

Photolithography

Key Topics:

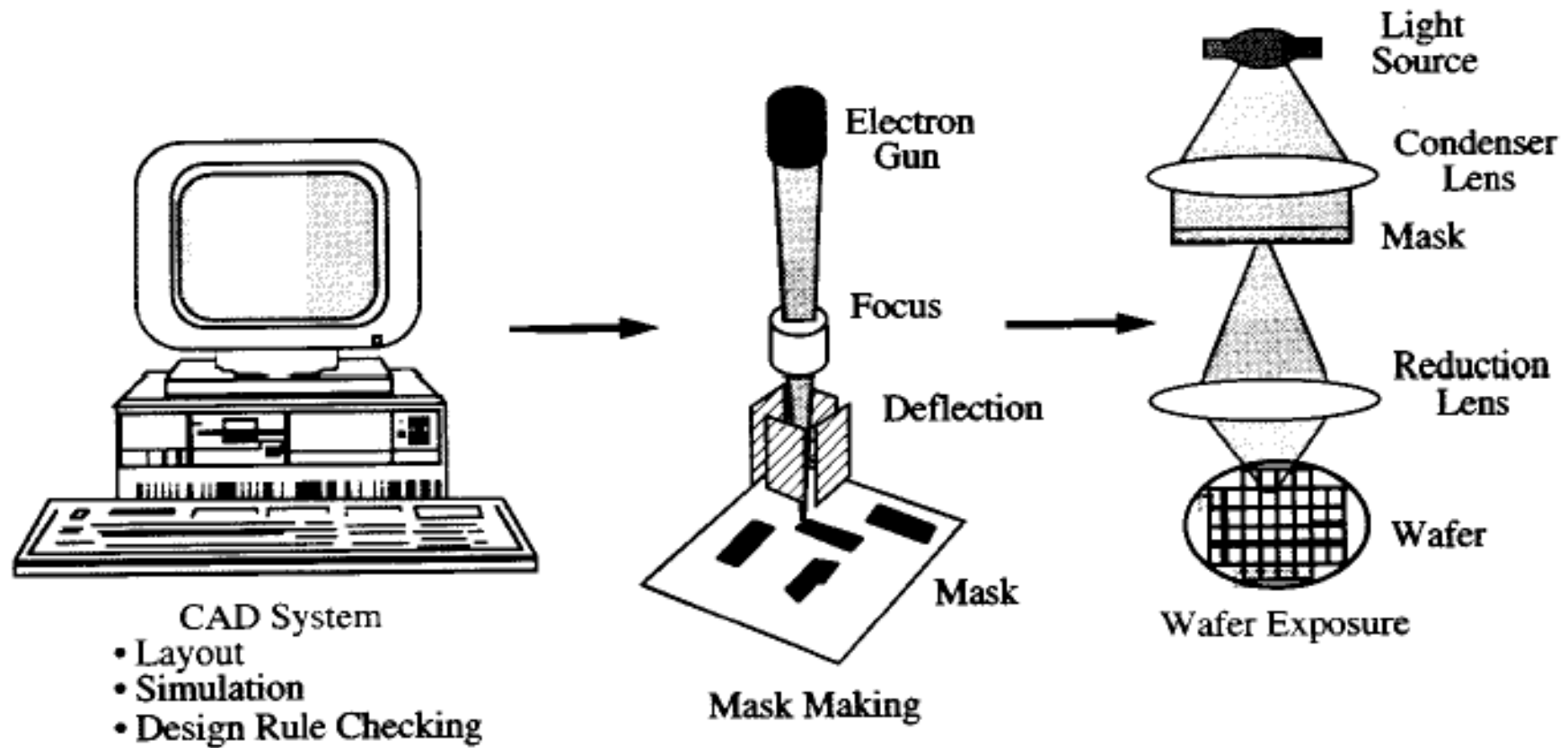
- Resolution
- Depth of Focus
- Overlay Errors
- Photoresist Response
- E-beam and X-ray lithography

Photo = $\phi\omega s$ = (through) light

Litho = $\lambda\iota\theta\omicron s$ = stone

Graphy = $\gamma\rho\alpha\phi\eta$ = writing

Design \Rightarrow Mask \Rightarrow Wafer



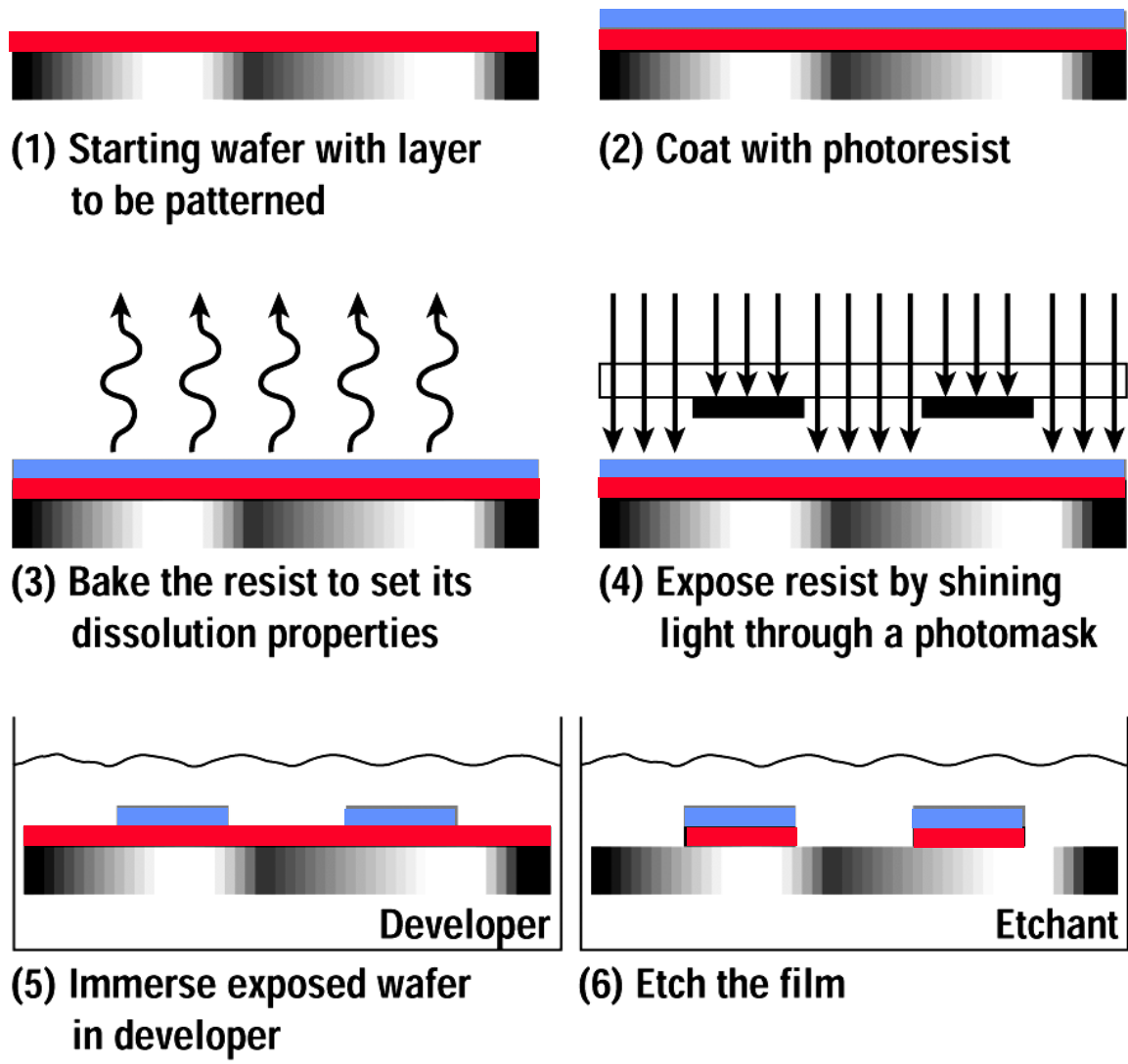
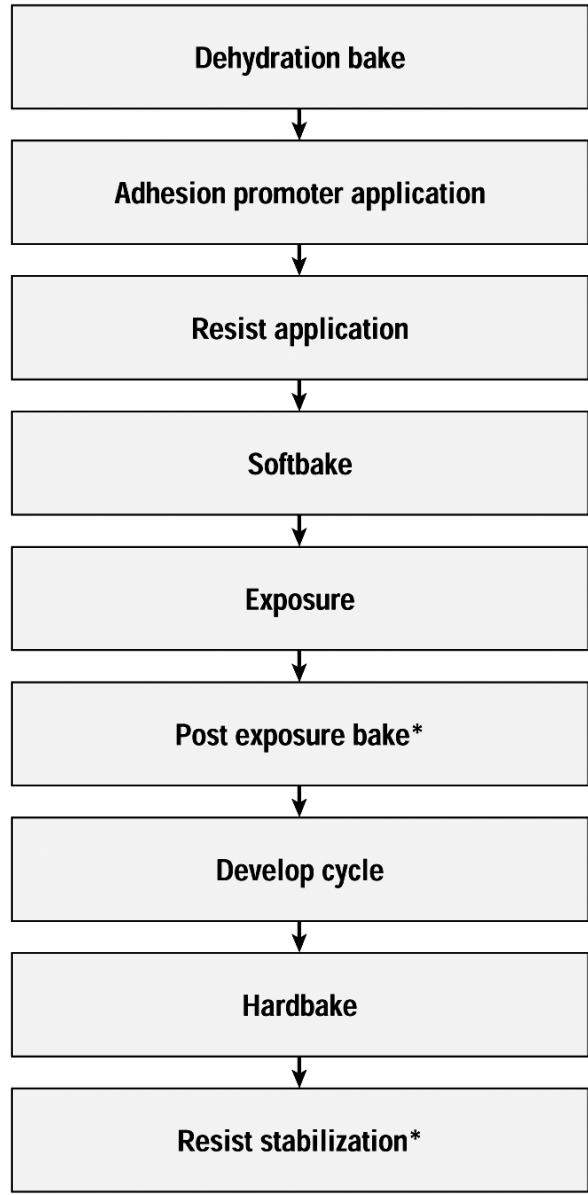


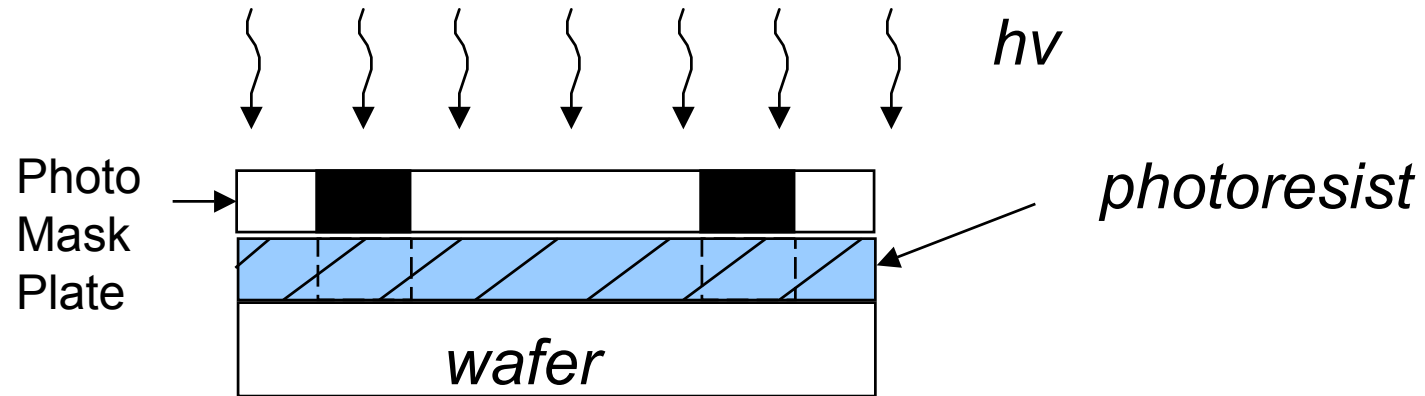
Figure 1.5 Steps required for a pattern transfer using optical lithography.



*Optional steps

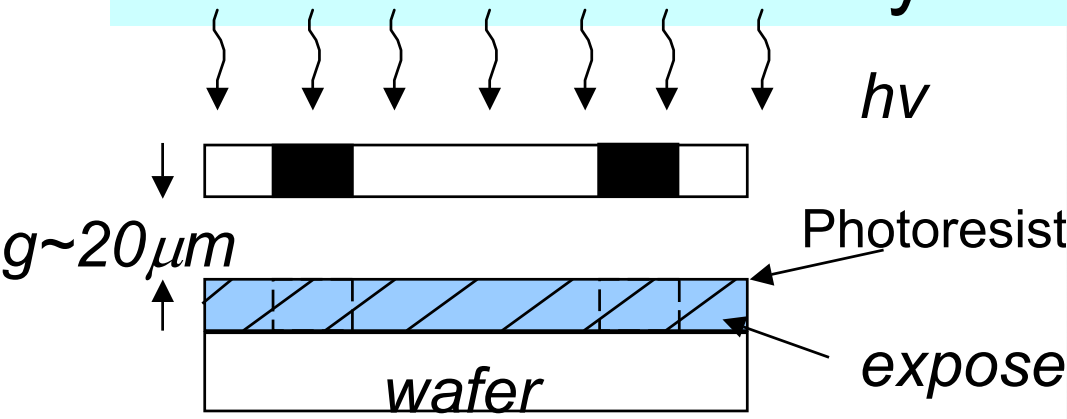
Figure 8.9 Typical process flow in a photolithography step.

Contact Printing



- Resolution $R < 0.5\mu\text{m}$
- mask plate is easily damaged or accumulates defects

Proximity Printing



$$R = k (\lambda g)^{1/2}$$

$\sim 1 \mu\text{m}$ for visible photons,
much smaller for X-ray lithography

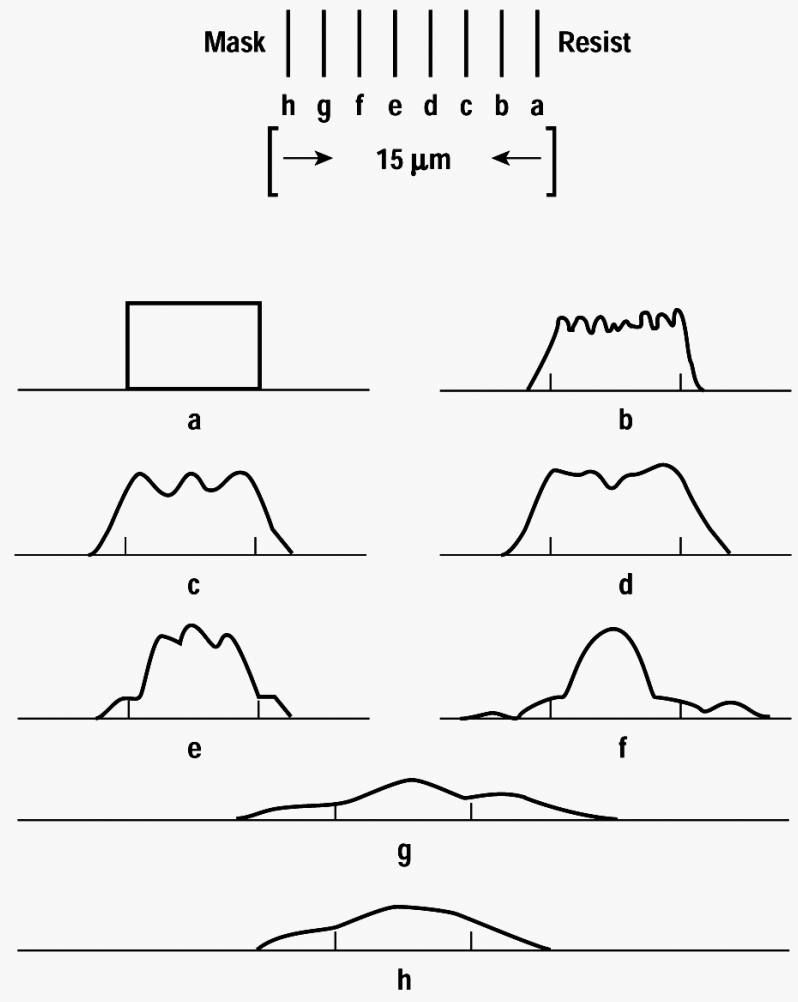
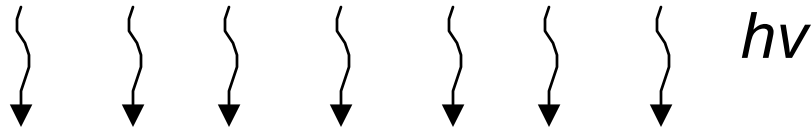


Figure 7.16 Intensity as a function of position on the wafer for a proximity printing system where the gap increases linearly from $g = 0$ to $g = 15 \text{ mm}$ (after Geikas and Ables).

Projection Printing



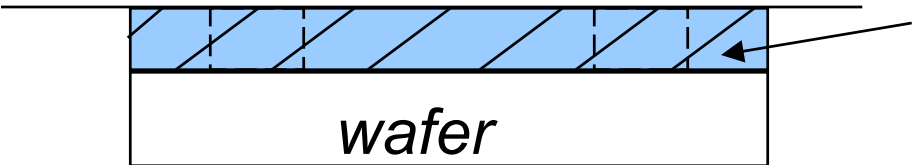
De-Magnification: nX



- 10X stepper
- 4X stepper
- 1X stepper

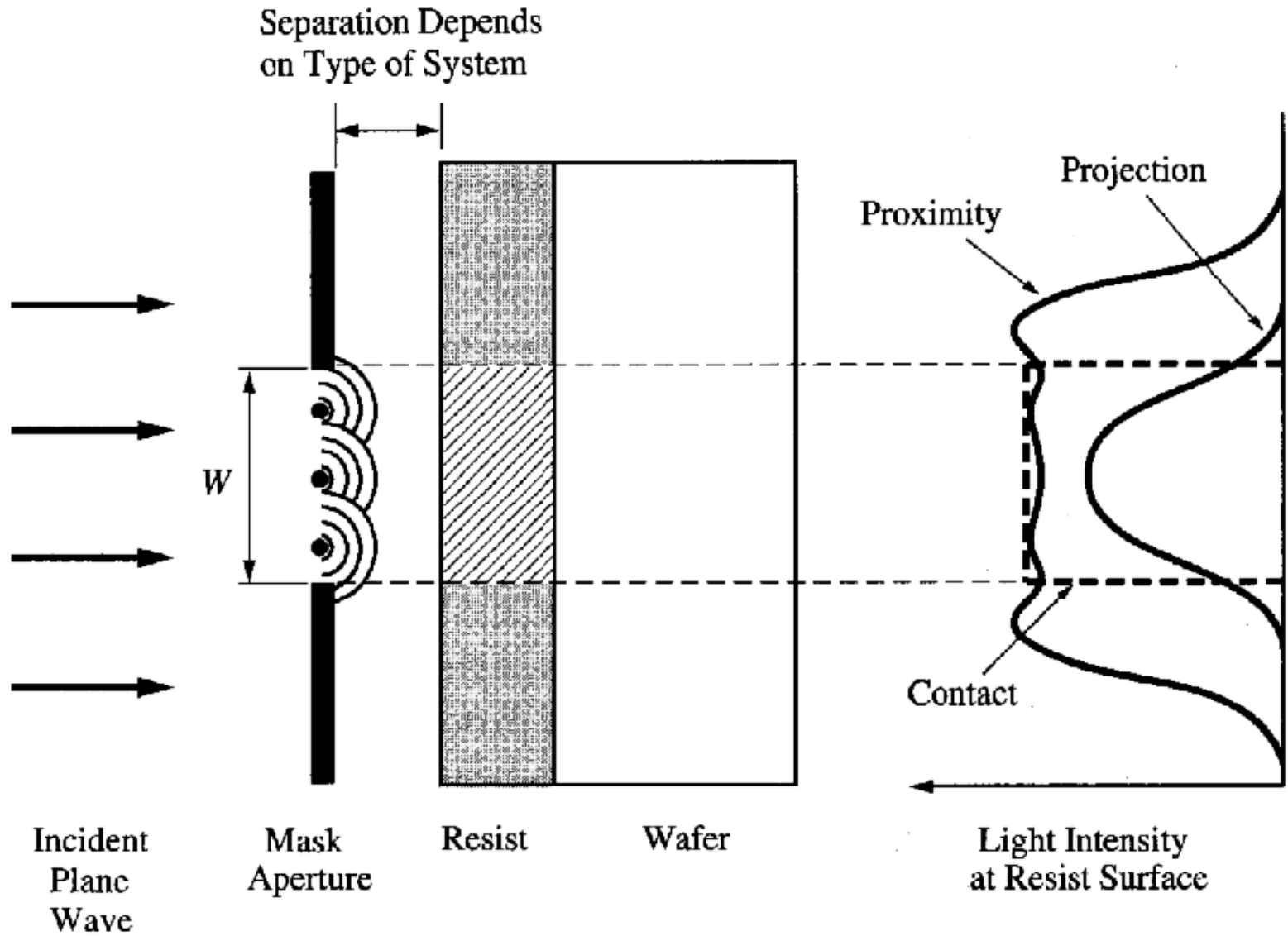


focal plane

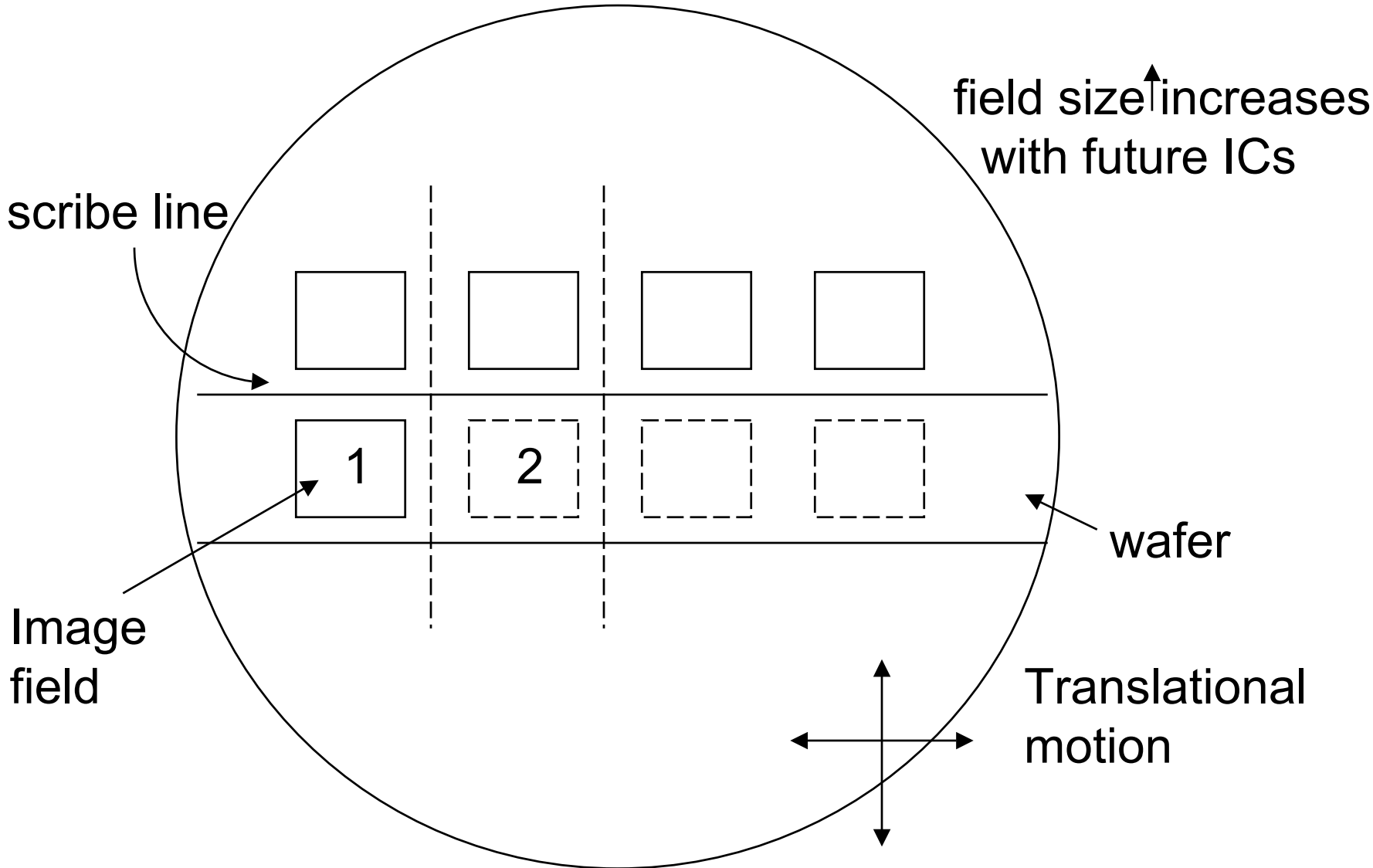


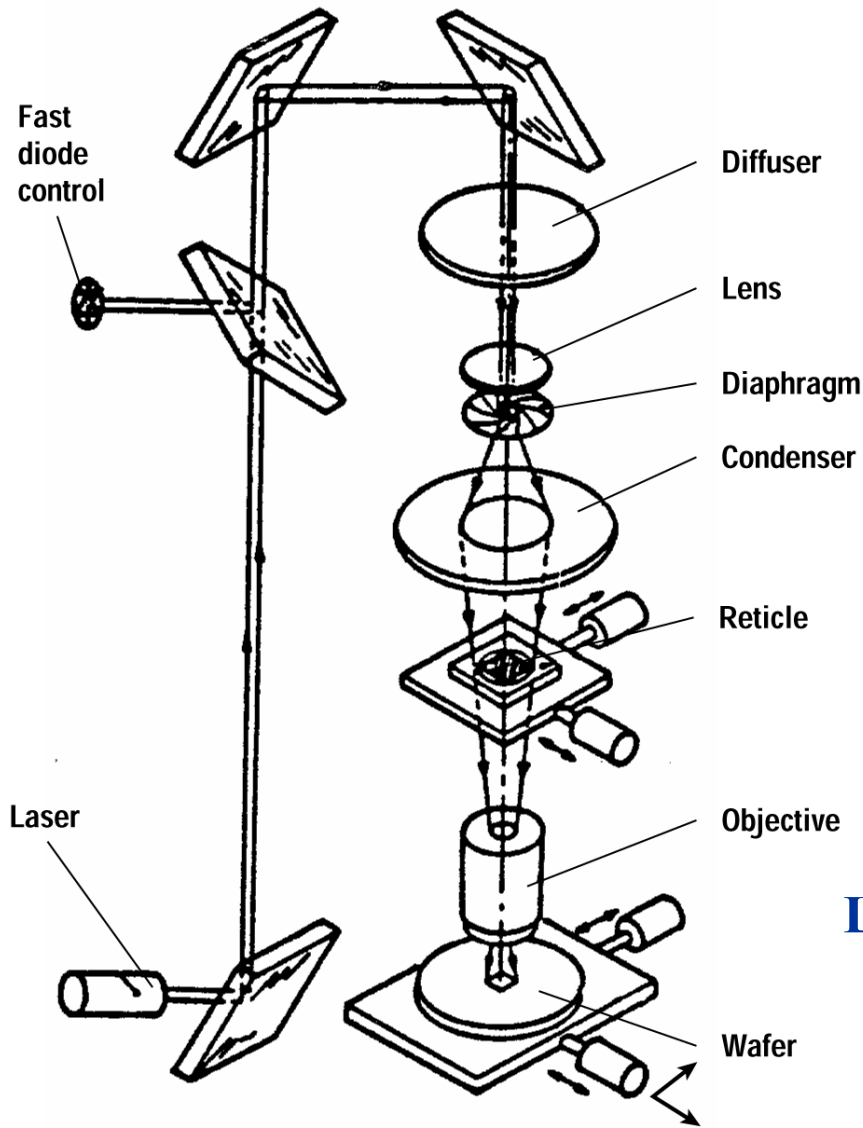
$\sim 0.2 \mu\text{m}$ resolution (deep UV photons)
 tradeoff: optics complicated and expensive

Aerial Images formed by Contact Printing, Proximity Printing and Projection Printing



Optical Stepper





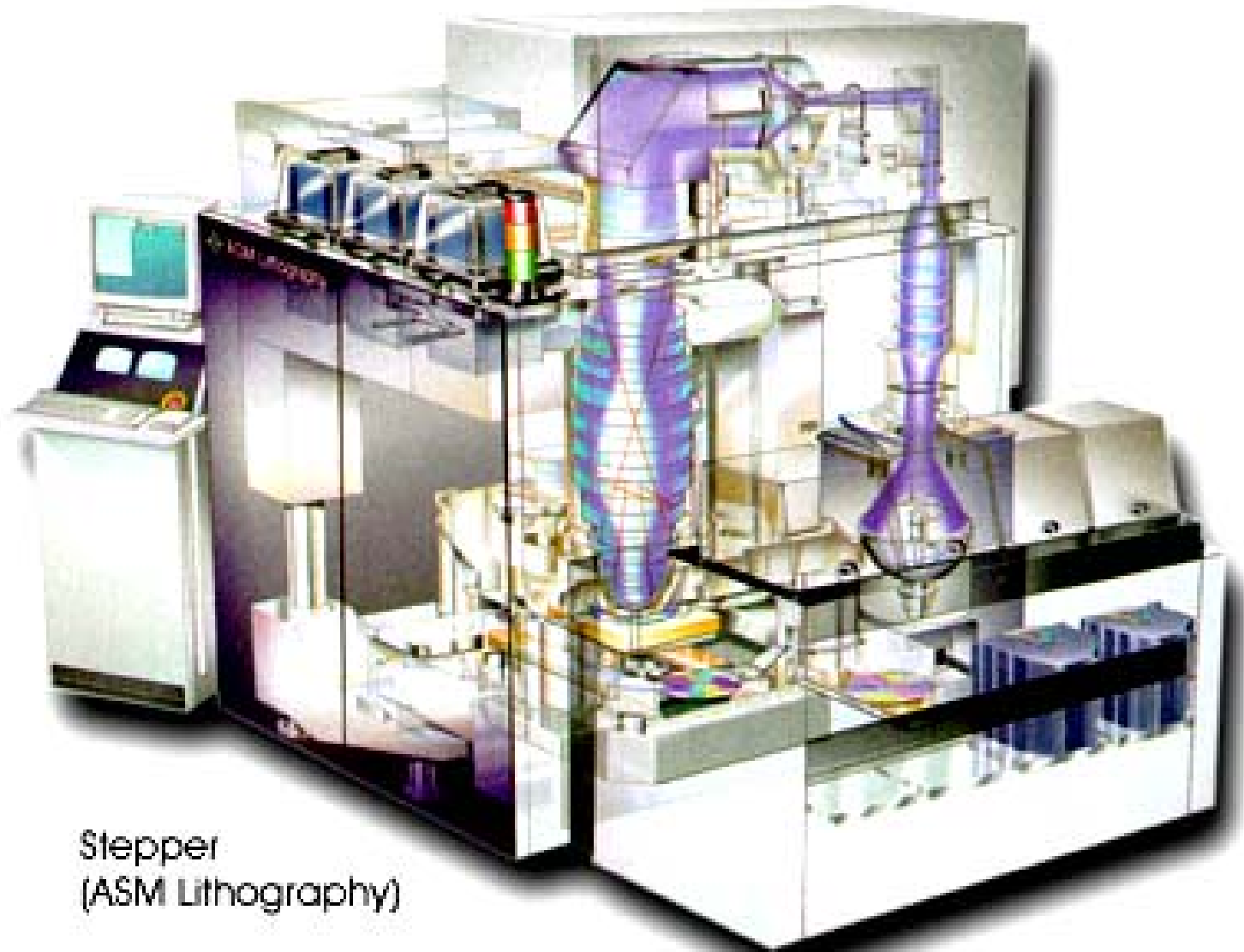
Excimer Laser Stepper

**Light is in pulses of 20 ns duration
at a repetition rate of a few kHz.
About 50 pulses are used.**

Figure 7.14 Optical train for an excimer laser stepper (after Jain).

See Plummer et al , Ch 5

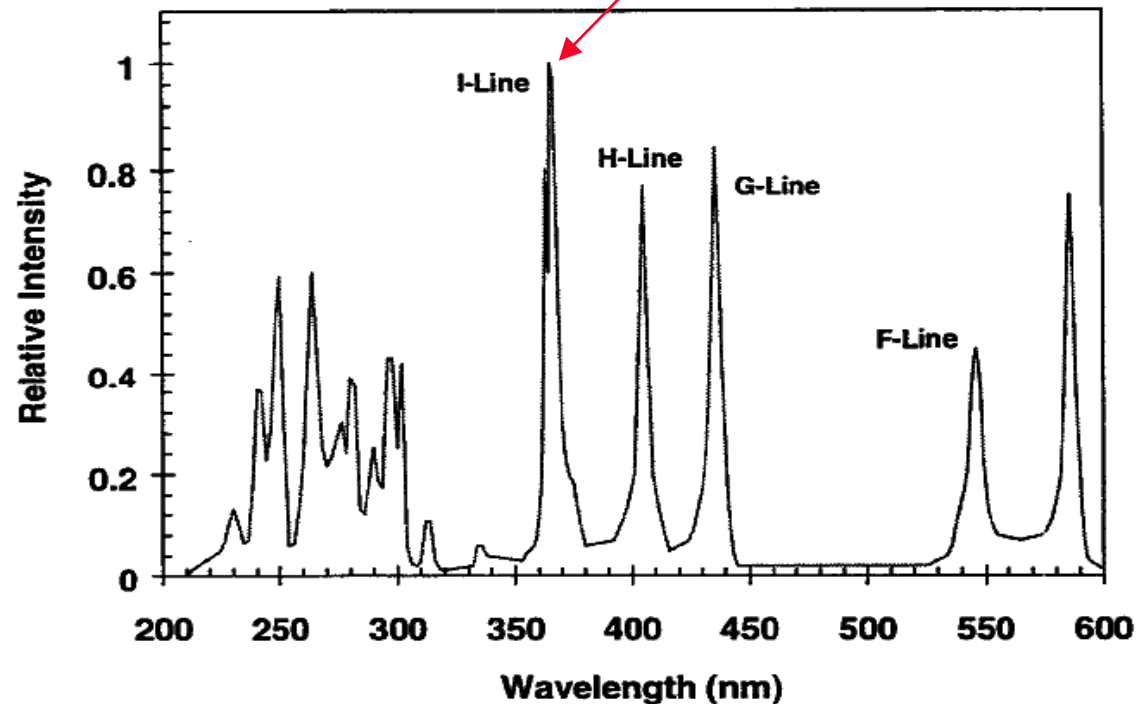
Excimer Laser Stepper



Stepper
(ASM Lithography)

Photon sources

- Hg Arc lamps 436(G-line), 405(H-line), 365(I-line) nm
- Excimer lasers: KrF (248nm) and ArF (193nm)
- Laser pulsed plasma (13nm, EUV)

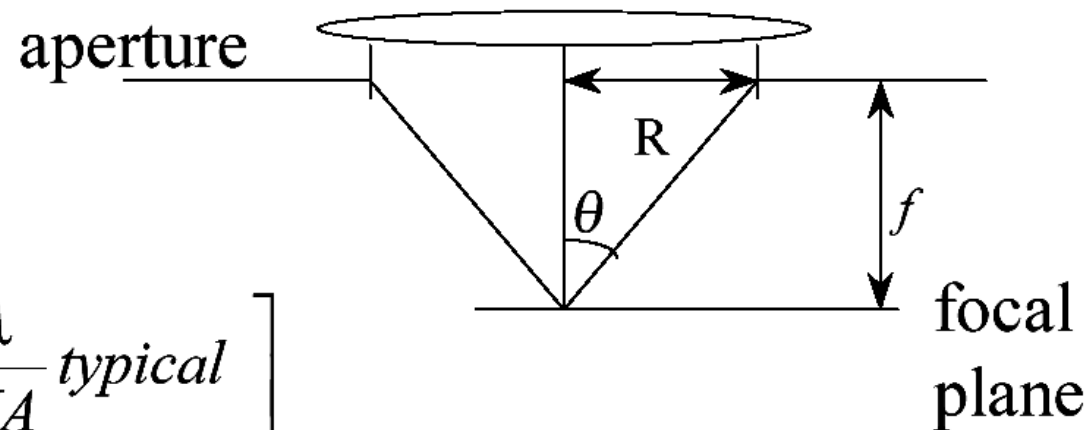


Source Monitoring

- Filters can be used to limit exposure wavelengths
- Intensity uniformity has to be better than several % over the collection area
- Needs spectral exposure meter for routine calibration due to aging

Projection Printing Considerations

(1) Resolution



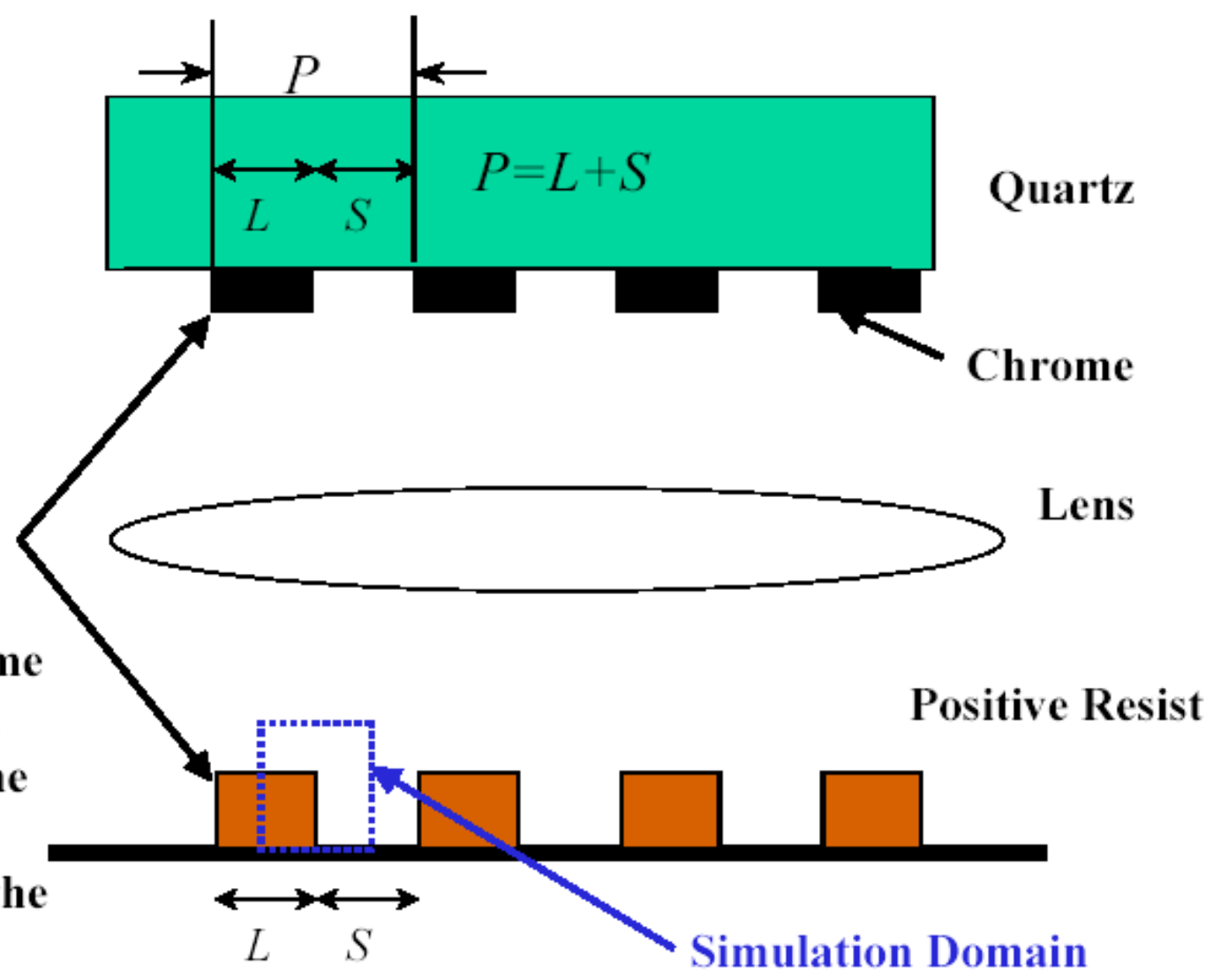
$$l_m = k_1 \frac{\lambda}{NA} \quad \left[0.6 \frac{\lambda}{NA} \text{ typical} \right]$$

$NA \equiv$ numerical aperture of lens.

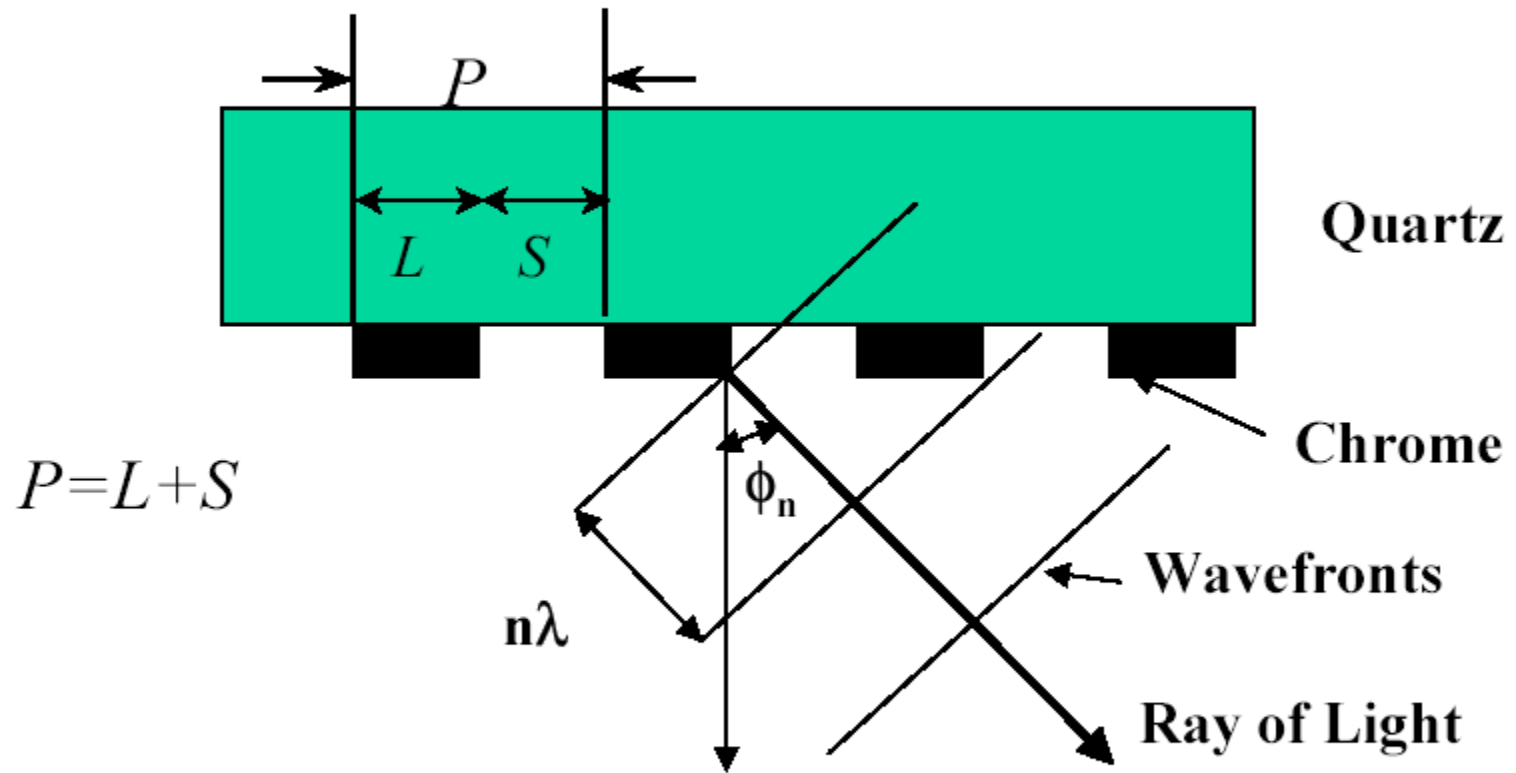
$$= \sin \theta$$

$k_1 =$ a constant between 0.25 and 1, depending on optics, resist, and process latitude

Line and Space Definition for EE143

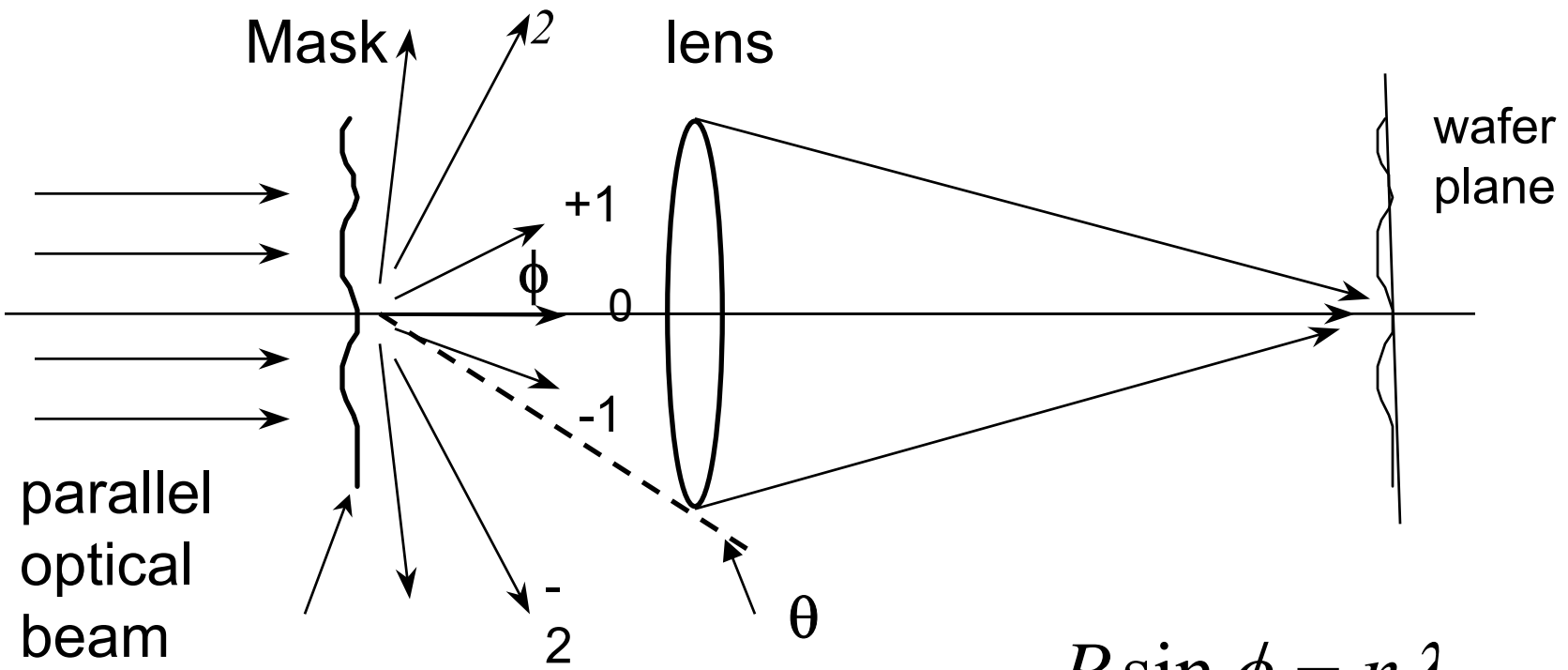


Bragg Condition



$$P \sin \phi_n = n\lambda$$

Qualitative Explanation of image degradation by lens

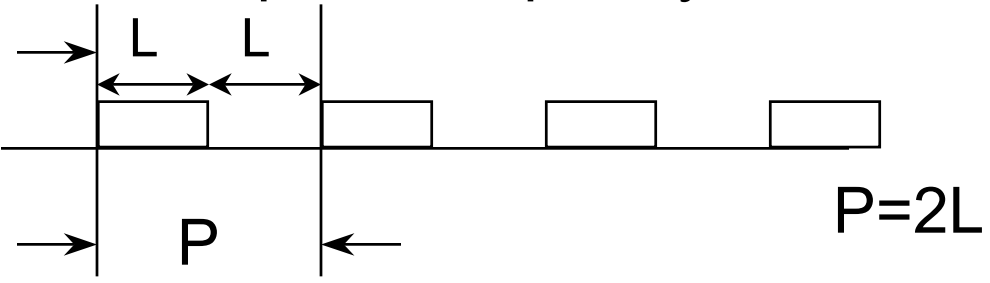


$$P \sin \phi = n\lambda$$

$$n = 0, \pm 1, \pm 2, \dots$$

$$\sin \theta = \text{NA of lens}$$

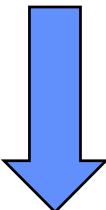
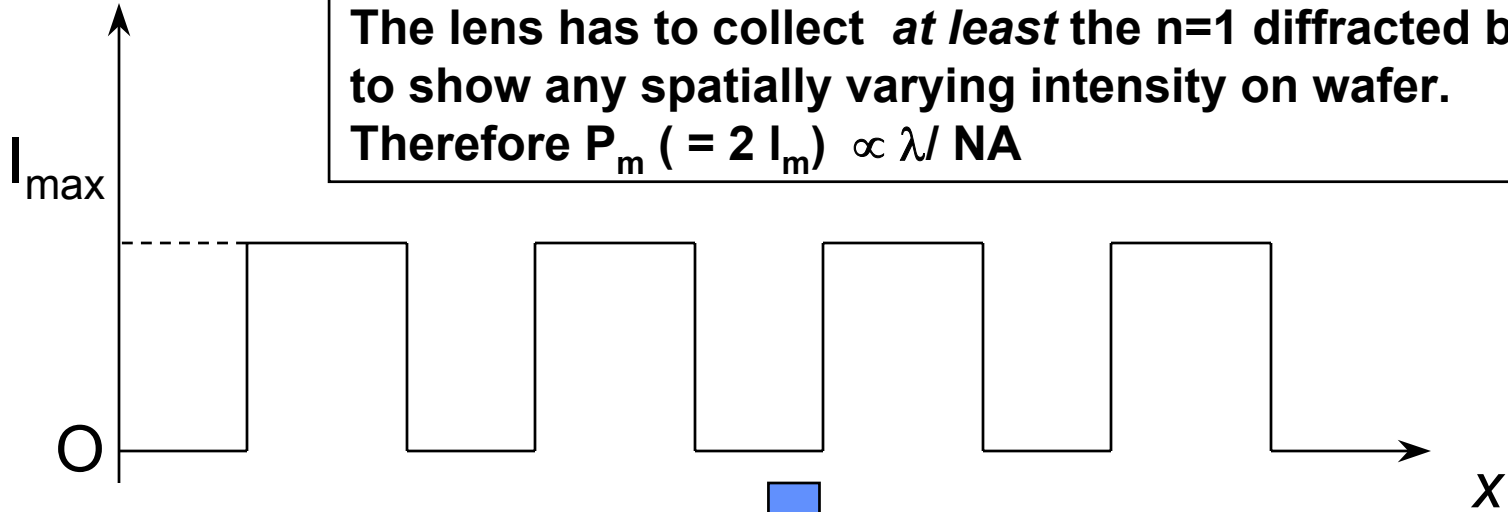
grating with spatial frequency $1/P$



Why $I_m \propto \frac{\lambda}{NA}$?

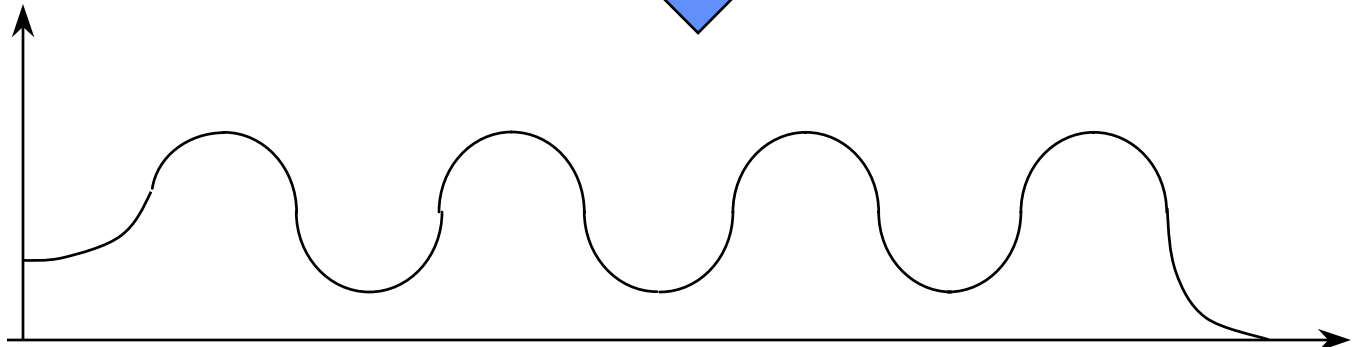
Mask Intensity

The lens has to collect *at least* the n=1 diffracted beams to show any spatially varying intensity on wafer.
 Therefore $P_m (= 2 I_m) \propto \lambda / NA$



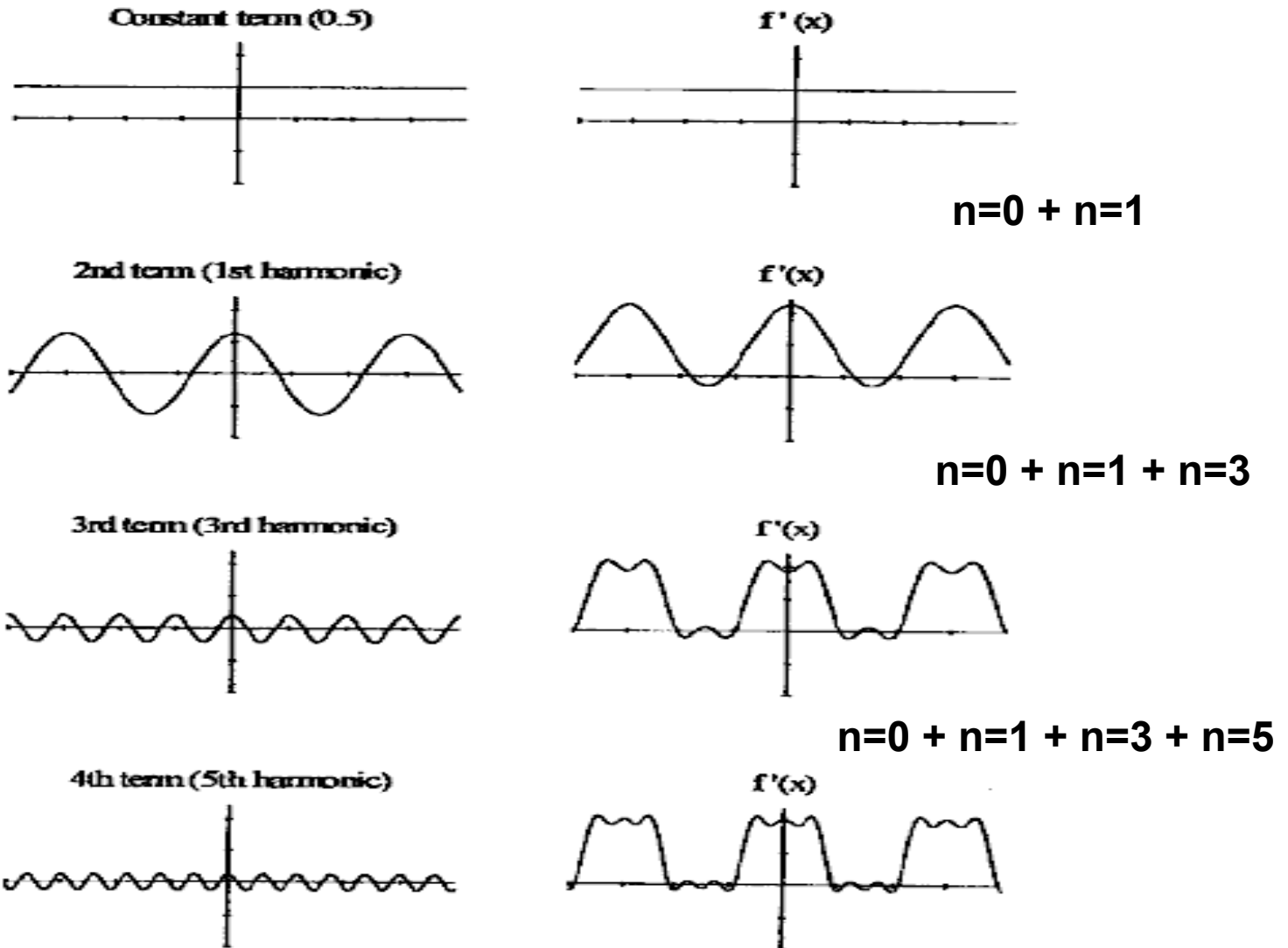
optical system

Image on wafer

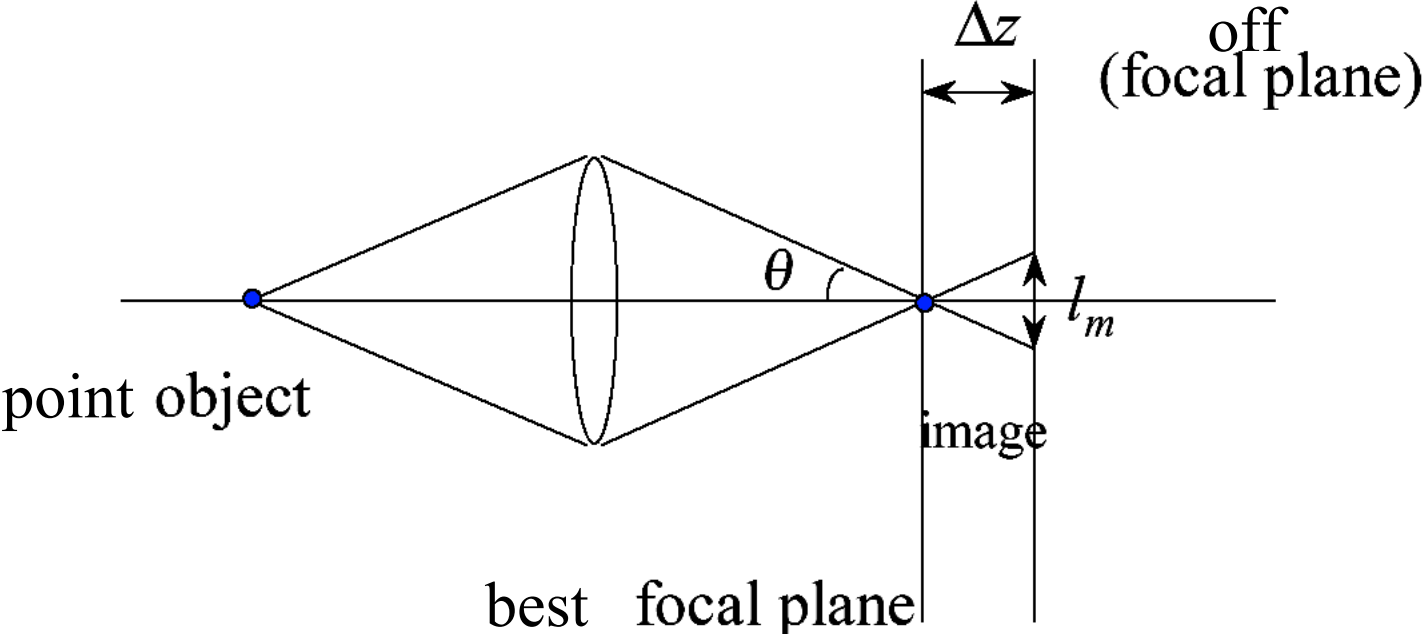


For advanced reading , see “Microlithography-Science and Technology ” by Sheats and Smith,

Effect of Fourier Components on aerial image of a rectangular waveform



Depth of Focus (DOF)



$$\Delta z = k_2 \frac{\lambda}{(NA)^2} \approx \frac{\pm l_m / 2}{\tan \theta} \approx \frac{\pm l_m / 2}{\sin \theta} = \pm \frac{\lambda}{2(NA)^2} \text{ for small } \theta$$

$0.5 < k_2 < 1$

Simulated aerial images with various degree of defocus

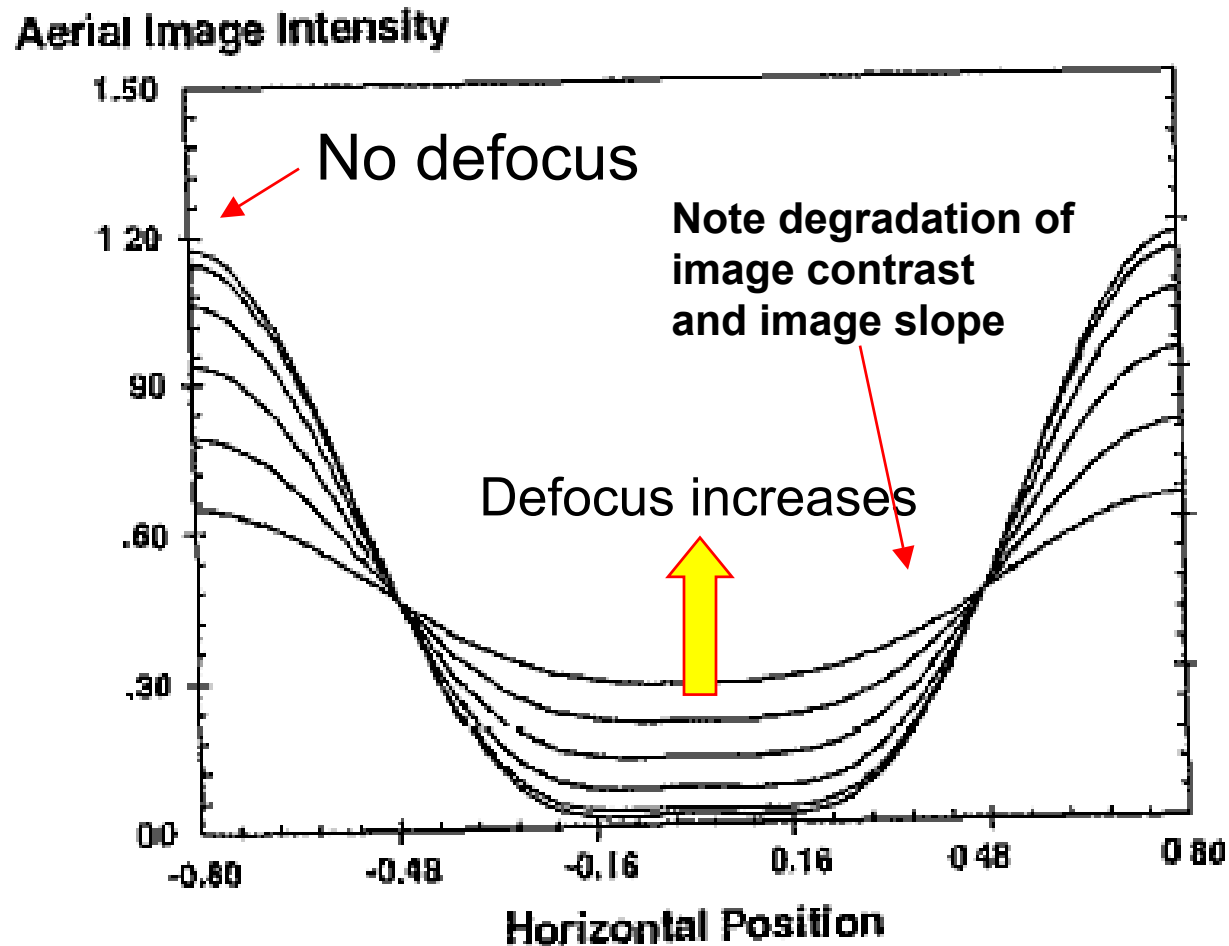
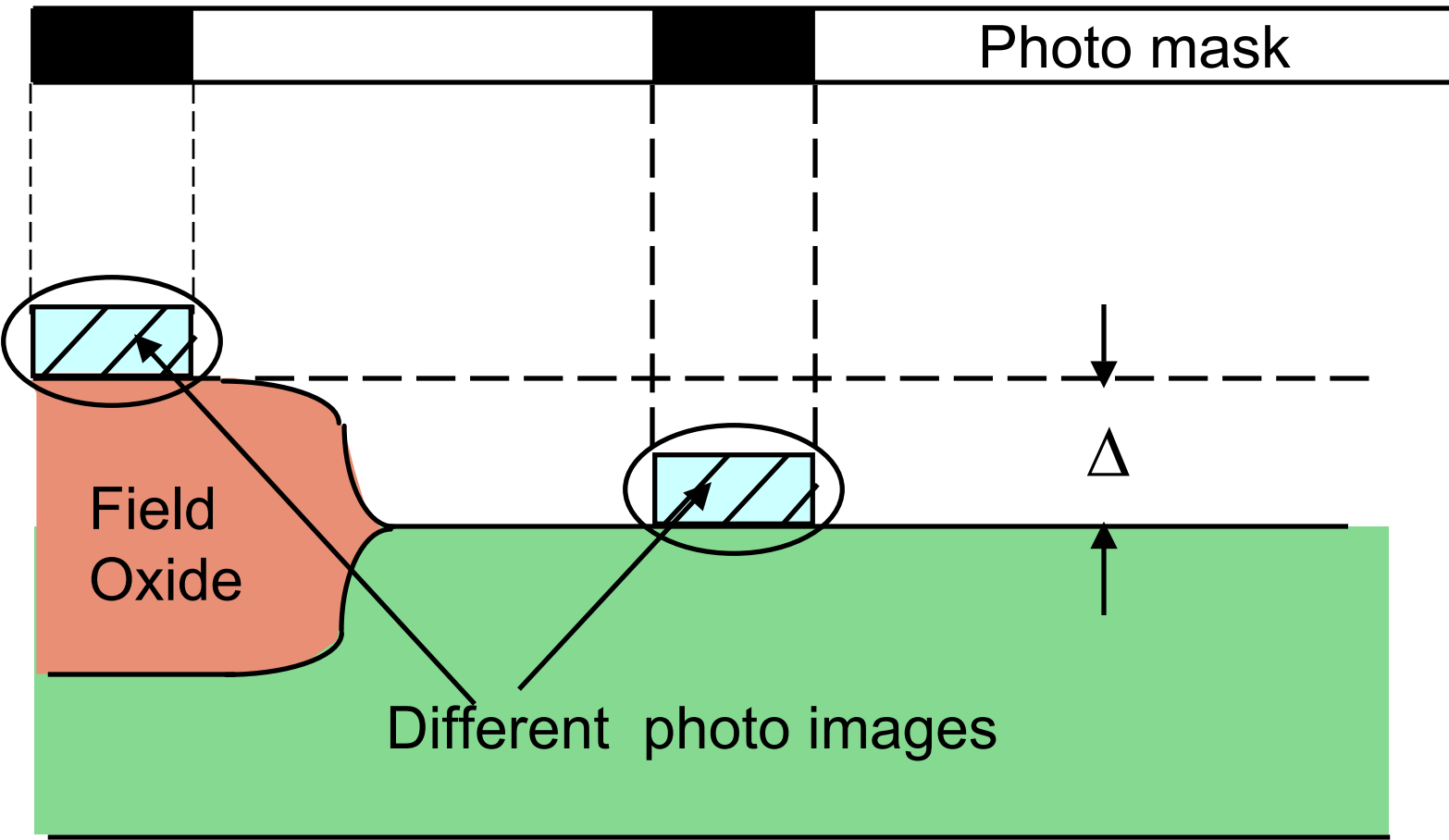


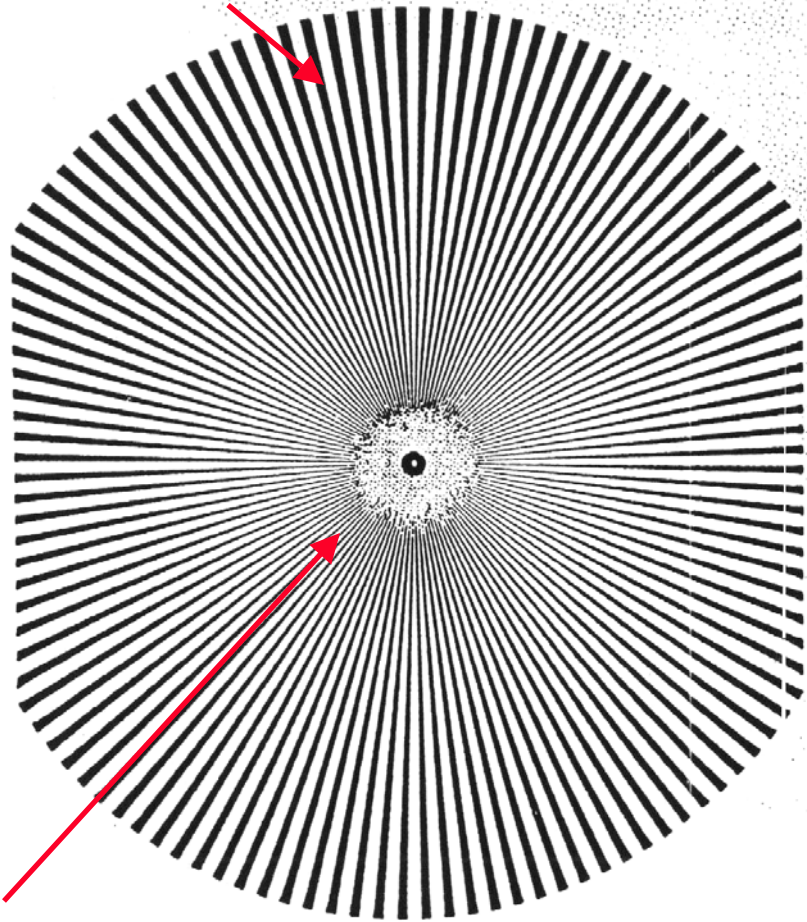
FIG. 7.10 Aerial image intensity of a $0.8 \lambda / \text{NA}$ line and space pattern as focus is changed in steps of 0.4 Rayleigh units.

Example of DOF problem

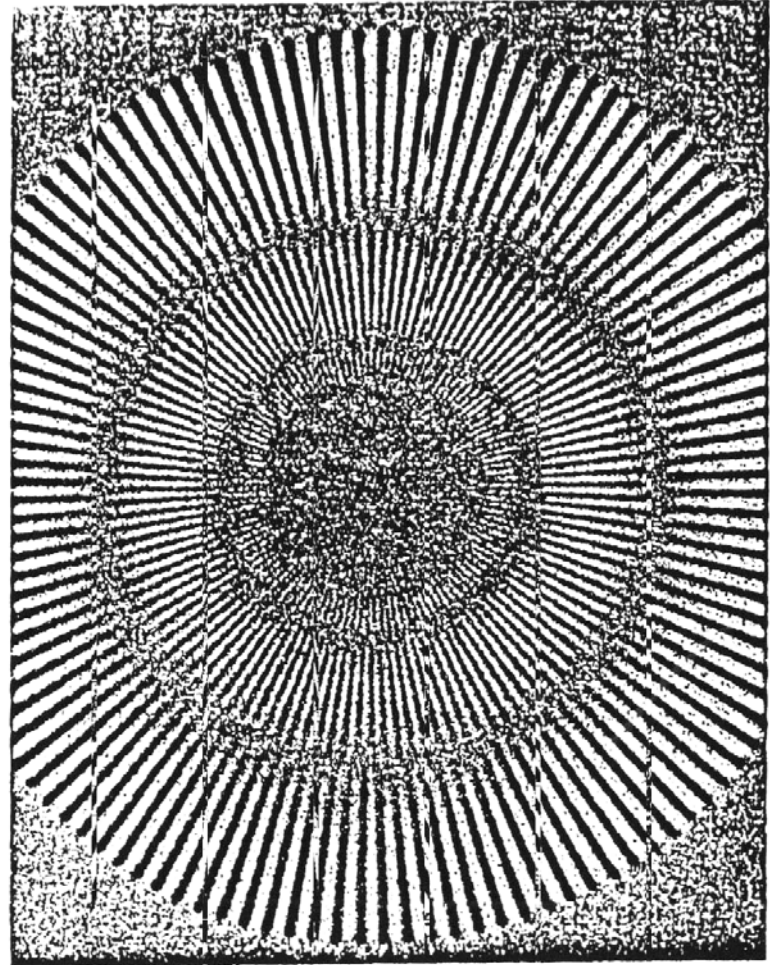


Focus versus Extreme Defocus (an illustration)

Large P features



(a)



(b)

For Reference only

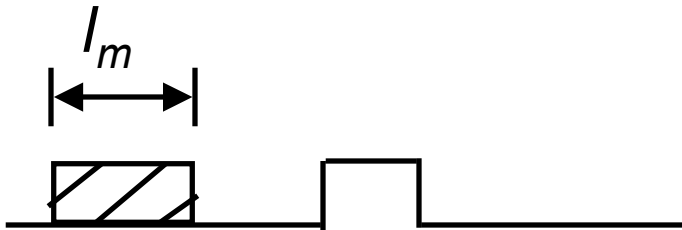
Small P features

Best focus

Extreme Defocus

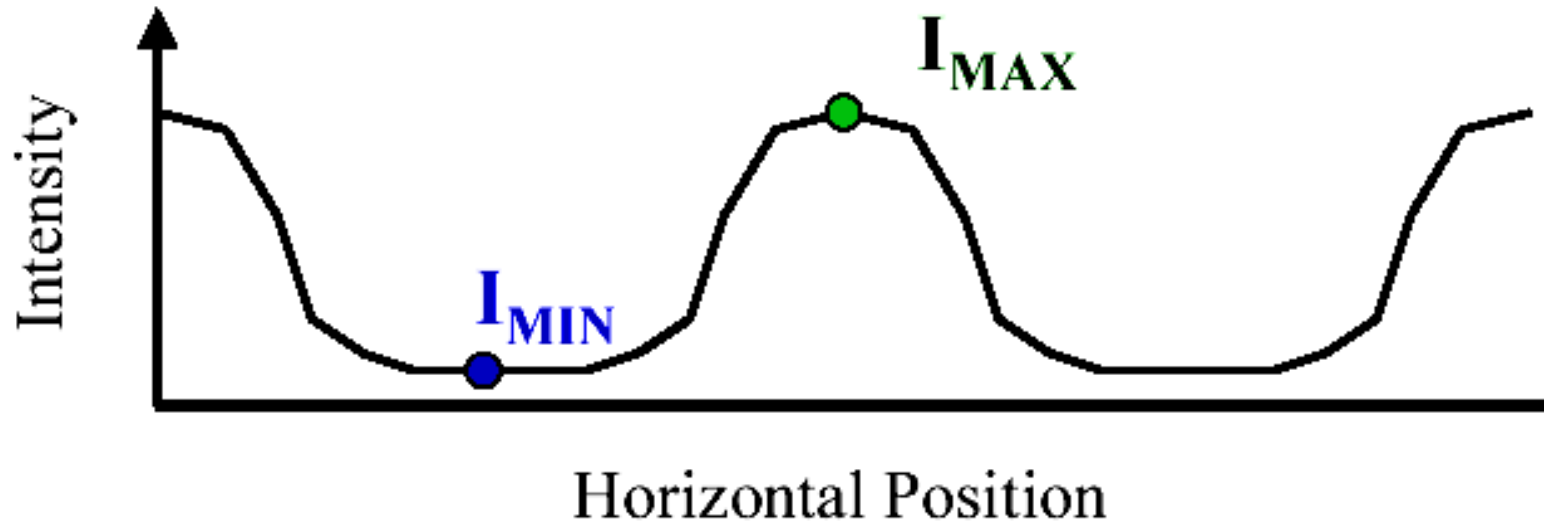
$$(1) l_m \cong 0.6 \frac{\lambda}{NA} \quad \text{want small } l_m$$

$$(2) DOF = \pm \frac{\lambda}{2(NA)^2} \quad \text{want large } DOF$$



(1) and (2) require a compromise between λ and NA !

Image Quality Metric: Contrast

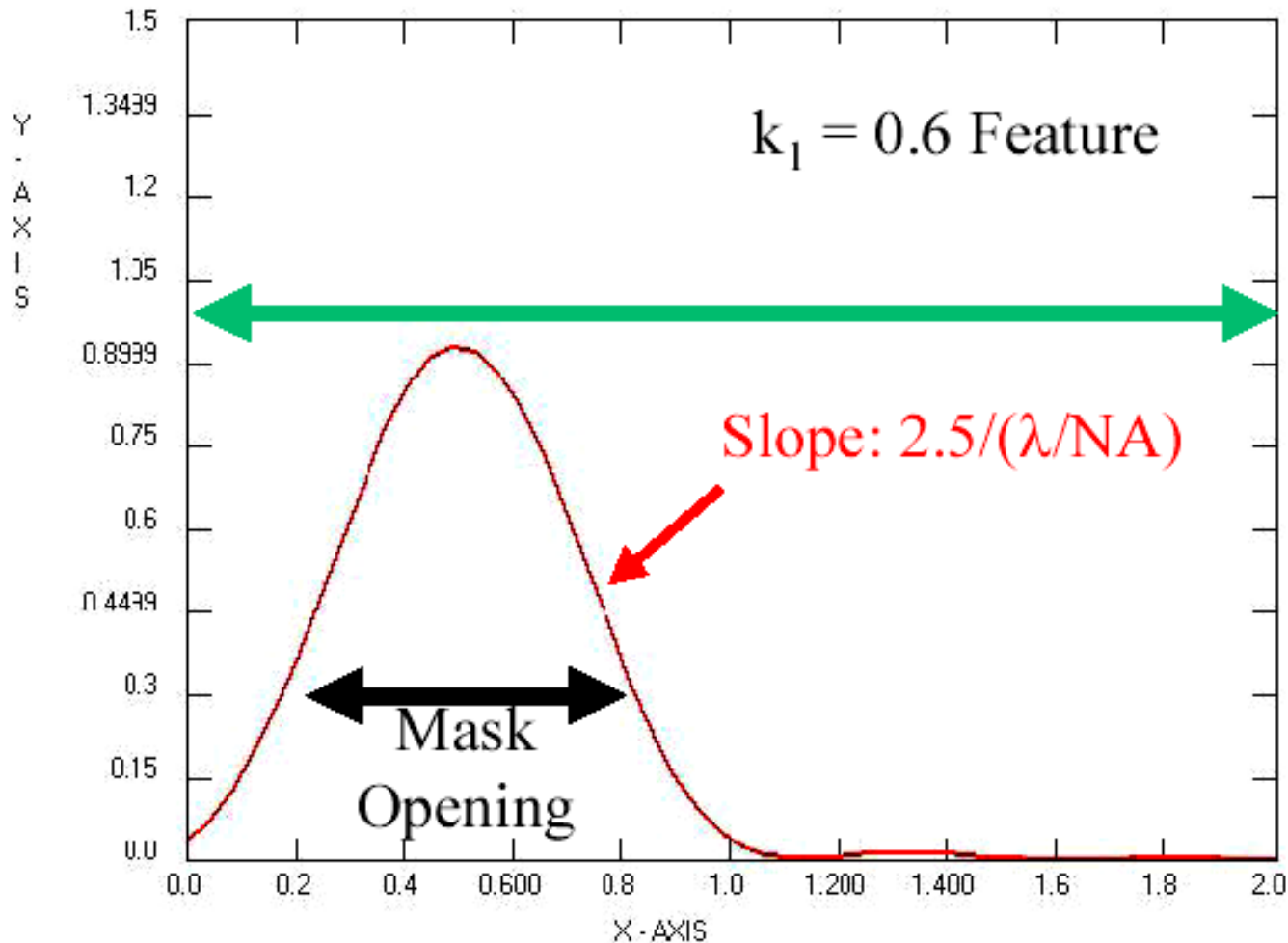


Contrast:

$$C = \frac{I_{MAX} - I_{MIN}}{I_{MAX} + I_{MIN}}$$

The contrast is always between 0 (no variation) and 1 (perfect minimum).

Image Quality metric: Slope of image

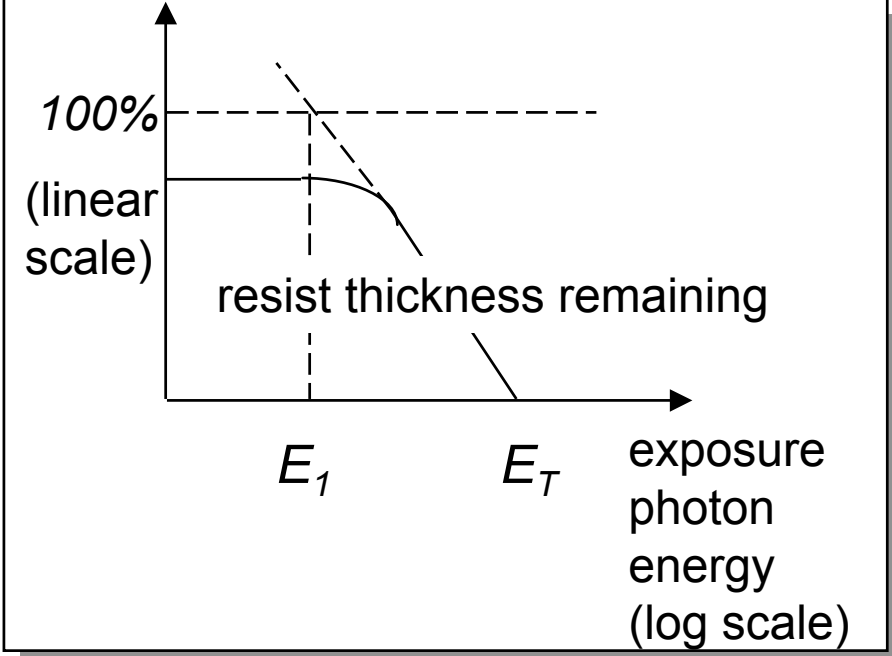
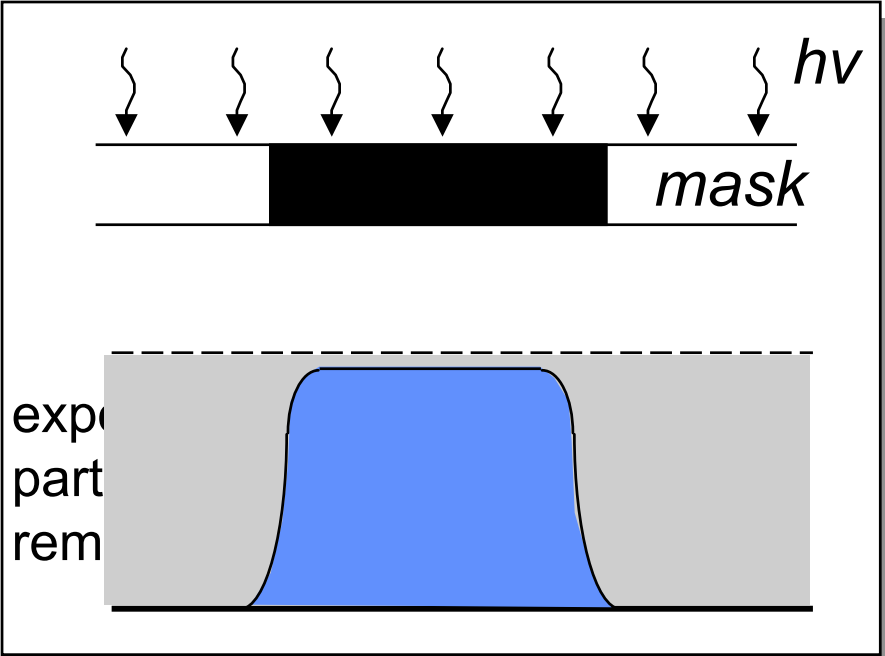


* simulated aerial image of an isolated line

Two Resist Types

- Negative Resist
 - Polymer (Molecular Weight (MW) ~65000)
 - Light Sensitive Additive Promotes Crosslinking
 - Volatile Solvents
 - Light breaks N-N => Crosslink Chains
 - Sensitive, hard, Swelling during Develop
- Positive Resist
 - Polymer (MW~5000)
 - Photoactive Inhibitor (20%)
 - Volatile Solvents
 - Inhibitor Loses N_2 => Alkali Soluble Acid
 - Develops by “etching” - No Swelling.

Positive Resist



$E_T = \text{resist sensitivity}$

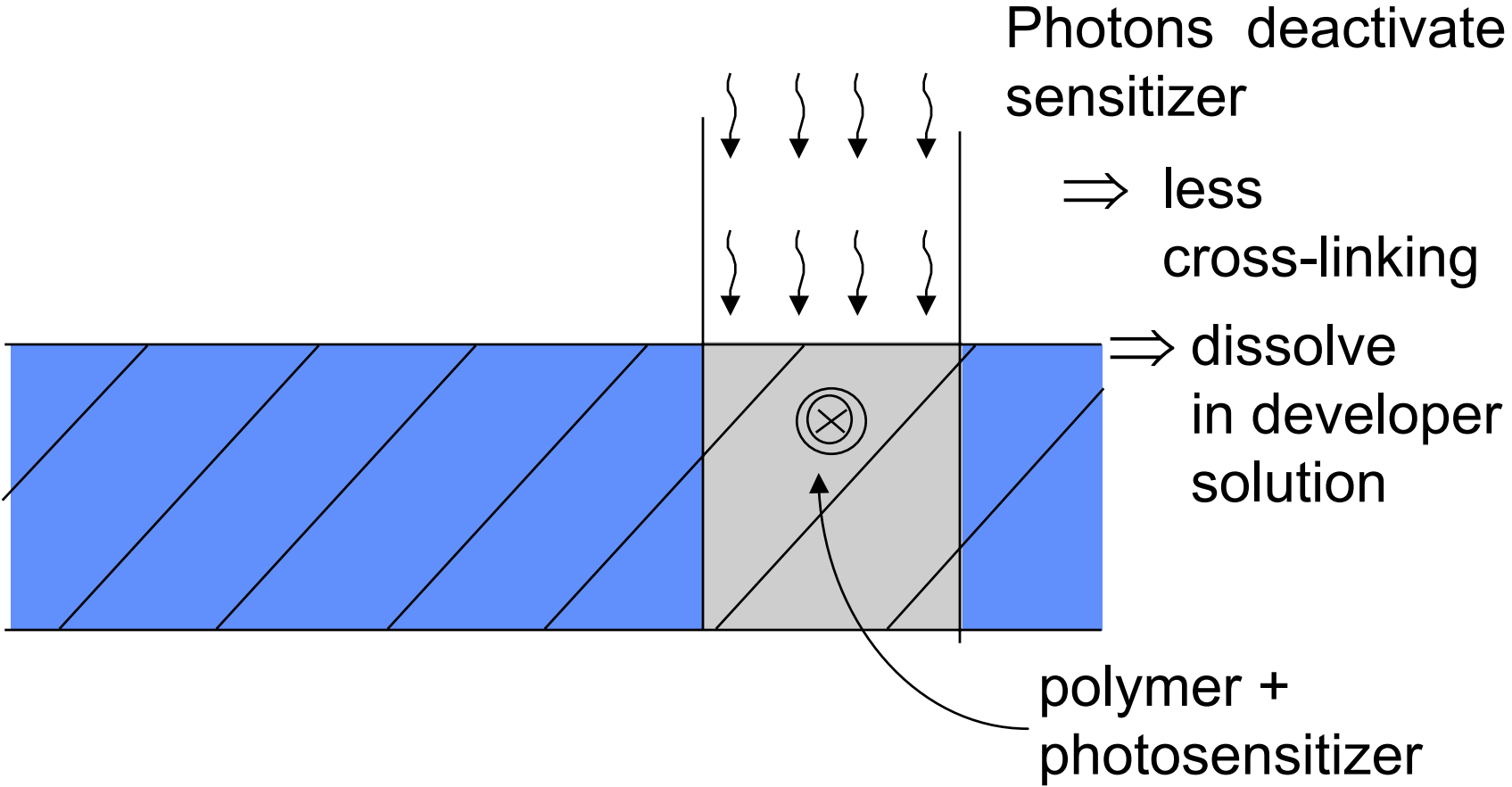
$\text{Resist contrast} \equiv \frac{1}{\log_{10}\left(\frac{E_T}{E_1}\right)}$

LOG TO BASE 10

$\gamma \sim 5 \text{ to } 10$

Note: In the 143 Reader, γ is defined as natural log

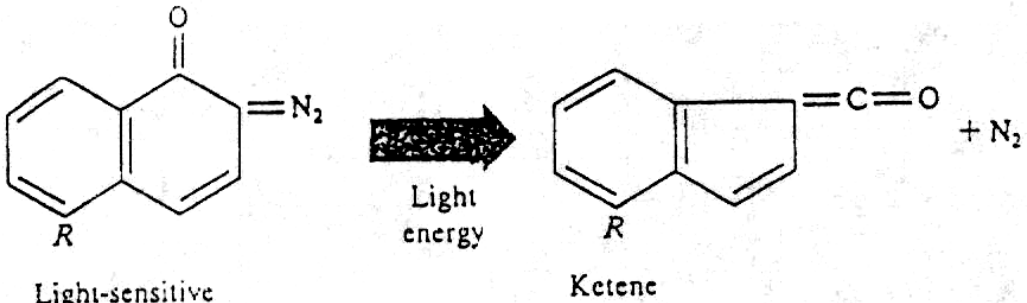
Positive P.R. Mechanism



Positive Resist Exposure Reaction

“diazide”

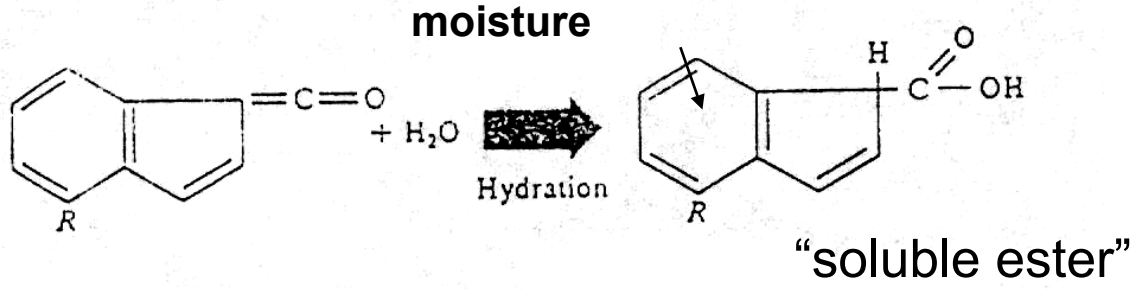
“ketene” - a = C = O group



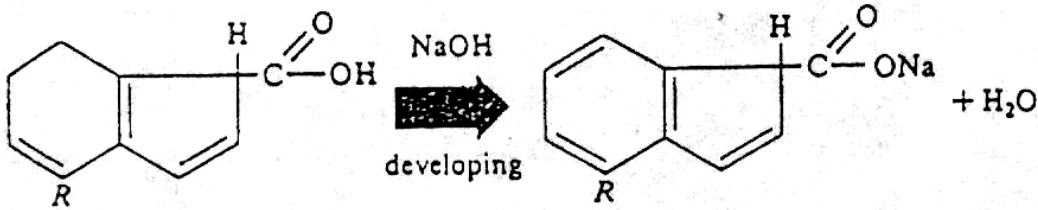
The ketene is short-lived intermediate

PAC

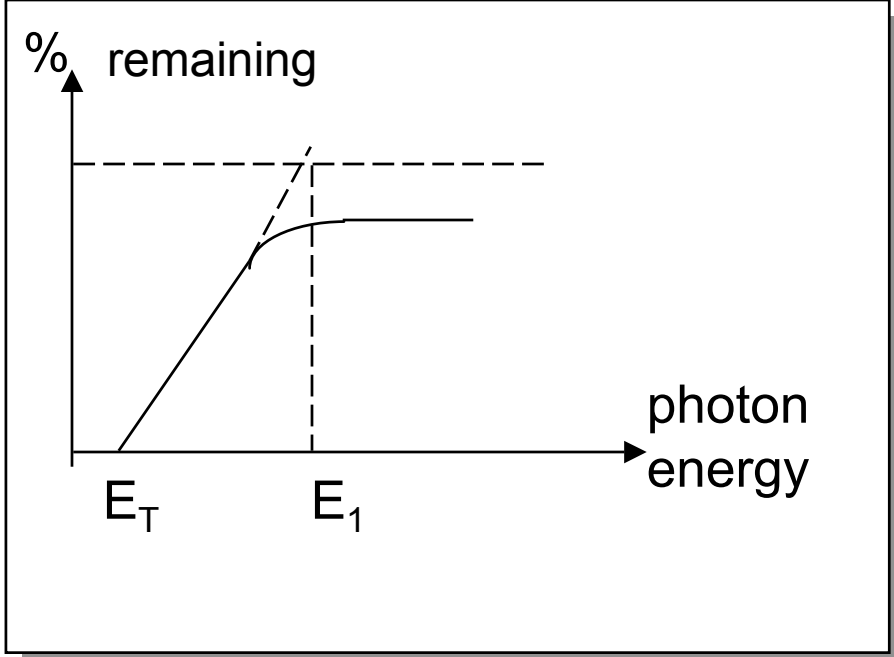
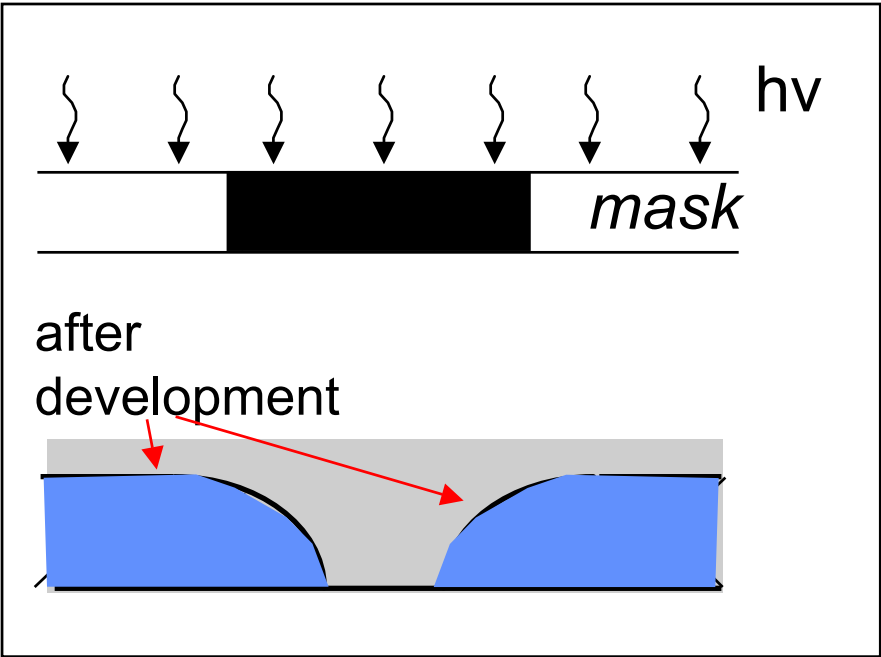
“carboxylic acid”



The carboxylic acid can react with the alkaline solution (the developer) to form a soluble ester.



Negative P.R. Mechanism



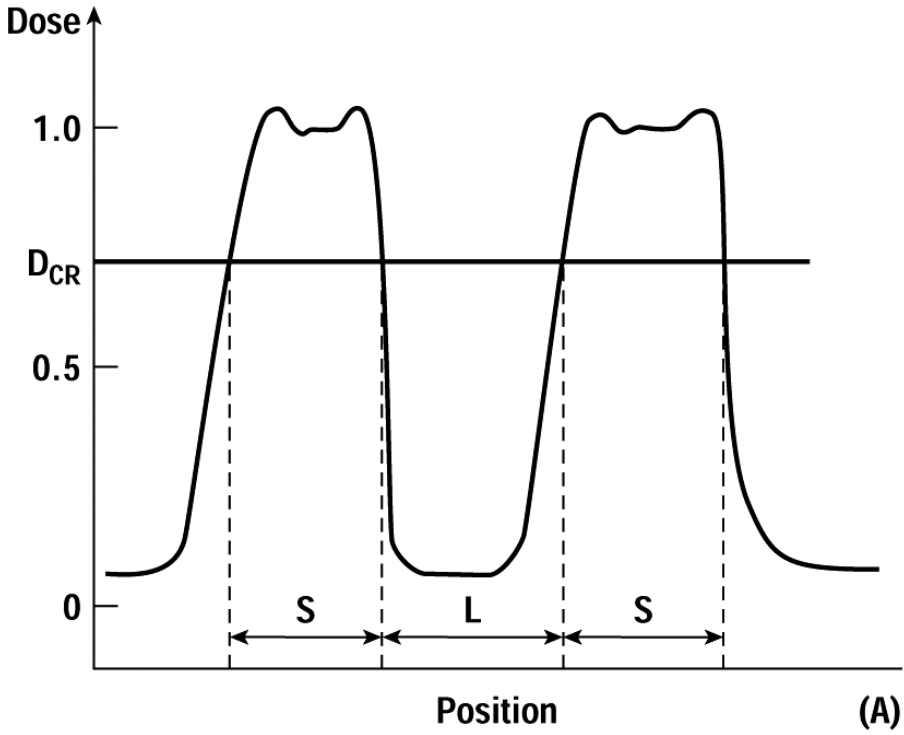
$$\gamma \equiv \frac{1}{\log\left(\frac{E_1}{E_T}\right)}$$

Log to base 10

$h\nu \Rightarrow$ cross-linking \Rightarrow insoluble in developer solution.

Infinite Contrast Resist

$$D_0 = D_{100} = D_{critical}$$



Finite Contrast Resist

$$D_0 \neq D_{100}$$

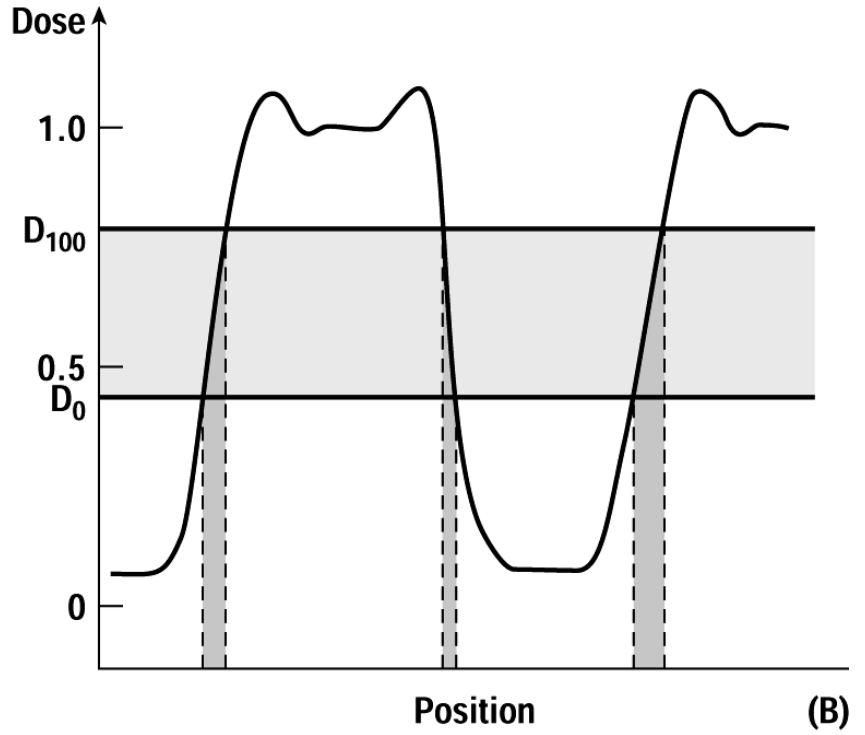
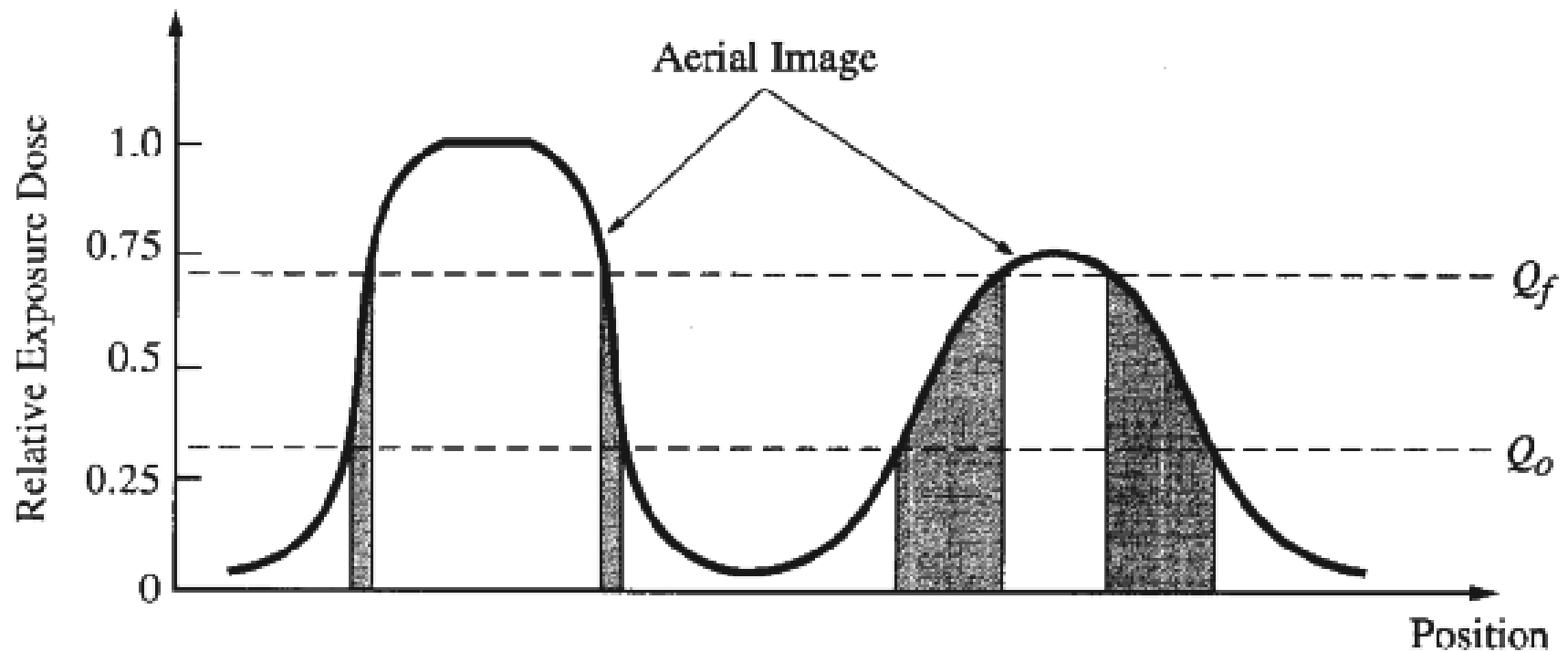


Figure 7.9 Plot of dose versus position on the wafer. Dose is given by the intensity of the light in the aerial image multiplied by the exposure time. Typical units are mJ/cm^2 .

energy

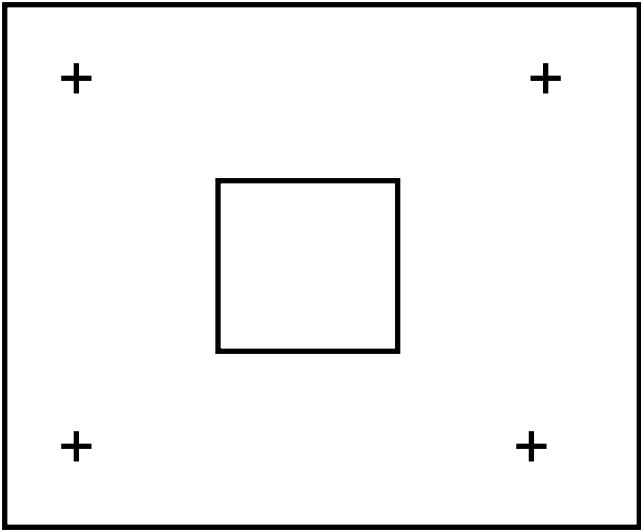
Figure 5-21 Example of how the quality of the aerial image and the resist contrast combine to produce the resist edge profile. The left side shows a sharp aerial image and steep resist edges (gray area). The example on the right shows a poorer aerial image and the resulting gradual edges on the resist profile.



Positive vs. Negative Photoresists

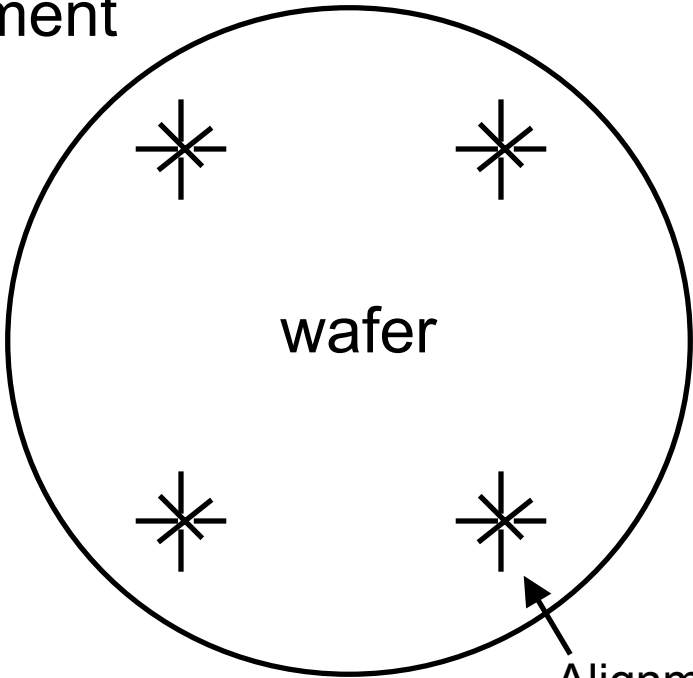
- **Positive P.R.:**
 - ✓ higher resolution
 - ✓ aqueous-based solvents
 - ✗ less sensitive
- **Negative P.R.:**
 - ✓ more sensitive => higher exposure throughput
 - ✓ relatively tolerant of developing conditions
 - ✓ better chemical resistance => better mask material
 - ✓ less expensive
 - ✗ lower resolution
 - ✗ organic-based solvents

Overlay Errors



photomask plate

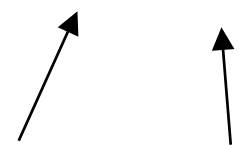
alignment mask



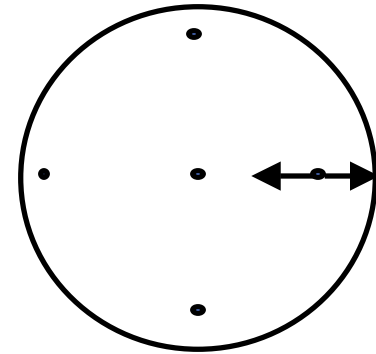
Alignment marks from previous masking level

(1) Thermal run-in/run-out errors

$$R = r \cdot (\Delta T_m \cdot \alpha_m - \Delta T_{si} \cdot \alpha_{si})$$

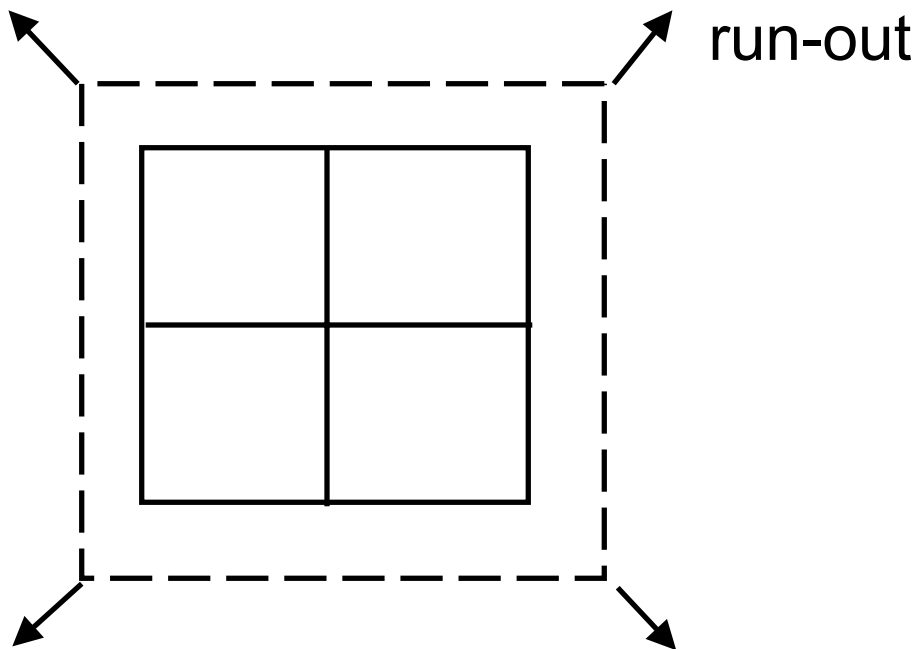


 run-out error wafer radius

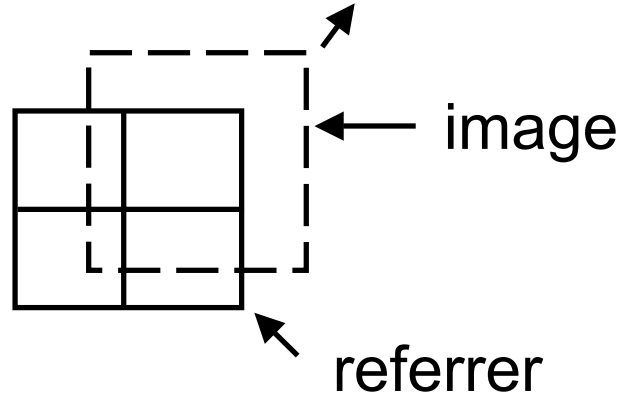
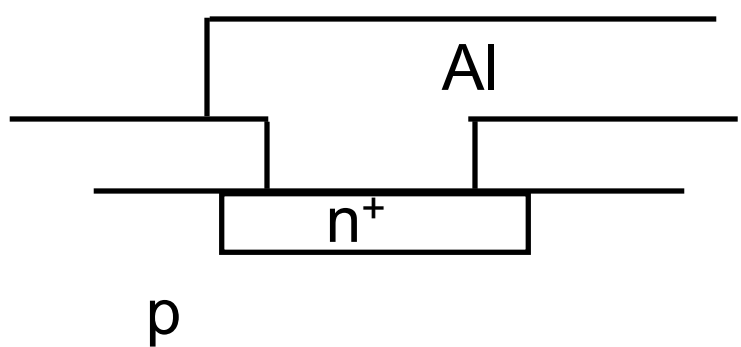


$\Delta T_m, \Delta T_{si}$ = change of mask and wafer temp.

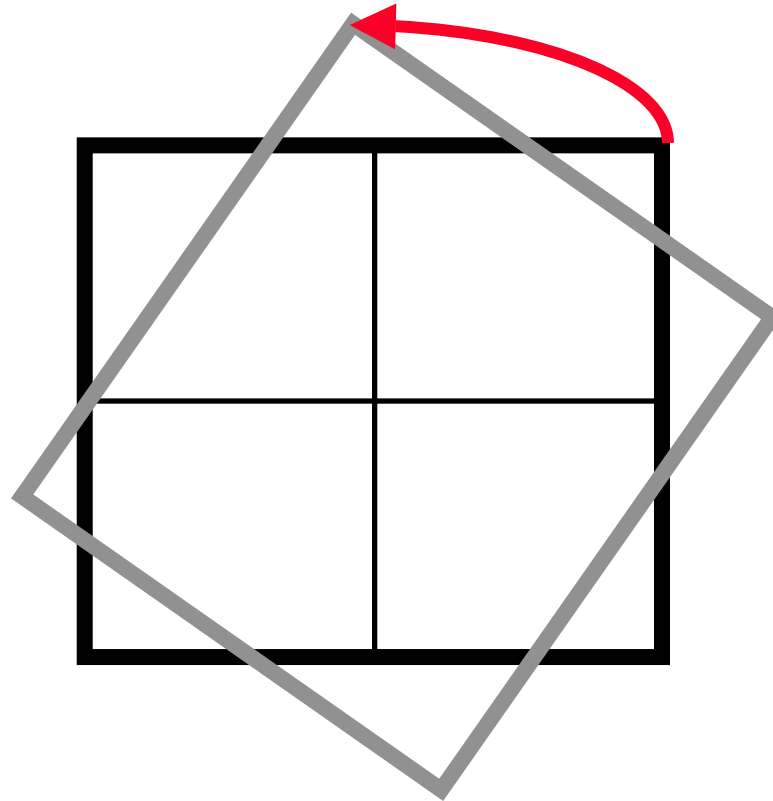
α_m, α_{si} = coefficient of thermal expansion of mask & Si



(2) Translational Error



(3) Rotational Error





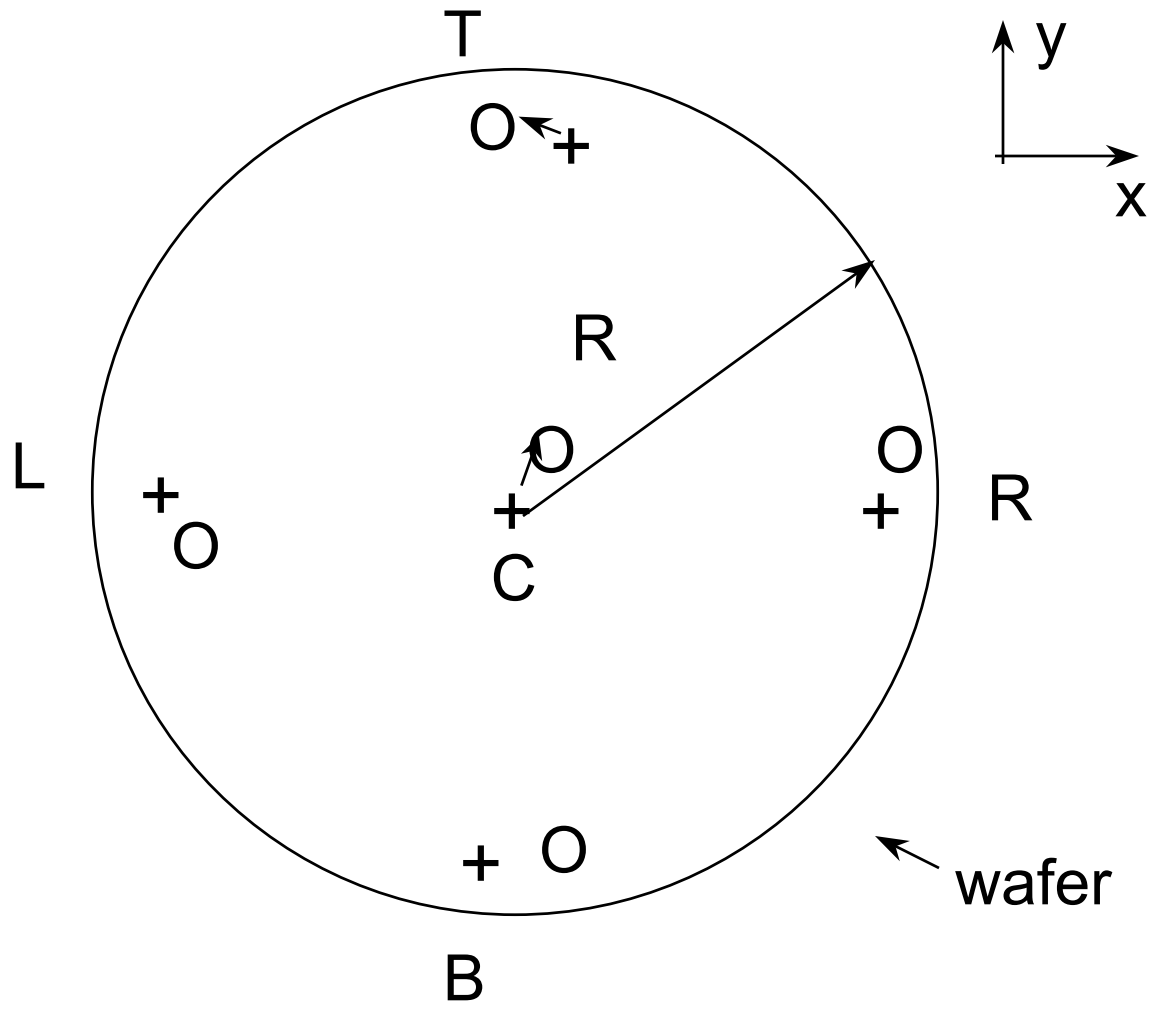
Misalignment



Runout

Figure 7.28 Two typical registration errors.

Characterization of Overlay Errors



O =optical image

+ =alignment marks on wafer

Example

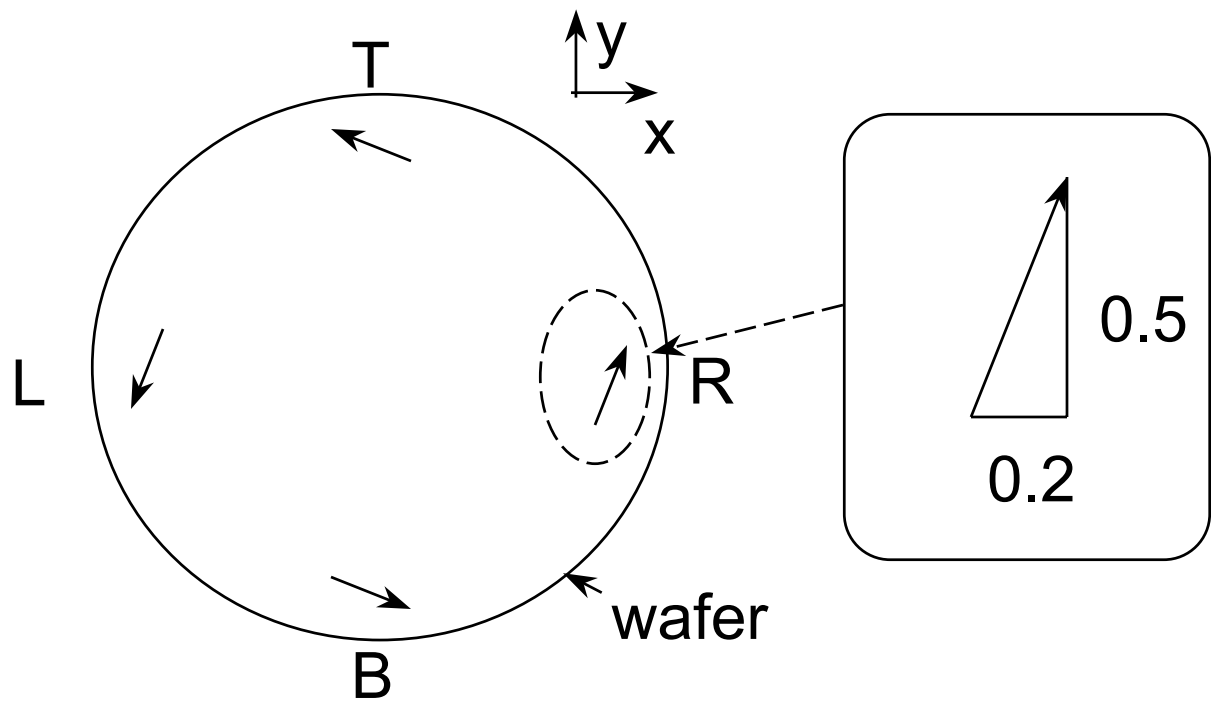
μm	T	R	C	L	B
x	0.0	0.7	0.5	0.3	1.0
y	0.7	1.0	0.5	0.0	0.3

* Center of wafer has only translation error

$$T_{\text{error}} = (0.5, 0.5)$$

After subtracting T_{error} ,

	T	R	C	L	B
x	-0.5	0.2	0	-0.2	0.5
y	0.2	0.5	0	-0.5	-0.2

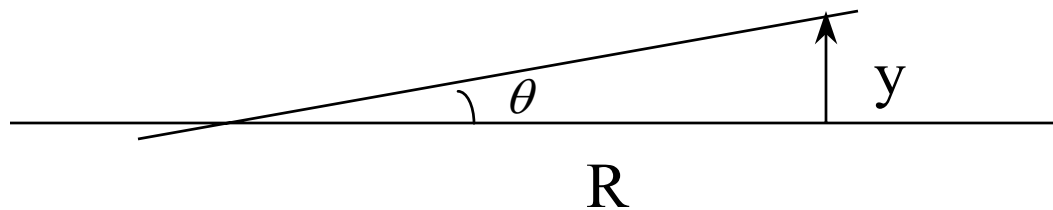


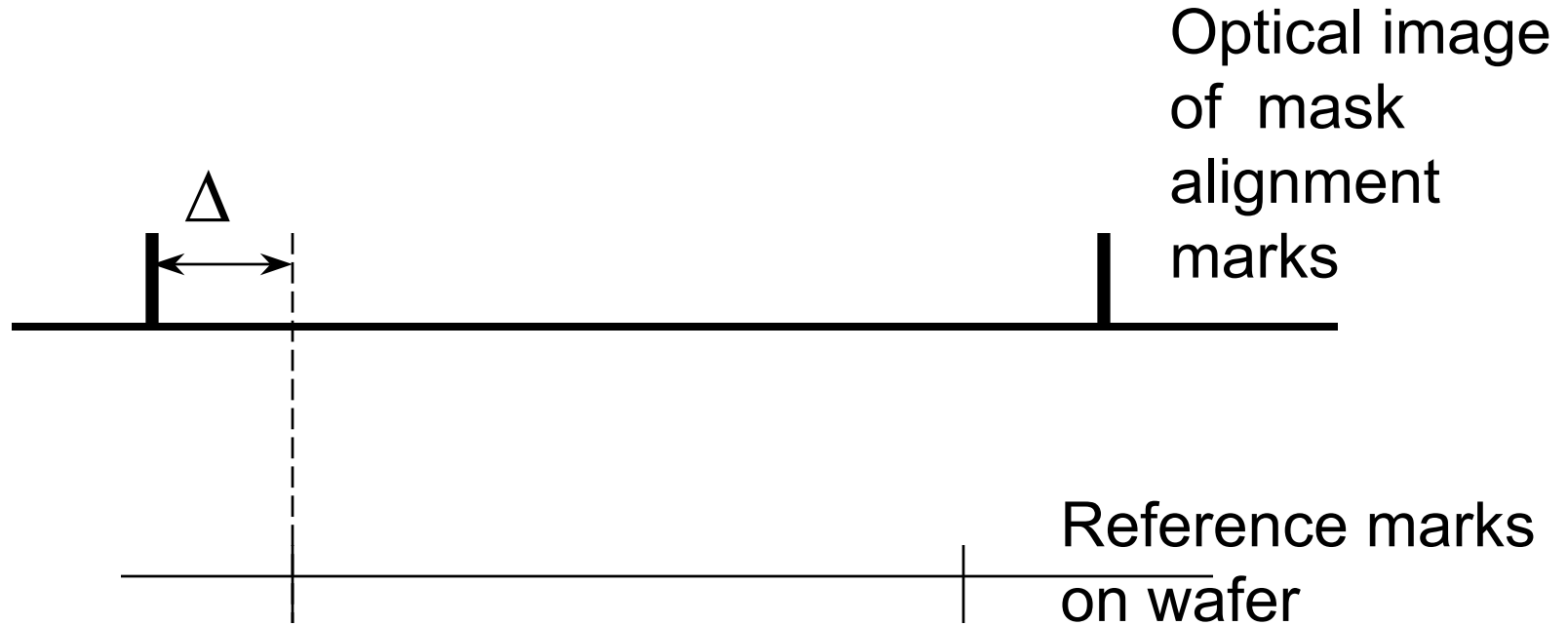
\therefore Run - out error = $0.2 \mu m$

\therefore Rotational error = $0.5 \mu m$ [counter - clockwise]

If wafer diameter is 4" $\Rightarrow D = 10 cm$

\therefore Rotational error = 10^{-5} radians





With thermal run-out, the alignment error is 1/2 of the image/reference difference [best scenario]