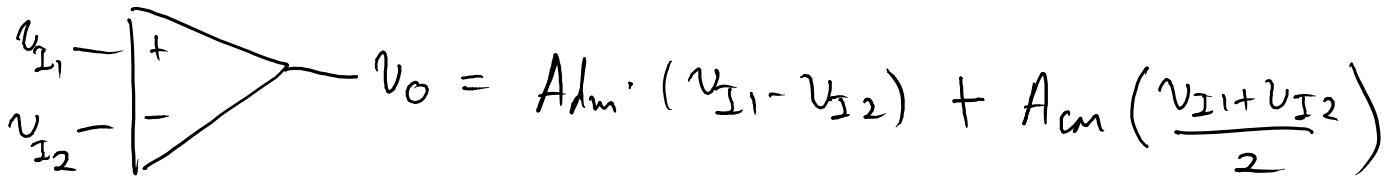
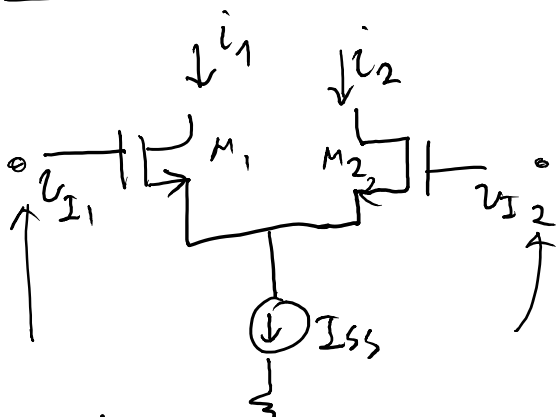


Differential Amplifier

Defs:  $v_{Id} = v_{I1} - v_{I2}$  ,  $v_{Ic} = \frac{v_{I1} + v_{I2}}{2}$

want: large  $A_{dm}$  , small  $A_{cm}$  ,  $CMRR = \left| \frac{A_{dm}}{A_{cm}} \right|$



$$\Delta i = i_1 - i_2$$

$$v_{Id} = v_{I1} - v_{I2}$$

$$i_1 = \frac{\mu_1'}{2} \frac{W}{L} (v_{GS1} - V_{th})^2$$

$$i_2 = \frac{\mu_2'}{2} \frac{W}{L} (v_{GS2} - V_{th})^2$$

Assumptions:

①  $M_1, M_2$  in SAT

②  $M_{1,2}$  identical

③ Neglect the B.E

④ Neglect  $r_o$

KVL:  $v_{I1} - v_{I2} = v_{GS1} - v_{GS2} = v_{Id}$

$$v_{Id} = v_{O1} - v_{O2} = \frac{\sqrt{i_{D1}} - \sqrt{i_{D2}}}{\sqrt{\frac{\mu_1'}{2} \frac{W}{L}}}$$

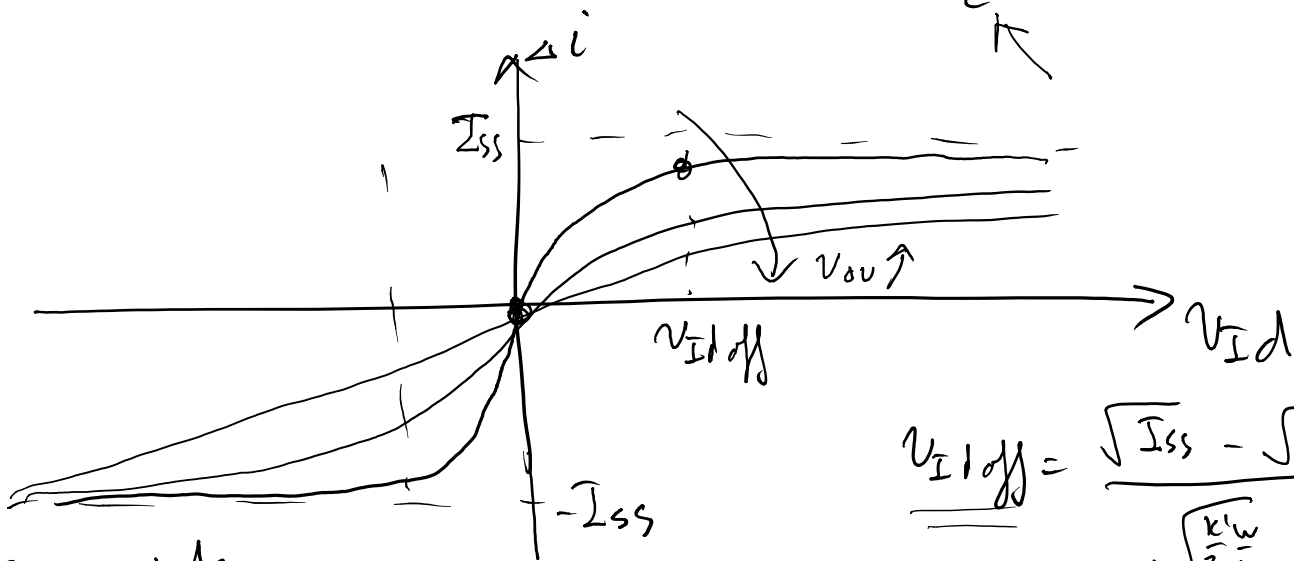
KCL:  $I_{SS} = i_1 + i_2$

Solve by  $i_1 \Rightarrow$

$$i_1 = \frac{I_{SS}}{2} + \frac{\kappa'}{4} \frac{w}{L} v_{Id} \sqrt{\frac{4I_{SS}}{\kappa' \frac{w}{L}} - v_{Id}^2}$$

$$i_2 = \frac{I_{SS}}{2} - \frac{\kappa'}{4} \frac{w}{L} v_{Id} \sqrt{\frac{4I_{SS}}{\kappa' \frac{w}{L}} - v_{Id}^2}$$

$$\Delta i = i_1 - i_2 = \frac{\kappa'}{2} \frac{w}{L} v_{Id} \sqrt{\frac{4I_{SS}}{\kappa' \frac{w}{L}} - v_{Id}^2}$$



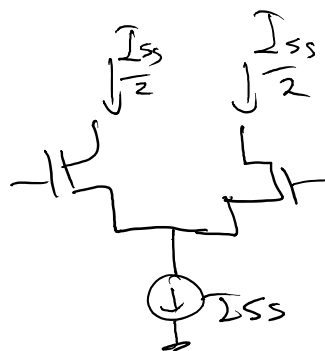
$$v_{Idoff} = \frac{\sqrt{I_{SS}} - \sqrt{0}}{\sqrt{\frac{\kappa' w}{2L}}}$$

key points:

① If  $v_{Id}$  small  
 $\Delta i \approx v_{Id} \sqrt{I_{SS}}$

②  $-I_{SS} < \Delta i < I_{SS}$

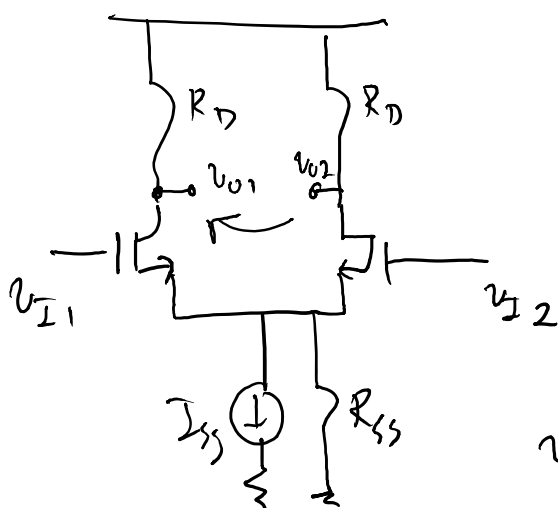
③  $v_{Idoff} = f\left(\frac{w}{L}, I_{SS}\right)$



$$= \frac{v_{ov} \sqrt{2}}{V_{GS} - V_{th}} \quad | \quad v_{Id} = 0$$

(4) Input range =  $\sqrt{2} \cdot V_{ov} \mid > 6 V_T$  (BJT)

(5) Similar to BJT with E-degeneration  $v_{Id}=0$



$$v_{O1} = A_{11} \cdot v_{I1} + A_{12} \cdot v_{I2}$$

$$v_{O2} = A_{21} \cdot v_{I1} + A_{22} \cdot v_{I2}$$

Change the variables:

$$v_{Id} = v_{I1} - v_{I2}$$

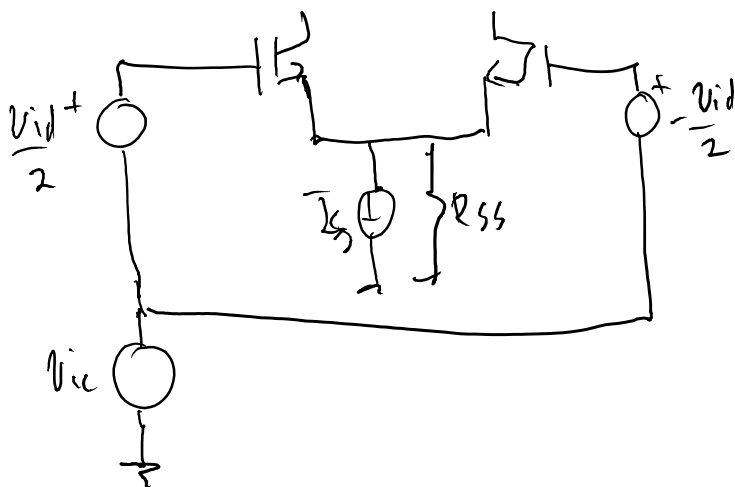
$$v_{Od} = v_{O1} - v_{O2}$$

$$v_{Ic} = \frac{v_{I1} + v_{I2}}{2}$$

$$v_{Oc} = \frac{v_{O1} + v_{O2}}{2}$$

$$v_{Od} = A_{dm} \cdot v_{Id} + A_{cm-dm} \cdot v_{Ic}$$

$$v_{Oc} = A_{dm-cm} \cdot v_{Id} + A_{cm} \cdot v_{Ic}$$

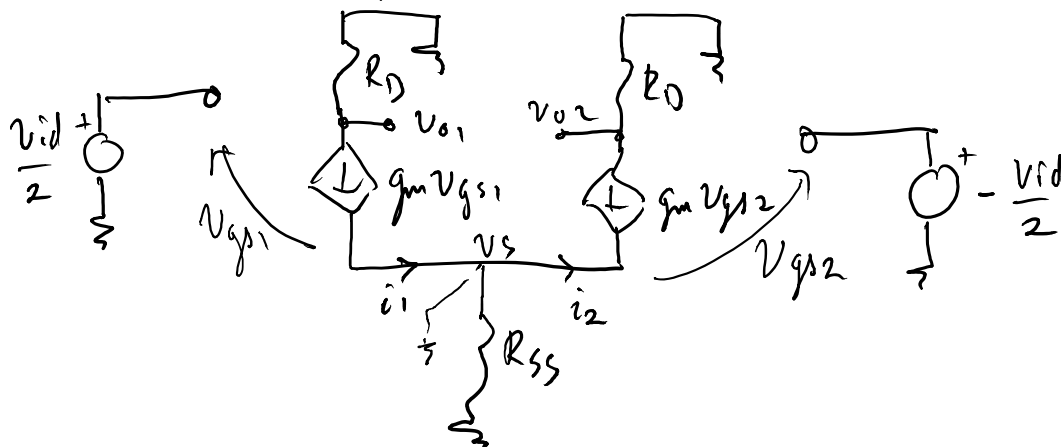


$$A_{dm} = ?$$

$$A_{cm} = ?$$

In balanced case:

$$A_{dm-cm} = A_{cm-dm} = 0$$

Superposition:a)  $v_{ic} = 0$  (Differential mode)  $A_{dm} = ?$ 

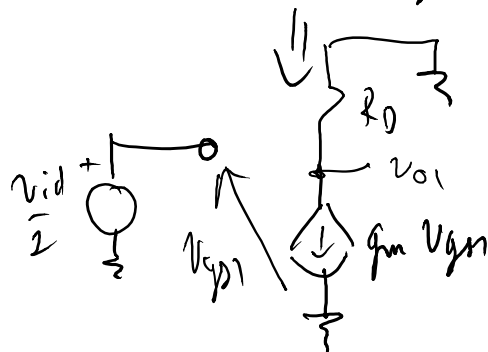
Assume:

$$v_S = 0$$

$$\frac{v_{id}}{2} = v_{gs1} = -v_{gs2}$$

$$i_1 = i_2$$

$$i_{R_{SS}} = 0 \Rightarrow v_S = 0$$



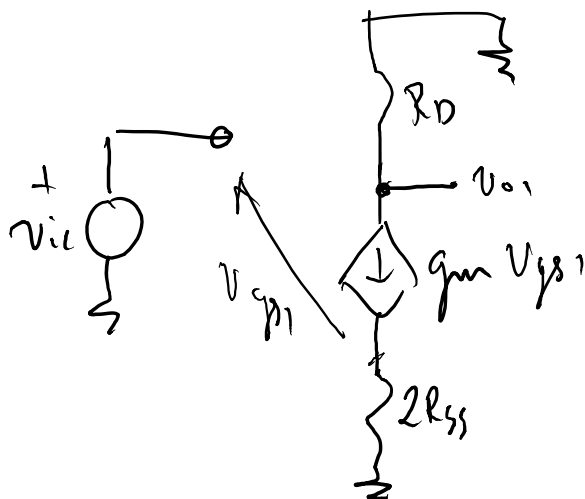
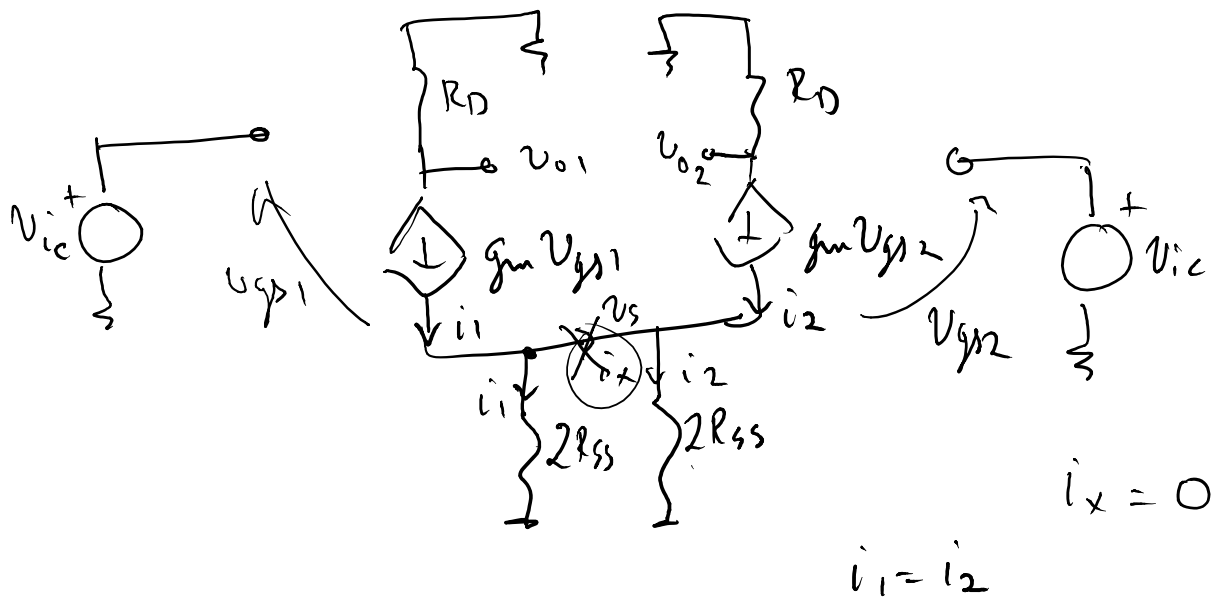
$$A_{dm} = \frac{v_{od}}{v_{id}} = -g_m R_D$$

$$\frac{v_{o1}}{\frac{v_{id}}{2}} = -g_m R_D$$

$$v_{od} = v_{o1} - v_{o2}$$

$$\frac{v_{o2}}{-\frac{v_{id}}{2}} = -g_m R_D$$

b) common-mode ( $v_{id} = 0$ )  $A_{cm} = ?$



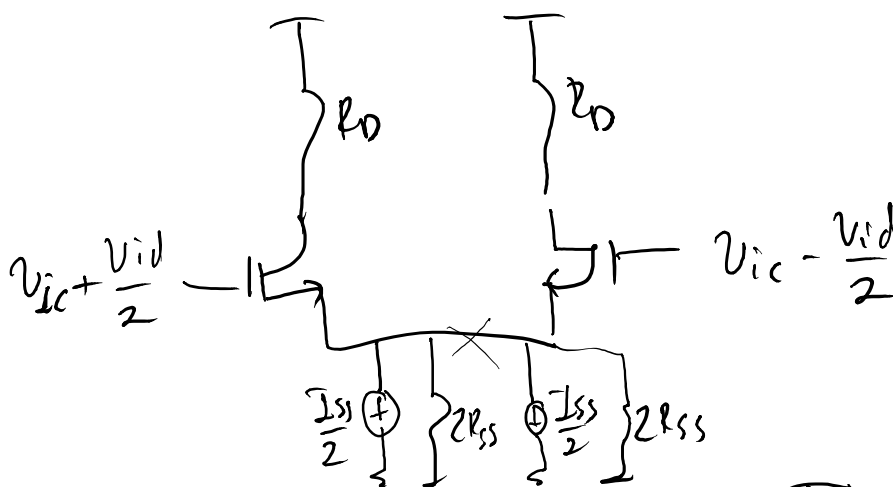
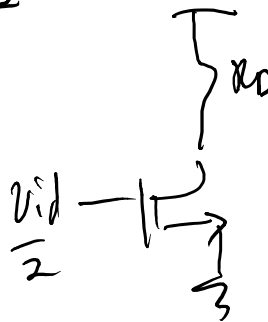
$$A_{cm} = - \frac{g_m R_D}{1 + (g_m \cdot (2R_{SS})_{+gmb})} = \frac{V_{oc}}{V_{ic}}$$

$$V_{OC} = \frac{V_{O1} + V_{O2}}{2} = V_{O1} = V_{O2}$$

# Small-signal half-circuit (bisection) analysis of balanced circuits

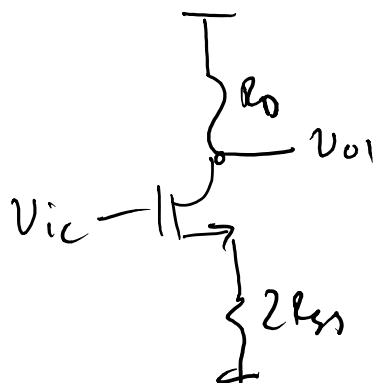
- ① Draw schematic of the dtt - see balance
- ② Use superposition
  - a) Apply DM input and simplify schematic
  - b) Apply CM input and simplify sch.
  - c) Add the two

①

②a) Apply DM  $\Rightarrow v_{ic} = 0$ 

$$A_{dm} = -g_m R_D$$

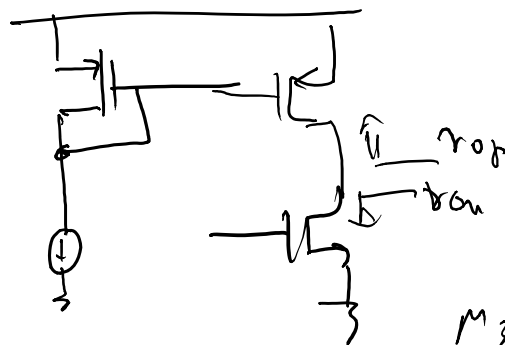
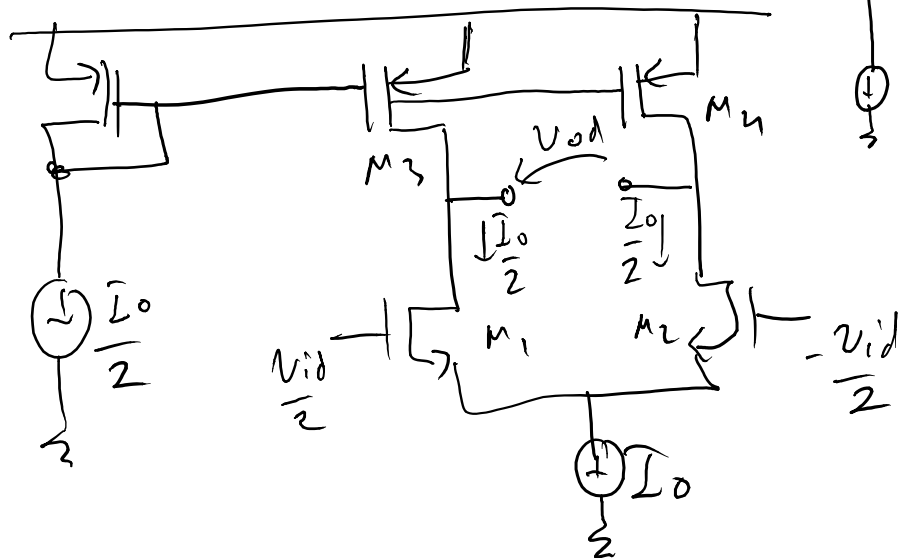
(2b)



$$A_{cm} = - \frac{g_m R_D}{1 + (2R_{ss})(g_m + g_{mb})}$$

$$CMRR = 1 + (g_m + g_{mb}) 2R_{ss}$$

Active 1:



$M_3, M_4$  identical

$$A_{dm} = \frac{v_{od}}{v_{id}} = -g_{m1}(r_{op} || r_{on})$$

$$= -g_{m1}(r_{o1} || r_{o3})$$

b) Diff pair with current mirror load

