

EE247

Lecture 20

ADC Converters

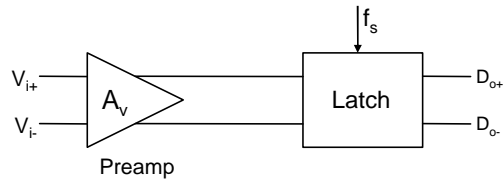
- Comparator architecture examples
- Flash ADC sources of error
 - Sparkle code
 - Meta-stability
- Techniques to reduce flash ADC complexity
 - Interpolating
 - Folding

Voltage Comparator Architectures

Comparator architectures

- High gain amplifier with differential analog input & single-ended large swing output
 - Output swing compatible with driving digital logic circuits
 - Open-loop amplification → no frequency compensation required
 - Precise gain not required
- Latched comparators; in response to a strobe, input stage disabled & digital output stored in a latch till next strobe
 - Two options for implementation :
 - High-gain amplifier + simple digital latch
 - Low-gain amplifier + a high-sensitivity latch
- Sample-data comparators
 - S/H input
 - Offset cancellation
 - Pipelined stages

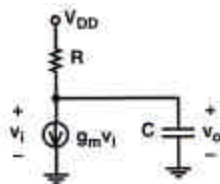
Latched Comparator



- Clock rate f_s
- Resolution
- Overload recovery
- Input capacitance (and linearity!)
- Power dissipation
- Input common-mode range
- Kickback noise
- ...

Comparators Overdrive Recovery

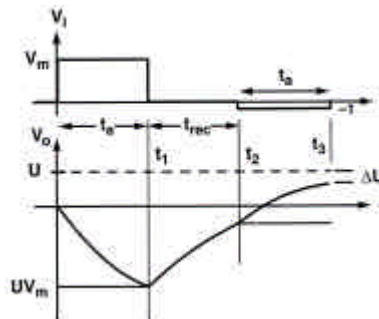
Linear model for a single-pole amplifier:



$U \rightarrow$ amplification after time t_a

During reset amplifier settles exponentially to its zero input condition with $\tau_0 = RC$

Assume $V_m \rightarrow$ maximum input normalized to $1/2lsb (=1)$

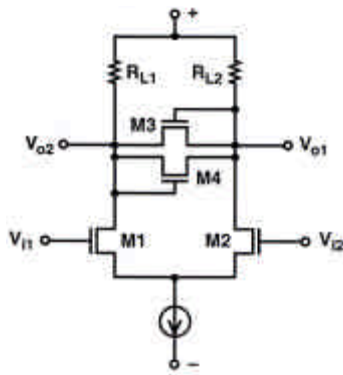


Example: Worst case input/output waveforms

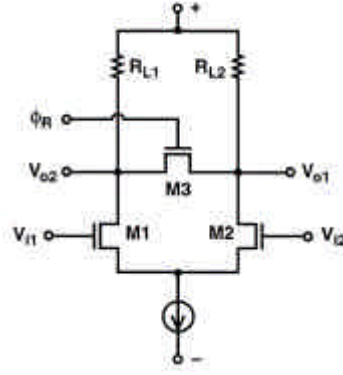
\rightarrow Limit output voltage swing by

1. Passive clamp
2. Active restore
3. Low gain/stage

Comparators Overdrive Recovery Limiting Output

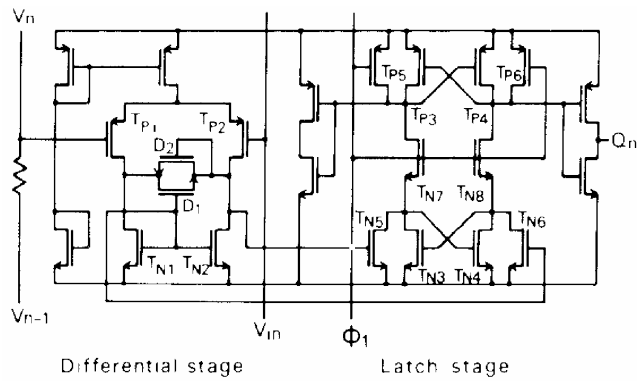


Clamp
Adds parasitic capacitance



Active Restore
After outputs are latched → Activate ϕ_R & equalize output nodes

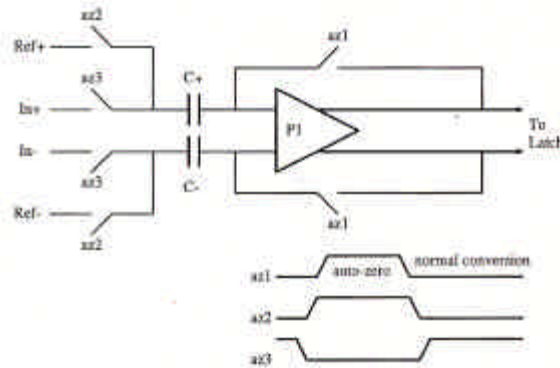
CMOS Comparator Example



- Flash ADC: 8bits, $\pm 1/2$ LSB INL @ $f_s=15\text{MHz}$ ($V_{ref}=3.8\text{V}$)
- No offset cancellation

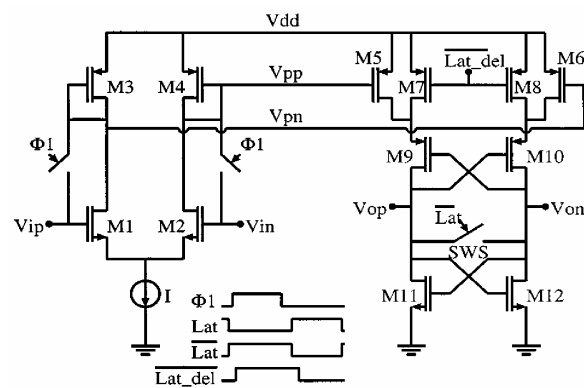
A. Yukawa, "A CMOS 8-Bit High-Speed A/D Converter IC," JSSC June 1985, pp. 775-9.

Comparator with Auto-Zero



I. Mehr and L. Singer, "A 500-Msample/s, 6-Bit Nyquist-Rate ADC for Disk-Drive Read-Channel Applications," JSSC July 1999, pp. 912-20.

Auto-Zero Implementation



Ref: I. Mehr and L. Singer, "A 55-mW, 10-bit, 40-Msample/s Nyquist-Rate CMOS ADC," JSSC March 2000, pp. 318-25.

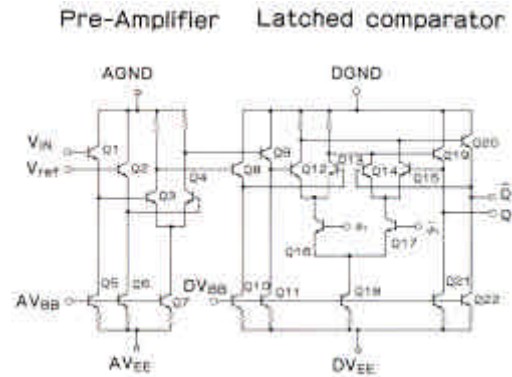
Bipolar Comparator Example

- Used in 8bit 400Ms/s & 6bit 2Gb/s flash ADC

- Signal amplification during ϕ_1 high, latch operates when ϕ_1 low

- Input buffers suppress kick-back & input current

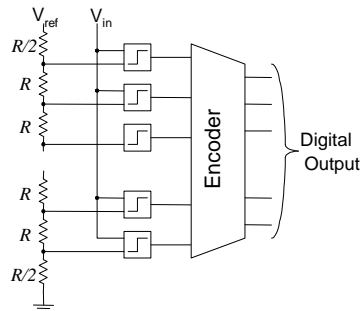
- Separate ground and supply buses for front-end preamp \rightarrow kick-back noise reduction



Ref: Y. Akazawa, et al., "A 400MSPS 8b flash AD conversion LSI," *IEEE International Solid-State Circuits Conference*, vol. XXX, pp. 98 - 99, February 1987.

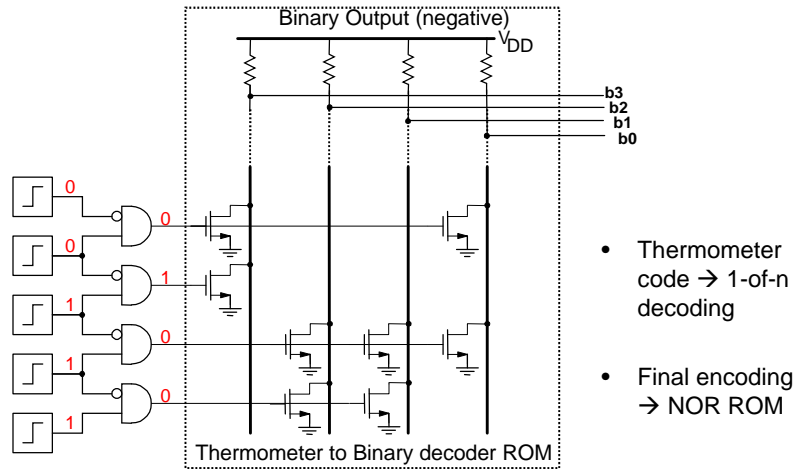
Ref: T. Wakimoto, et al., "Si bipolar 2GS/s 6b flash A/D conversion LSI," *IEEE International Solid-State Circuits Conference*, vol. XXXI, pp. 232 - 233, February 1988.

Flash Converter Sources of Error

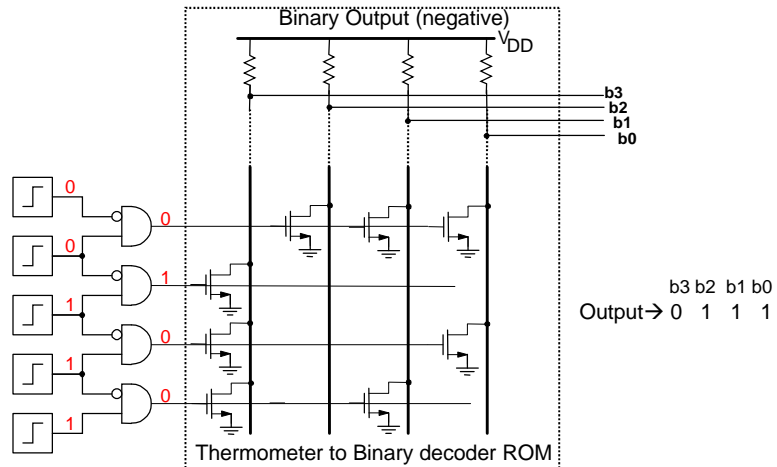


- Comparator input:
 - Offset
 - Nonlinear input capacitance
 - Kickback noise (disturbs reference)
 - Signal dependent sampling time
- Comparator output:
 - Sparkle codes (... 111101000 ...)
 - Metastability

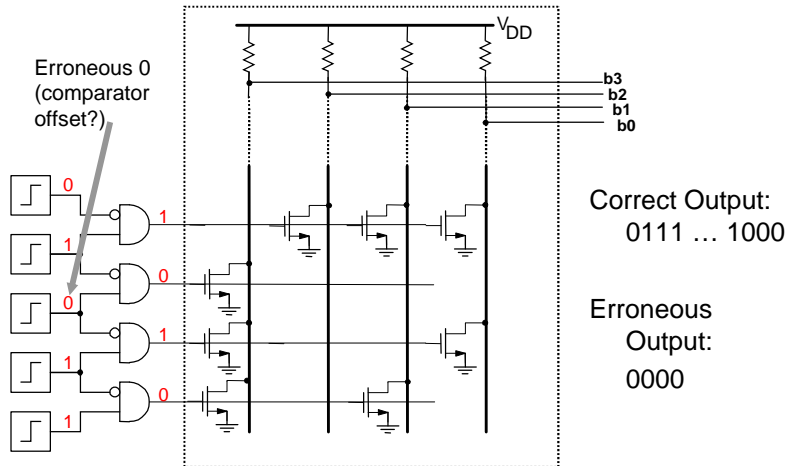
Typical Flash Output Encoder



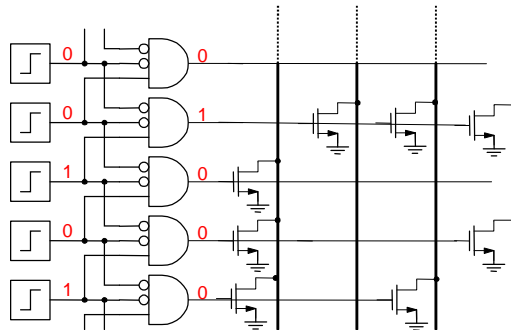
Typical Flash Output Decoder



Sparkle Codes



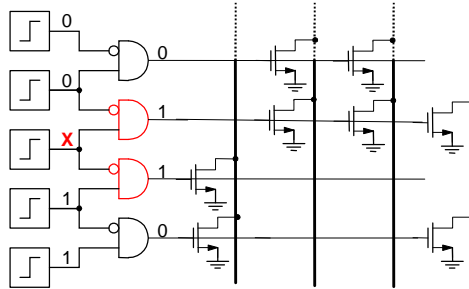
Sparkle Tolerant Encoder



Protects against a *single* sparkle.

Ref: C. Mangelsdorf et al, "A 400-MHz Flash Converter with Error Correction," JSSC February 1990, pp. 997-1002.

Meta-Stability



Different gates interpret metastable output X differently

Correct output: 0111 or 1000

Erroneous output: 0000

Solutions:

- Latches (high power)
- Gray encoding

Ref: C. Portmann and T. Meng, "Power-Efficient Metastability Error Reduction in CMOS Flash A/D Converters," JSSC August 1996, pp. 1132-40.

Gray Encoding

Thermometer Code							Gray			Binary		
T ₁	T ₂	T ₃	T ₄	T ₅	T ₆	T ₇	G ₃	G ₂	G ₁	B ₃	B ₂	B ₁
0	0	0	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	1	0	0	1
1	1	0	0	0	0	0	0	1	1	0	1	0
1	1	1	0	0	0	0	0	1	0	0	1	1
1	1	1	1	0	0	0	1	1	0	1	0	0
1	1	1	1	1	0	0	1	1	1	1	0	1
1	1	1	1	1	1	0	1	0	1	1	1	0
1	1	1	1	1	1	1	1	0	0	1	1	1

$$G_1 = T_1 \overline{T_3} + T_5 \overline{T_7}$$

$$G_2 = T_2 \overline{T_6}$$

$$G_3 = T_4$$

- Each T_i affects only one G_i
→ Avoids disagreement of interpretation by multiple gates
- Protects also against sparkles
- Follow Gray encoder by (latch and) binary encoder

Reducing Flash ADC Complexity

E.g. 10-bit “straight” flash

- Input range: 0 ... 1V
- LSB = Δ : ~ 1mV
- Comparators: 1023 with offset \ll LSB
- Input capacitance: $1023 * 100\text{fF} = 102\text{pF}$
- Power: $1023 * 3\text{mW} = 3\text{W}$

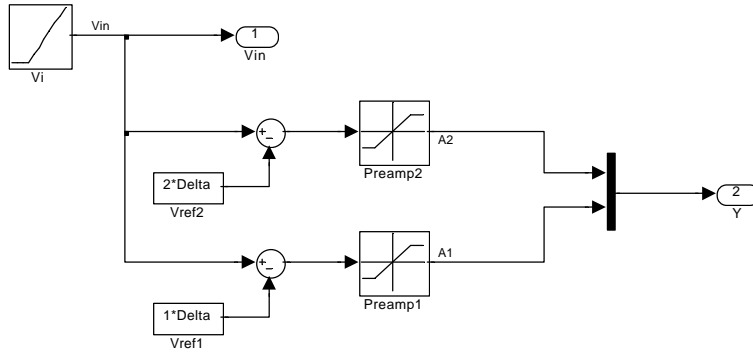
Techniques:

- Interpolation
- Folding
- Folding & Interpolation
- Two-step, pipelining

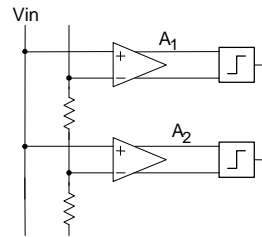
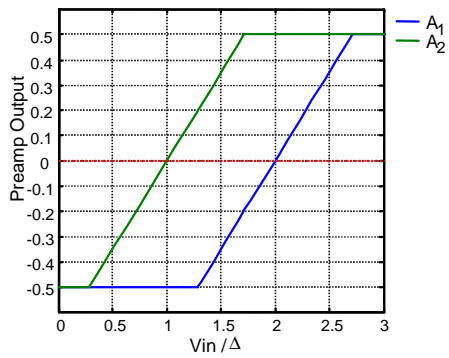
Interpolation

- Idea
 - Interpolation between preamp outputs
- Reduces number of preamps
 - Reduced input capacitance
 - Reduced area, power dissipation
- Same number of latches
- Important “side-benefit”
 - Decreased sensitivity to preamp offset
 - improved DNL

Simulink Model



Preamp Output

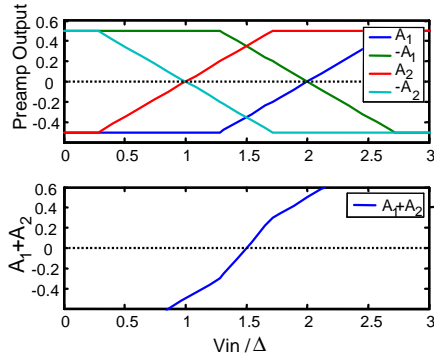


Zero crossings (to be detected by latches) at $V_{in} =$

$$V_{ref1} = 1 \Delta$$

$$V_{ref2} = 2 \Delta$$

Differential Preamp Output



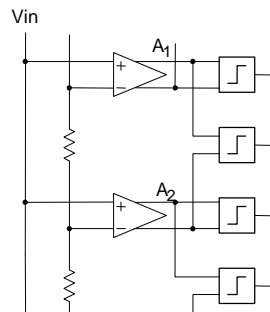
Zero crossings at $V_{in} =$

$$V_{ref1} = 1 \Delta$$

$$V_{ref12} = 0.5 * (1+2) \Delta$$

$$V_{ref2} = 2 \Delta$$

Interpolation in Flash ADC



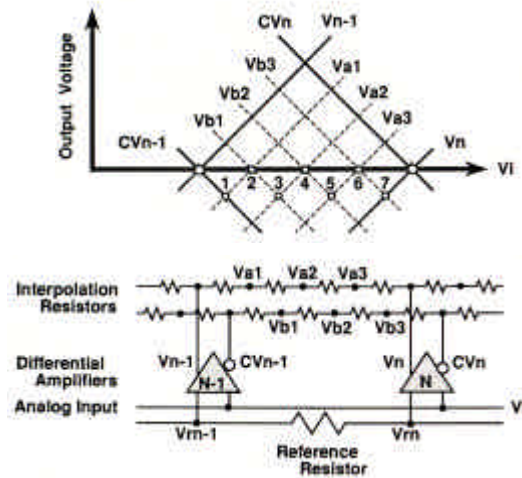
Half as many reference voltages and preamps

Interpolation factor: x2

Possible to accomplish higher interpolation factor

→ Resistive interpolation

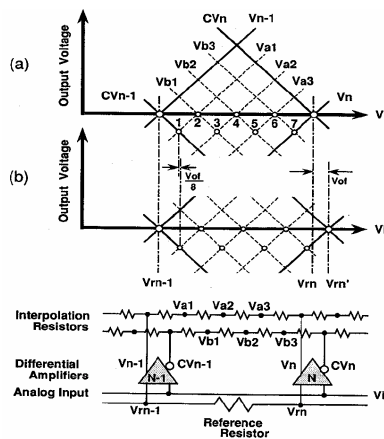
Resistive Interpolation



- Resistors produce additional levels
- With 4 resistors, the “interpolation factor” $M=8$ (ratio of latches/preamps)

Ref: H. Kimura et al, “A 10-b 300-MHz Interpolated-Parallel A/D Converter,” JSSC April 1993, pp. 438-446.

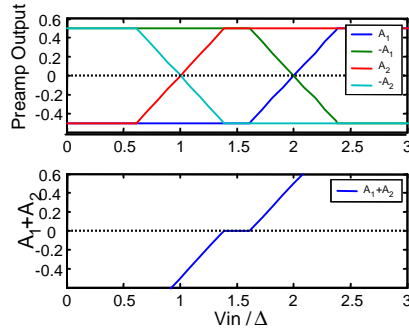
DNL Improvement



- Preamp offset distributed over M resistively interpolated voltages:
→ impact on DNL divided by M
- Latch offset divided by gain of preamp
→ use “large” preamp gain ...

Ref: H. Kimura et al, “A 10-b 300-MHz Interpolated-Parallel A/D Converter,” JSSC April 1993, pp. 438-446.

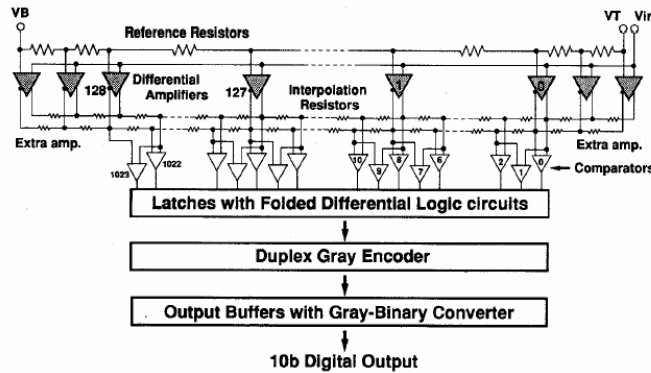
Preamp Input Range



Linear preamp input ranges must overlap
i.e. range > Δ

Sets upper bound on gain
 $\ll V_{DD} / \Delta$

Interpolated-Parallel ADC



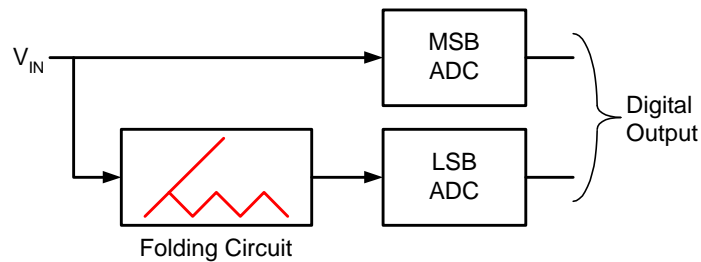
Ref: H. Kimura et al, "A 10-b 300-MHz Interpolated-Parallel A/D Converter," JSSC April 1993, pp. 438-446.

Measured Performance

Resolution		10 b (7+3)
Maximum conversion frequency		300 MHz
Integral non-linearity		± 1.0 LSB
Differential non-linearity		± 0.4 LSB
SNR/THD	10MHz input	56/-59 dB
	50MHz input	48/-47 dB
Input capacitance		8 pF
Input range		2 V
Power supply		-5.2V
Power dissipation		4.0W
Chip size		9.0×4.2 mm²
Element count		36,000
Technology		1.0 μm bipolar:ft=25GHz

Ref: H. Kimura et al, "A 10-b 300-MHz Interpolated-Parallel A/D Converter," JSSC April 1993, pp. 438-446.

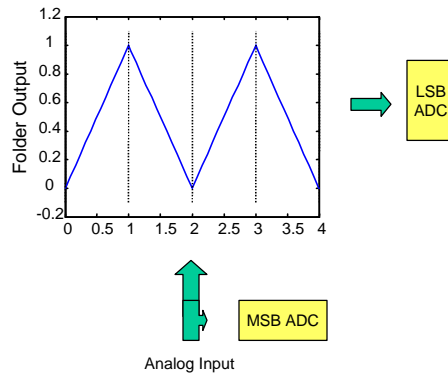
Folding Converter



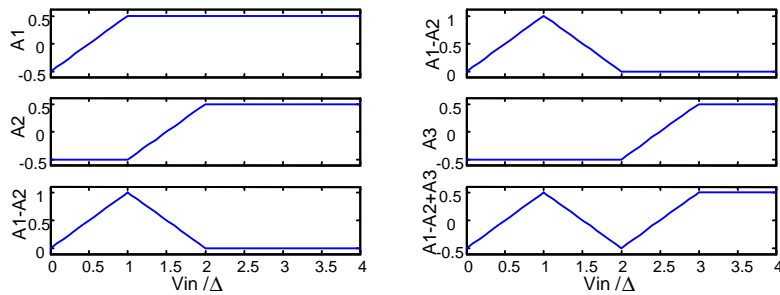
- Significantly fewer comparators than flash $\sim 2^{B/2+1}$
- Fast
- Nonidealities in folder limit resolution to ~ 10 Bits

Folding

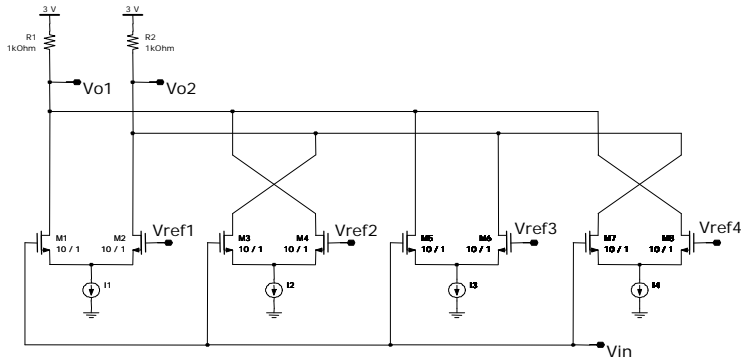
- Folder maps input to smaller range
- MSB ADC determines which fold input is in
- LSB ADC determines position within fold
- Logic circuit combines LSB and MSB results



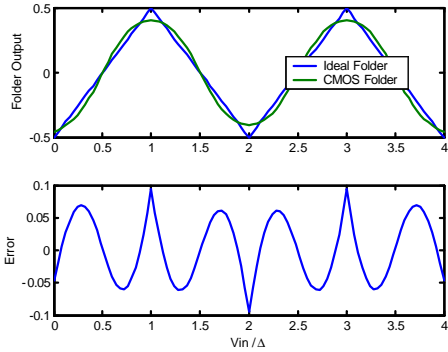
Generating Folds



Folding Circuit



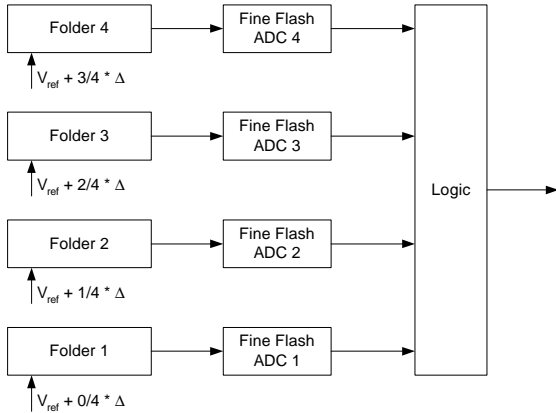
CMOS Folder Output



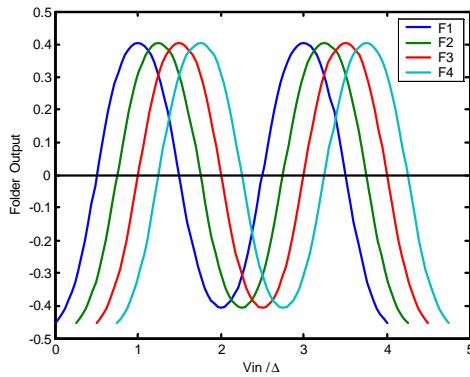
Accurate only at zero-crossings

Lowdown →
Most folding ADCs do not actually use the folds, but only the zero-crossings!

Parallel Folders



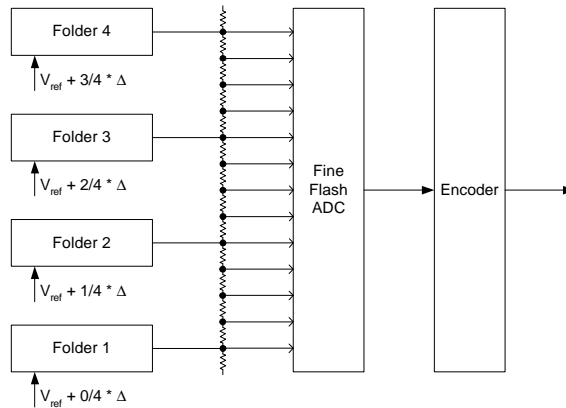
Parallel Folder Outputs



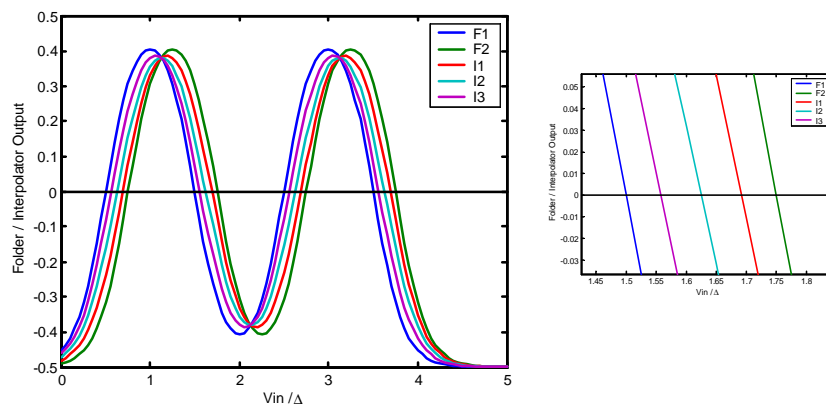
- 4 Folders
- 16 Zero crossings
- → only 4 LSB bits

- Better resolution
 - More folders → Large complexity
 - Interpolation

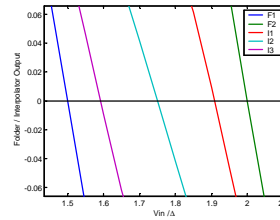
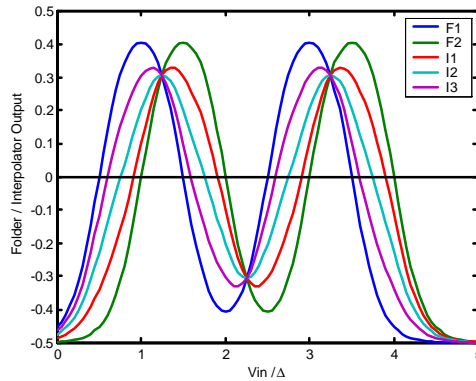
Folding & Interpolation



Folder / Interpolator Output

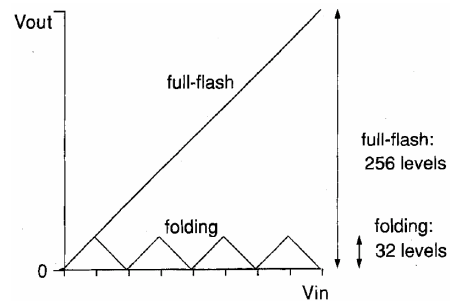
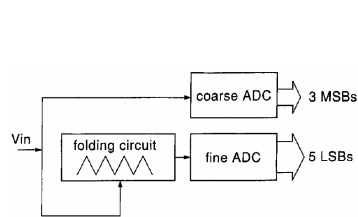


Folder / Interpolator Output

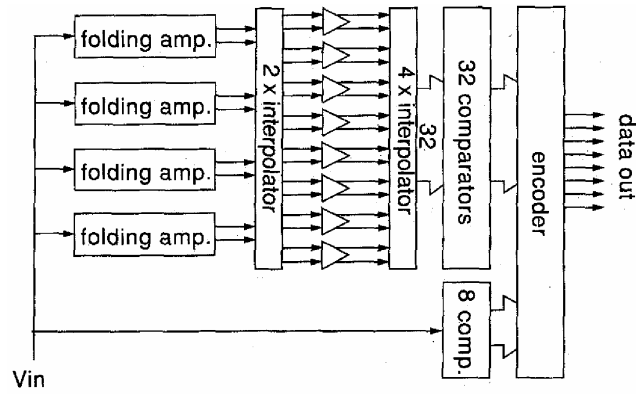


Interpolate only between closely spaced folds to avoid nonlinear distortion

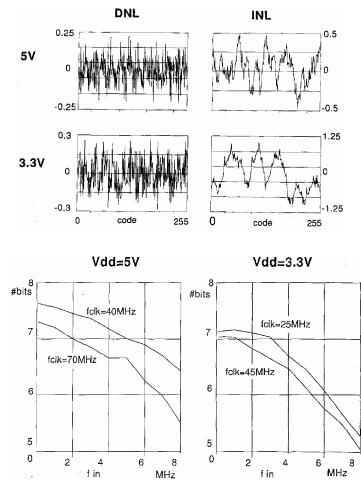
A 70-MS/s 110-mW 8-b CMOS Folding and Interpolating A/D Converter



A 70-MS/s 110-mW 8-b CMOS Folding and Interpolating A/D Converter



A 70-MS/s 110-mW 8-b CMOS Folding and Interpolating A/D Converter



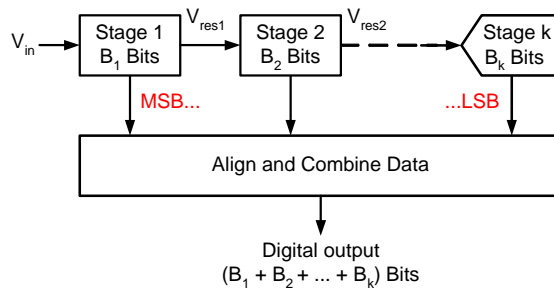
parameter	
resolution	8bit
input capacitance	4.8 pF
reference ladder resistance	720 Ω
active area	0.7 mm ²
technology	0.8 μ m, 1 poly, 2 metal, CMOS
supply voltage	$V_{dd}=5V$ $V_{dd}=3.3V$
analog input	2V _{pp} 1.4V _{pp}
Integral nonlinearity	$\pm 0.5LSB$ $\pm 1.0LSB$
Differential nonlinearity	$\pm 0.2LSB$ $\pm 0.3LSB$
max. clock frequency	70MHz 45MHz
power dissipation	110mW 45mW

Pipelined ADCs

Pipelined A/D Converters

- Ideal Operation
- Errors and Correction
 - Redundancy
 - Digital Calibration
- Implementation
 - Practical Circuits
 - Stage Scaling

Block Diagram

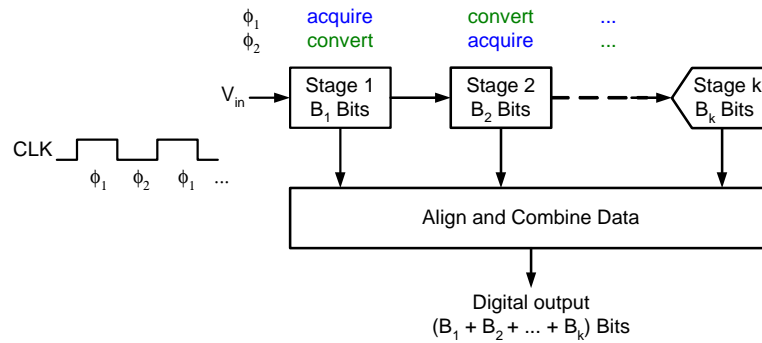


- Idea: Cascade several low resolution stages to obtain high overall resolution
- Each stage performs coarse A/D conversion and computes its quantization error, or "residue"

Characteristics

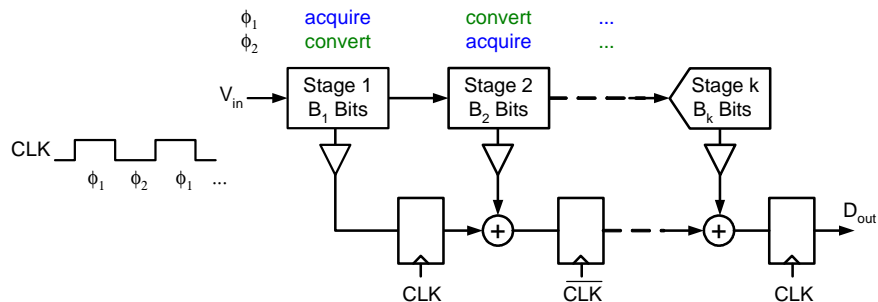
- Number of components (stages) grows linearly with resolution
- Pipelining
 - Trading latency for conversion speed
 - Latency may be an issue in e.g. control systems
 - Throughput limited by speed of one stage ® Fast
- Versatile: 8...16bits, 1...200MS/s
- Many analog circuit non-idealities can be corrected digitally

Concurrent Stage Operation



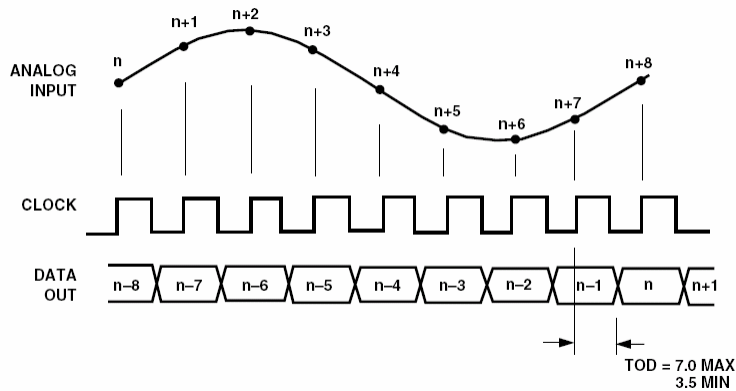
- Stages operate on the input signal like a shift register
- New output data every clock cycle, but each stage introduces $\frac{1}{2}$ clock cycle latency

Data Alignment



- Digital shift register aligns sub-conversion results in time

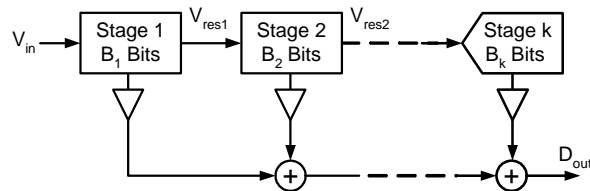
Latency



[Analog Devices, AD 9226 Data Sheet]

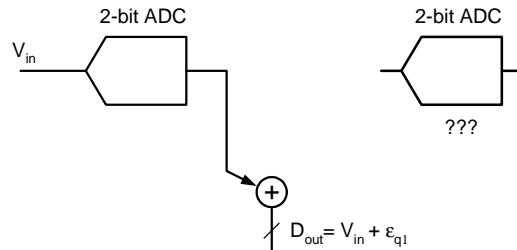
Pipelined ADC Analysis

- Ignore timing and use simple static model



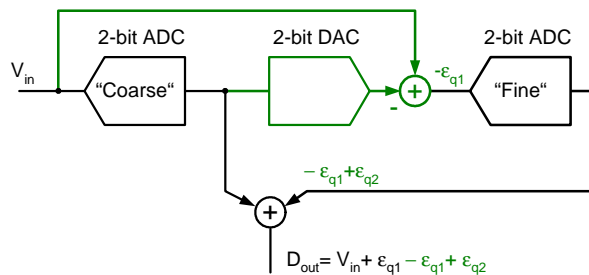
- Let's first look at "two-stage pipeline"
 - E.g.: Two cascaded 2-bit ADCs to get 4 bits of total resolution

Two Stage Example



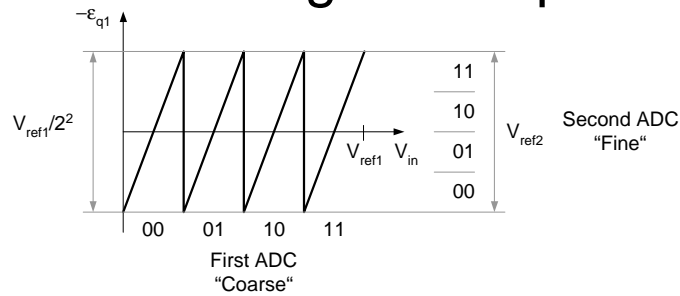
- Using only one ADC: Output contains large quantization error
- "Missing voltage" or "residue" ($-\epsilon_{q1}$)
- Idea: Use second ADC to quantize and add $-\epsilon_{q1}$

Two Stage Example



- Use DAC to compute missing voltage
- Add quantized representation of missing voltage
- Why does this help? How about ϵ_{q2} ?

Two Stage Example



- Fine ADC is re-used 2^2 times
- Fine ADC's full scale range needs to span only 1 LSB of coarse quantizer

$$e_{q2} = \frac{V_{ref2}}{2^2} = \frac{V_{ref1}}{2^2 \cdot 2^2}$$

Two Stage Transfer Function

