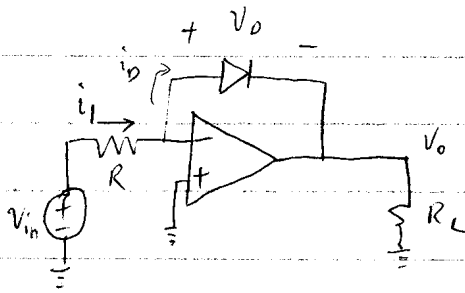


HW 8 Solution

2



$$i_1 = i_D$$

$$\frac{V_{in}}{R} = i_D \quad \text{since } V_- = V_+ = 0$$

$$\frac{V_{in}}{R} = K V_D^2$$

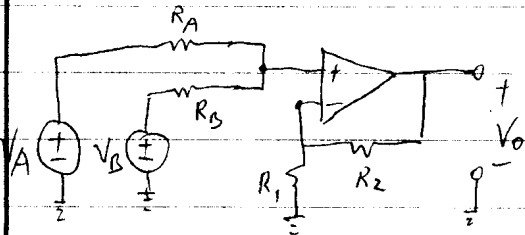
$$\frac{V_{in}}{R} = K(0 - V_o)^2 \quad \text{since } V_D = V_- - V_o$$

$$\frac{V_{in}}{R} = K(-V_o)^2$$

$$V_o = -\sqrt{\frac{V_{in}}{RK}}$$

This is an inverting amplifier

3



$$\text{KCL for node } + : \frac{V_A - V_+}{R_A} + \frac{V_B - V_+}{R_B} = 0$$

$$\text{KCL for node } - : \frac{V_o - V_-}{R_2} + \frac{0 - V_-}{R_1} = 0$$

$$V_- = \frac{R_1}{R_1 + R_2} V_o = V_+$$

$$\text{substitute } V_+ : \frac{V_A - \frac{R_1}{R_1 + R_2} V_o}{R_A} + \frac{V_B - \frac{R_1}{R_1 + R_2} V_o}{R_B} = 0$$

$$V_o = \left(\frac{R_1 + R_2}{R_1} \right) \frac{V_A R_B + V_B R_A}{R_A + R_B}$$

4

KCL for node - : $\frac{V_{in}(t) - V_-}{10K} = \frac{V_o - V_-}{R_2}$ $V_- = V_+ = V$

$$V_o = -\frac{R_2}{10K} V_{in}(t) + (1 + \frac{R_2}{10K}) V$$

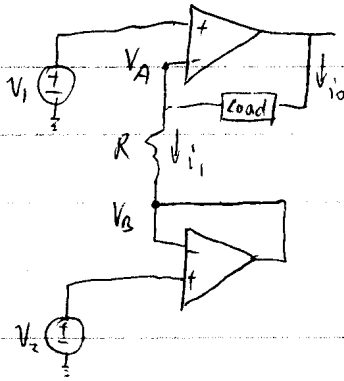
$$V_o = -\frac{R_2}{10K} (2 + 3 \cos(2000\pi t)) + (1 + \frac{R_2}{10K}) V$$

set dc component of V_o to 0 :

$$0 = -\frac{2R_2}{10K} + (1 + \frac{R_2}{10K}) V$$

$$R_2 = 10K$$

5 a



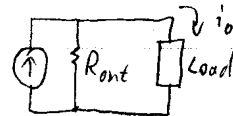
$$i_o = i_1$$

$$i_o = \frac{V_A - V_B}{R}$$

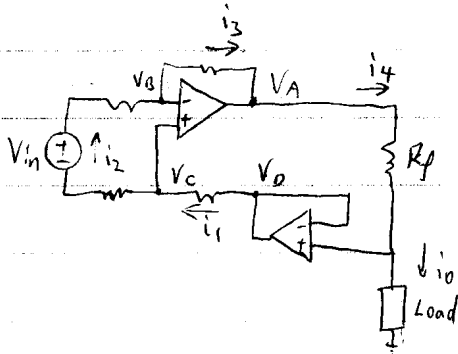
$$i_o = \frac{V_1 - V_2}{R}$$

$$V_B = V_2 \quad V_A = V_1$$

Output impedance is ∞ , because i_o is not depended on the Load impedance. Imaging :



b



Note $i_1 = i_2 = i_3$ $i_4 = i_o$

$$V_A = V_D + i_4 R_f = i_1 R + V_D + i_3 R$$

$$i_4 = \frac{2 i_1 R}{R_f}$$

$$i_1 = \frac{V_D - V_C}{R}$$

$$V_B - V_C = i_1 R + V_{in} + i_1 R = 0$$

$$i_1 = -\frac{V_{in}}{2R}$$

$$i_o = i_4 = -\frac{V_{in}}{R_f}$$

Out impedance is ∞ , same argument.

6 a KCL for V_o : $\frac{A_{ol} V_i - V_o}{R_o} = \frac{V_o - V_s}{R_{in}}$ $V_i = V_s - V_o$

$$V_o = \left(\frac{A_{ol}(V_s - V_o)}{R_o} + \frac{V_s}{R_{in}} \right) \cdot \left(\frac{R_o R_{in}}{R_o + R_{in}} \right)$$

$$\frac{V_o}{V_s} = \frac{A_{ol} R_{in} + R_o}{R_o + R_{in} + A_{ol} R_{in}}$$

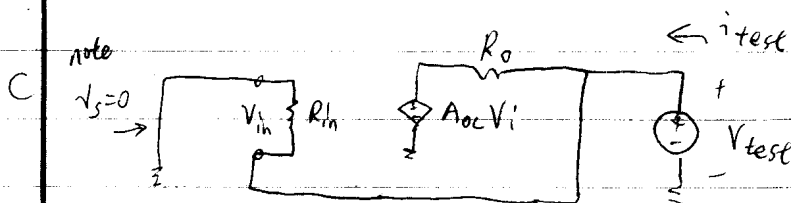
substitute values: $\boxed{\frac{V_o}{V_s} = 0.99999}$ (not 1)

b $i_s = \frac{V_s - V_o}{R_{in}}$ $V_o = A_{ol}(i_s R_{in}) + i_s R_o$

$$i_s = \frac{V_s - A_{ol} R_{in} i_s + R_o i_s}{R_{in}}$$

$$i_s = \frac{V_s}{R_{in} + R_o + A_{ol} R_{in}} \rightarrow Z_{in} = \frac{V_s}{i_s} = R_{in} + R_o + A_{ol} R_{in}$$

$$Z_{in} = 10'' \Omega \text{ (not } \infty)$$



$$V_i = -V_{test}$$

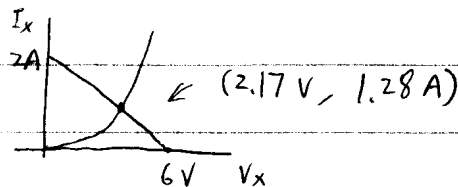
$$i_{test} = \frac{V_{test}}{R_{in}} + \frac{V_{test} - A_{ol} V_i}{R_o}$$

$$Z_o = \frac{V_{test}}{i_{test}} = \frac{1}{\frac{1}{R_{in}} + \frac{1 + A_{ol}}{R_o}} = 2.5 \times 10^{-4} \Omega \text{ (not 0)}$$

7 Using loadline analysis: $6V = 3\Omega \cdot I_x + V_x$

plot $6 = 3I_x + V_x$

$$i_x = \sqrt{x^3/8}$$



8 As the load resistance becomes smaller, the reverse current through the zener diode becomes smaller in magnitude. The smallest load for which the load voltage remains at 10V corresponds to zero diode current.

The the load current is equal to the current through the 100 Ω resistor which is $i_L = \frac{15-10}{100} = 50\text{mA}$.

\therefore the minimum load is $R_L = V_0/i_L = 200\Omega$

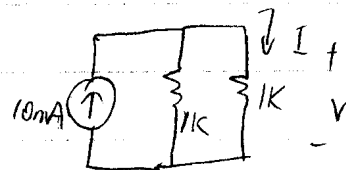
9a The diode is on, $V=0$ since voltage across ideal diode is 0.

$$I = \frac{10-0}{2.7\text{K}} = 3.7\text{mA}$$

b The diode is off, $I=0$ $\therefore V=10\text{V}$

c The diode is on, $V=0$ $I = \frac{0-0}{2.7\text{K}} = 0$

d The diode is on, equivalent ckt



$$I = 10\text{mA} \cdot \frac{1}{2} = 5\text{mA}$$

$$V = 5\text{mA} \cdot 1\text{K}\Omega = 5\text{V}$$