser, "A 12-b, 75MS/s Pipelined ADC using Open-Loop Residue Amplification," *ISSCC Dig. Techn. Papers*, pp. 328-329, 2003

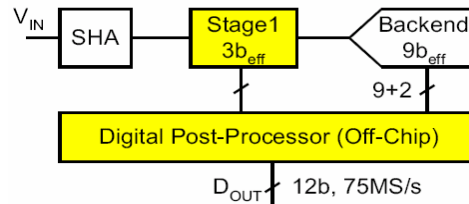
Inter-stage Gain Nonlinearity



- Pre-computed table look-up
- p_2 continuously estimated & updated (account for temp. & other variations)

Ref: B. Murmann and B. E. Boser, "A 12-b, 75MS/s Pipelined ADC using Open-Loop Residue Amplification," *ISSCC Dig. Techn. Papers*, pp. 328-329, 2003

Inter-stage Gain Nonlinearity Compensation Proof of Concept Evaluation Prototype



- Re-used 14-bit ADC in 0.35 μ m from Analog Devices [Kelly, ISSCC 2001]
- Modified only 1st stage with 3- b_{eff} \rightarrow open-loop amplifier built with simple diff-pair + resistive load instead of the conventional feedback around high-gain amp
- Conventional 9- b_{eff} backend, 2-bit redundancy in 1st stage
- Real-time post-processor off-chip (FPGA)

Ref: B. Murmann and B. E. Boser, "A 12-b, 75MS/s Pipelined ADC using Open-Loop Residue Amplification," *ISSCC Dig. Techn. Papers*, pp. 328-329, 2003

Measurement Results 12-bit ADC w Extra 2-bits for Calibration

