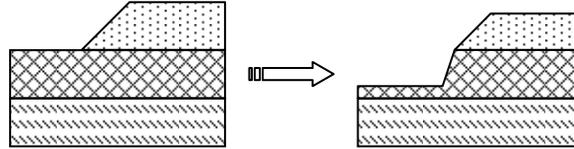


**I: Surface micromachining: partial list of issues**

Pay attention to all of these issues when you do homework 3 – some of them will be very important. But you should already be familiar with most of them from homework 2.

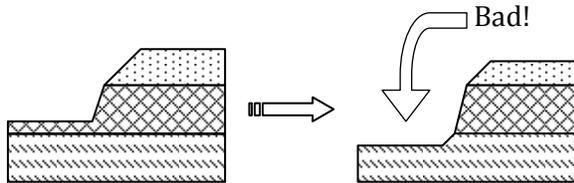
**1. Sidewall slope**

An anisotropic etch transfers the sidewall slope of the masking layer (such as photoresist) to the underlying layer. Because the etch progresses linearly in time, we know that a straight-line profile in the masking layer will cause a straight-line profile in the underlying layer.



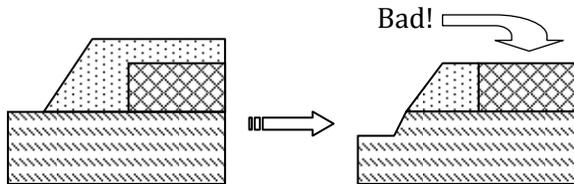
**2. Finite selectivity and overetch**

Because our film thicknesses and etch rates vary, we always overetch to guarantee that we've removed the entire film. But then we start etching the underlying film!



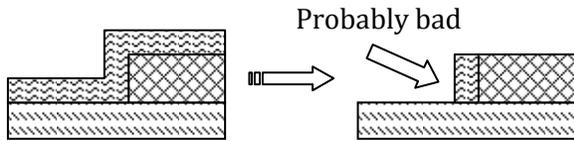
**3. Photoresist too thin**

Photoresist needs to be thick enough to withstand the etch, even over raised topography.



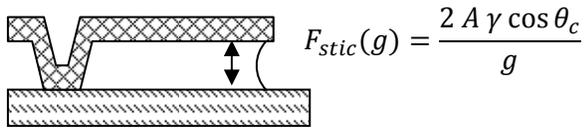
**4. Stringers**

Film "thickness" (from the standpoint of an anisotropic etch) increases when the film goes over a step in topography.



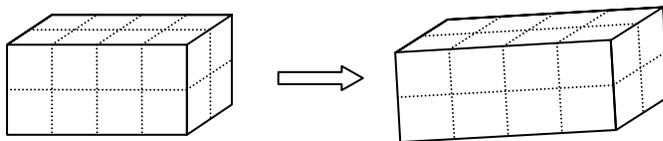
**5. Stiction**

Stiction occurs when the elastic restoring force cannot overcome the (nonlinear) stiction force at any point during the drying process.



**6. Residual stress (uniform and gradient)...**

**II: Elasticity**



Displacement:  $\vec{u}(\vec{x})$

Strain:  $\vec{\epsilon}(\vec{x}) = \frac{d\vec{u}}{d\vec{x}} = \begin{pmatrix} \epsilon_x & \gamma_{xy} & \gamma_{xz} \\ \gamma_{yx} & \epsilon_y & \gamma_{yz} \\ \gamma_{zx} & \gamma_{zy} & \epsilon_z \end{pmatrix}$

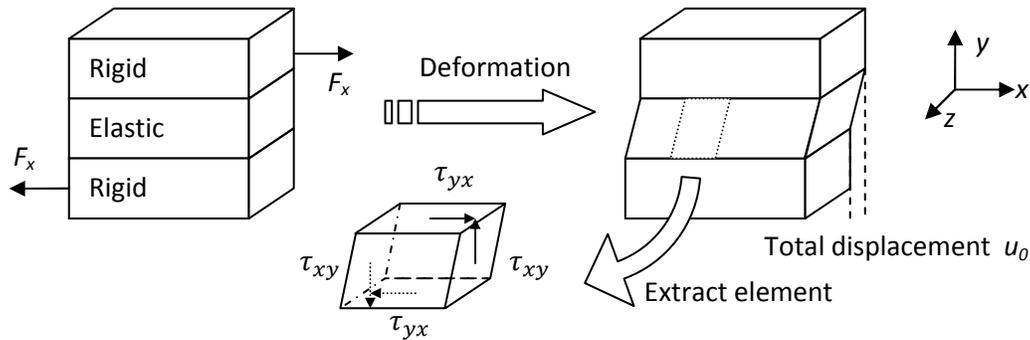
Stress:  $\vec{\Sigma}(\vec{x}) = \begin{pmatrix} \sigma_x & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_y & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_z \end{pmatrix}$

Can conceptualize strain this way: take a block of material, paint lines on it, and then deform it.

Displacement: how far a particular line moves

Strain: how far a particular line moves, relative to the lines next to it.

### 1. Simple example: "sandwich" of three blocks



Consider a block of elastic material sandwiched between two blocks of "rigid" material (much greater shear modulus). Apply a shear force  $F_x$  to the two rigid blocks. The elastic block experiences a uniform shear stress:

$$\tau_{yx} = \frac{F_x}{A}$$

The subscript  $y$  denotes that the stress occurs on a plane normal to the  $y$ -direction, and the subscript  $x$  denotes that the stress itself is in the  $x$ -direction.

Now consider a small element of the elastic material. In order for the element to be in static equilibrium (no acceleration), two conditions must hold:

$$\begin{aligned} \Sigma F_x &= 0 \\ \Sigma M_z &= 0 \end{aligned}$$

The zero-force condition requires equal and opposite stresses on the top and bottom faces ( $y$ -normal).

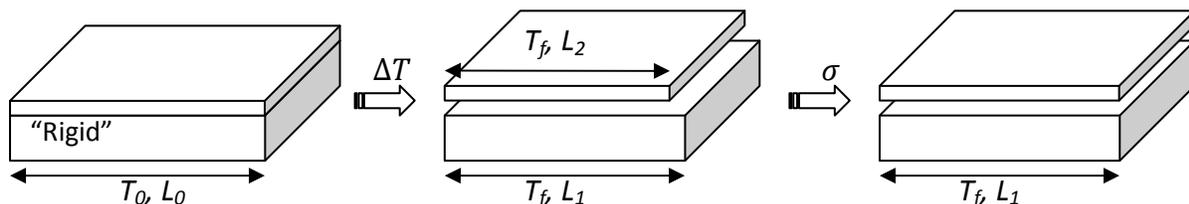
The zero-moment condition requires counterbalancing stresses on the left and right faces ( $x$ -normal):

$$\tau_{xy} = \tau_{yx}$$

(What's wrong with the sketch of the three blocks?)

### 2. Trickier example: mismatched thermal expansion (as seen in lecture)

Can analyze this situation by superposing two effects: thermal expansion and elasticity



Two blocks of material have the same size at temperature  $T_0$ .

Change temperature. Find the size that the blocks would have if they were not attached together. (Thermal strain only; zero stress).

Find the stress necessary to force the thin film to have the same size as the rigid substrate. This is the thermal stress.